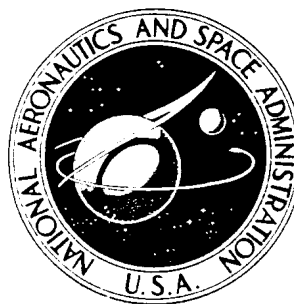


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A FORTRAN PROGRAM FOR  
DETERMINING AIRCRAFT STABILITY  
AND CONTROL DERIVATIVES  
FROM FLIGHT DATA

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# A FORTRAN PROGRAM FOR DETERMINING AIRCRAFT STABILITY AND CONTROL DERIVATIVES FROM FLIGHT DATA

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## INTRODUCTION

Determination of aircraft stability and control derivatives from flight data is of great importance in flight testing and control system design. Several methods have been used, but recent interest has turned toward maximum likelihood estimators. In addition to producing the "best" possible estimates as defined by some probabilistic criterion, these methods can be automated to a large extent.

Experience at the NASA Flight Research Center has shown that derivatives can be extracted with minimum effort by relatively inexperienced personnel using maximum likelihood estimators. Others have had some difficulty, perhaps partially due to inadequately designed programs. A production version of a maximum likelihood estimation program has been developed and used at the Flight Research Center to determine aircraft stability and control derivatives from large amounts of flight data. The program was designed to be compatible with as many types of computers as feasible and was structured to accommodate alterations easily. The program is applicable to many linear parameter estimation problems, although several of the features are intended specifically for aircraft stability and control applications. Reference 1 discusses an earlier program from which this maximum likelihood estimation program was conceptually derived.

This report presents the modified maximum likelihood estimation computer program used at the Flight Research Center for derivative extraction as well as associated programs for table lookup of initial estimates of the derivatives and for plotting results. Program listings and sample check cases for each program are included in the appendixes.

## SYMBOLS

Parenthetical symbols are computer identifiers for data channels.

A                      stability matrix, or axial force (appendix E)

$a_n$ (AN)	vertical acceleration, $g$
$a_x$ (AX)	longitudinal acceleration, $g$
$a_y$ (AY)	lateral acceleration, $g$
$B$	control matrix
$C_m$	dimensionless pitching-moment coefficient
$C_n$	dimensionless yawing-moment coefficient
$C_Z$	dimensionless normal-force coefficient
$c$	vector of unknowns
$c_0$	<i>a priori</i> value of $c$
$D1$	signal weighting matrix
$D2$	<i>a priori</i> weighting matrix
$E[ \ ]$	expected value
$E_k$	relative error
$G$	observation matrix
$g$	acceleration of gravity, $m/sec^2$ ( $ft/sec^2$ )
$H$	observation matrix
$I$	identity matrix
$I_X$	moment of inertia about the longitudinal axis, $kg-m^2$ ( $slug-ft^2$ )
$I_{XZ}$	cross-product of inertia about the longitudinal and normal axes, $kg-m^2$ ( $slug-ft^2$ )
$I_Z$	moment of inertia about the normal axis, $kg-m^2$ ( $slug-ft^2$ )
$i$	time index
$J$	cost functional



$L$	rolling moment divided by moment of inertia about longitudinal axis, $\text{rad/sec}^2$
$L_0, L_{0_2}, L_{0_3}, L_{0_4}$	rolling acceleration equation biases
$M$	pitching moment divided by moment of inertia about lateral axis, $\text{rad/sec}^2$
$M_0, M_{0_2}, M_{0_3}, M_{0_4}$	pitching acceleration equation biases
$N$	yawing moment divided by moment of inertia about normal axis, $\text{rad/sec}^2$ , or number of time points
$N_0, N_{0_2}, N_{0_3}, N_{0_4}$	yawing acceleration equation biases
$p$ (P)	roll rate, $\text{deg/sec}$ or $\text{rad/sec}$
$q$ (Q)	pitch rate, $\text{deg/sec}$ or $\text{rad/sec}$
$\bar{q}$	dynamic pressure, $\text{N/m}^2$ ( $\text{lb/ft}^2$ )
$R$	acceleration transformation matrix
$r$ (R)	yaw rate, $\text{deg/sec}$ or $\text{rad/sec}$
$S$	reference area, $\text{m}^2$ ( $\text{ft}^2$ )
$s$	auxiliary time variable, $\text{sec}$
$T$	total time, $\text{sec}$
$t$	time, $\text{sec}$
$\Delta t$	time interval between samples, $\text{sec}$
$u$	control vector
$V$	velocity, $\text{m/sec}$ ( $\text{ft/sec}$ )
$v$	variable bias vector
$W$	aircraft weight, $\text{N}$ ( $\text{lb}$ )
$X$	longitudinal force divided by mass, $\text{m/sec}^2$ ( $\text{ft/sec}^2$ )
$X_0, X_{0_2}, X_{0_3}, X_{0_4}$	longitudinal acceleration equation biases

$x$	state vector
$Y$	side force divided by mass and velocity, rad/sec
$Y_0, Y_{0_2}, Y_{0_3}, Y_{0_4}$	side force equation biases
$y$	computed observation vector
$Z$	normal force divided by mass and velocity, rad/sec
$Z_0, Z_{0_2}, Z_{0_3}, Z_{0_4}$	normal force equation biases
$z$	measured observation vector
$\alpha$ (A)	angle of attack, deg or rad
$\beta$ (B)	angle of sideslip, deg or rad
$\delta$	control, deg or rad
$\delta_a$ (DA)	aileron position, deg or rad
$\delta_c, \delta_1, \delta_2$ (DC, D1, D2)	extra controls, deg or rad
$\delta_e$ (DE)	elevator position, deg or rad
$\delta_r$ (DR)	rudder position, deg or rad
$\eta$	noise vector
$\theta$ (THET)	pitch attitude, deg or rad
$\dot{\theta}_0, \dot{\theta}_{0_2}, \dot{\theta}_{0_3}, \dot{\theta}_{0_4}$	biases in Euler pitch rate equation
$\tau$	revised time interval, sec
$\phi$ (PHI)	Euler roll attitude, deg or rad
$\dot{\phi}_0, \dot{\phi}_{0_2}, \dot{\phi}_{0_3}, \dot{\phi}_{0_4}$	biases in Euler roll rate equation

$\nabla_c$	gradient with respect to $c$
$\nabla_c^2$	second gradient with respect to $c$ (Hessian matrix)
$\mathbf{0}$	null matrix
Superscript:	
$*$	transpose
Subscripts:	
$p, q, r, V, \alpha, \beta,$ $\delta_a, \delta_c, \delta_e,$ $\delta_r, \delta_1, \delta_2$	partial derivatives with respect to the subscripted variable
$i, k$	$i^{\text{th}}$ and $k^{\text{th}}$ elements of vector or matrix
$L$	iteration number
$0$	constant value

A dot over a quantity denotes the time derivative of that quantity.

### PARAMETER ESTIMATION

The problem considered is: Given a set of flight time histories of an aircraft's response variables, find the values of some unknown parameters in the system equations that best represent the actual aircraft response. An intuitive mathematical approach to this problem would be to minimize the difference between the flight response and the response computed from the system equations. This difference could be defined for each response variable as the integral of the error squared. These signal errors could then be multiplied by weighting factors and summed to obtain the total response error, thereby defining an integral squared error criterion.

A mathematically more precise formulation can be made in probabilistic terms. For each possible estimate of the unknown parameters, a probability that the aircraft response time histories take on the values actually observed can be defined. The estimates should be chosen so that this probability is maximized. This process is referred to as a maximum likelihood formulation of the problem. Maximum likelihood estimators have many desirable characteristics; for example, they yield asymptotically unbiased and consistent estimates. If the measurement noise is assumed to be Gaussian, white, stationary, and uncorrelated, this formulation is equivalent to a response error formulation, in which the weightings used are the inverse of the measurement noise covariance matrix.

To mathematically describe the maximum likelihood estimator it is first necessary to define the equations of motion for the aircraft system. These equations are:

$$R\dot{x}(t) = Ax(t) + Bu(t) \quad (1)$$

$$y(t) = \begin{bmatrix} -\frac{I}{G} & - \end{bmatrix} x(t) + \begin{bmatrix} -\frac{\mathbf{0}}{H} & - \end{bmatrix} u(t) + \begin{bmatrix} -\frac{\mathbf{0}}{v} & - \end{bmatrix} \quad (2)$$

$$z(t) = y(t) + \eta(t) \quad (3)$$

where

$x$  state vector  
 $u$  control vector  
 $v$  bias vector  
 $y$  computed observation vector  
 $z$  measured observation vector  
 $\eta$  noise vector

For the aircraft problem being considered, it is convenient to separate the equations of motion into longitudinal and lateral-directional sets. The linearized longitudinal equations are:

$$\frac{d}{dt} \begin{bmatrix} \alpha \\ q \\ V \\ \theta \end{bmatrix} = \begin{bmatrix} Z_\alpha & 1 & Z_V & -\sin(\theta) \cos(\varphi) \frac{g}{V} \\ M_\alpha & M_q & M_V & 0 \\ X_\alpha & 0 & X_V & -\cos(\theta)g \\ 0 & \cos(\varphi) & 0 & 0 \end{bmatrix} \begin{bmatrix} \alpha \\ q \\ V \\ \theta \end{bmatrix} + \begin{bmatrix} Z_{\delta_e} & Z_{\delta_c} & Z_{\delta_1} & Z_{\delta_2} & Z_0 \\ M_{\delta_e} & M_{\delta_c} & M_{\delta_1} & M_{\delta_2} & M_0 \\ X_{\delta_e} & X_{\delta_c} & X_{\delta_1} & X_{\delta_2} & X_0 \\ 0 & 0 & 0 & 0 & \dot{\theta}_0 \end{bmatrix} \begin{bmatrix} \delta_e \\ \delta_c \\ \delta_1 \\ \delta_2 \\ 1 \end{bmatrix} \quad (4)$$

$$a_n = -\frac{V}{g} \left[ \dot{\alpha} - q + \sin(\theta) \cos(\varphi) \frac{g}{V} \theta \right] + a_{n,bias} \quad (5)$$

The linearized lateral-directional equations are:

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & -\frac{I_{XZ}}{I_X} & 0 \\ 0 & -\frac{I_{XZ}}{I_Z} & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} \beta \\ p \\ r \\ \varphi \end{bmatrix} = \begin{bmatrix} Y_\beta & \sin(\alpha) & -\cos(\alpha) & \cos(\varphi) \cos(\theta) \frac{g}{V} \\ L_\beta & L_p & L_r & 0 \\ N_\beta & N_p & N_r & 0 \\ 0 & 1 & \cos(\varphi) \tan(\theta) & 0 \end{bmatrix} \begin{bmatrix} \beta \\ p \\ r \\ \varphi \end{bmatrix} + \begin{bmatrix} Y_{\delta_a} & Y_{\delta_r} & Y_{\delta_1} & Y_{\delta_2} & Y_0 \\ L_{\delta_a} & L_{\delta_r} & L_{\delta_1} & L_{\delta_2} & L_0 \\ N_{\delta_a} & N_{\delta_r} & N_{\delta_1} & N_{\delta_2} & N_0 \\ 0 & 0 & 0 & 0 & \dot{\varphi}_0 \end{bmatrix} \begin{bmatrix} \delta_a \\ \delta_r \\ \delta_1 \\ \delta_2 \\ 1 \end{bmatrix} \quad (6)$$

$$a_y = \frac{V}{g} \left[ \dot{\beta} - \sin(\alpha)p + \cos(\alpha)r - \cos(\varphi) \cos(\theta) \frac{g}{V} \varphi \right] + a_{y,bias} \quad (7)$$

The unknown parameters are contained in the matrices  $A$ ,  $B$ ,  $G$ , and  $H$  and in the bias vector,  $v$ . For notational simplicity, the unknown parameters will be regarded as forming a vector  $c$ . Then  $A$ ,  $B$ ,  $G$ ,  $H$ , and  $v$  are functions of  $c$ . There is no provision for modeling state noise, that is, random or unknown inputs to the system such as turbulence. (This problem is treated in reference 2.) Instead, it is assumed that noise is introduced only in the measurement process. It is also assumed that there is no noise in the control measurements.

The integral squared error criterion can now be expressed as finding the vector of unknowns,  $c$ , that minimizes the cost functional:

$$J = \frac{1}{T} \int_0^T [z(t) - y(t)]^* D1 [z(t) - y(t)] dt \quad (8)$$

or as approximated in the discrete case:

$$J = \frac{1}{(N - 1)} \sum_{i=1}^N (z_i - y_i)^* D1 (z_i - y_i) \quad (9)$$

where  $D1$  is the symmetric, non-negative definite weighting matrix,  $i$  is a time index, and  $N$  is the number of time points. The cost functional,  $J$ , can also be called the index of performance or the fit error.

## SOLUTION BY THE MODIFIED NEWTON-RAPHSON METHOD

Several algorithms for the minimization of nonlinear functionals exist that could be used to minimize  $J$ . The modified Newton-Raphson method has proved to be the most suitable for aircraft derivative determination, both in terms of computer time and convergence properties.

The Newton-Raphson algorithm is an iterative method of functional minimization which requires some initial estimate of  $c$  and a means of computing the first and second gradients of  $J$  with respect to  $c$ . Revised estimates of  $c$  are then obtained from the equation

$$c_L = c_{L-1} - \left( \nabla_c^2 J \right)_L^{-1} \left( \nabla_c J \right)_L^* \quad (10)$$

where  $L$  denotes the iteration number,  $\nabla_c$  indicates the gradient with respect to  $c$ , and  $\nabla_c^2$  indicates the second gradient. The first and second gradients of  $J$  are then

$$\nabla_c J = \frac{2}{(N - 1)} \sum_{i=1}^N (z_i - y_i)^* D1 \nabla_c (z_i - y_i) \quad (11)$$

$$\nabla_c^2 J = \frac{2}{N-1} \sum_{i=1}^N \nabla_c(z_i - y_i)^* D1 \nabla_c(z_i - y_i) + \frac{2}{(N-1)} \sum_{i=1}^N (z_i - y_i)^* D1 \nabla_c^2(z_i - y_i) \quad (12)$$

Computation of  $\nabla_c(z_i - y_i)$  is relatively straightforward, as described in reference 3. Computation of  $\nabla_c^2(z_i - y_i)$  is much more time consuming; however, Balakrishnan shows in reference 4 that the contribution of this term to the second gradient goes to zero as the process converges. Thus, if we neglect this term, the method is still an asymptotically unbiased estimator. The Newton-Raphson algorithm with this term neglected is referred to as the modified Newton-Raphson algorithm and provides the same result as obtained by quasilinearization.

Reference 1 describes a modification in the computation of the gradient that is used on the first iteration. This modification, analogous to linear least squares, helps to obtain convergence when the initial estimates are far from the minimum. With this modification it is often possible to start with estimates of zero for all the unknowns and still converge to the correct solution.

### INCLUSION OF A PRIORI INFORMATION

Information from wind tunnel studies, previous flight tests, and other sources (referred to collectively as predicted derivatives) is often available on the values of some of the aircraft derivatives. It may be desirable to include this information in the program's algorithm. The use of this information is particularly important when there is a linear dependence or near dependence of the effect of several derivatives, for instance, in a maneuver in which the control motion is due largely or solely to a feedback of the states. The second gradient matrix then becomes ill-conditioned, resulting in poor convergence properties and unreliable estimates. In most instances a true minimum of the cost functional is still approached, despite the ill conditioning. The location of this minimum may not be important, however, because the linearly dependent derivatives could be altered greatly without significantly increasing the cost. In this instance the slight improvement in the fit obtained by altering the derivatives would not seem sufficient justification for altering them from the *a priori* values.

One solution to this problem would be to add to the cost functional a quadratic penalty function for departure from the *a priori* values. The cost functional,  $J$ , would then be

$$J = \frac{1}{(N-1)} \sum_{i=1}^N (z_i - y_i)^* D1(z_i - y_i) + (c - c_0)^* D2(c - c_0) \quad (13)$$

where  $c_0$  is the *a priori* estimate, and  $D2$  is a symmetric, non-negative definite

weighting matrix. The algorithm with this penalty function will be referred to as the modified maximum likelihood estimator. It is important in this formulation for the elements of  $D2$  to be small enough that, in general,  $(c - c_0)^* D2 (c - c_0)$  is significantly less than  $\frac{1}{(N - 1)} \sum_{i=1}^N (z_i - y_i)^* D1 (z_i - y_i)$ . Thus the estimates of those parameters that are well defined by the response data will not be altered.

The first and second gradients of  $J$  now become

$$\nabla_c J = \frac{2}{(N - 1)} \sum_{i=1}^N (z_i - y_i)^* D1 \nabla_c (z_i - y_i) + 2(c - c_0)^* D2 \quad (14)$$

$$\nabla_c^2 J = \frac{2}{(N - 1)} \sum_{i=1}^N \nabla_c (z_i - y_i)^* D1 \nabla_c (z_i - y_i) + 2 D2 \quad (15)$$

where the second term of equation (12) has been neglected.

When this feature is used, convergence is generally improved. With small enough values of  $D2$ , the estimates of the derivatives are not affected when the maneuver is well conditioned, but poorly conditioned maneuvers may converge and reveal some information instead of diverging.

## CONFIDENCE LEVELS

One advantage of using a maximum likelihood estimator to determine aircraft stability and control derivatives is that an objective measure of the validity of the estimates is obtainable. With some other methods the main criterion of the validity of an estimate is the engineer's subjective judgment.

If the noise obeys the stated assumptions and  $D1$  is, in fact, the inverse of the noise covariance matrix, the Cramèr-Rao inequality (ref. 3) gives a lower bound on the covariance matrix of the estimates as follows:

$$E \left[ (c - c_0)(c - c_0)^* \right] \geq \left[ \sum_{i=1}^N \nabla_c (z_i - y_i)^* D1 \nabla_c (z_i - y_i) \right]^{-1} \quad (16)$$

The right side of this inequality is recognized as  $(\nabla_c^2 J)^{-1}$  evaluated without the term for *a priori*. This expression is available in the minimization algorithm (eq. (12)), so these confidence levels (sometimes referred to in the literature as

uncertainty levels) may be obtained with little additional effort. They can be useful in assessing the validity of the estimates obtained even when the noise characteristics are different from those assumed.

## DESCRIPTION AND USE OF PROGRAMS

A basic computer program and two associated programs form a package that has been used at the NASA Flight Research Center to successfully analyze 1500 maneuvers from 20 aircraft. The basic program, referred to as the modified maximum likelihood estimation program, or MMLE, is designed to obtain maximum likelihood estimates from flight data. The associated programs, SETUP and SUMMARY, although not directly related to the mathematical aspects of parameter estimation, have proved useful in extracting aircraft derivatives. The programs are designed to be used easily with the longitudinal and lateral equations of motion (eqs. (4) to (7)) by applying appropriate default values. For the options in the programs, the values designated as defaults are used only if no other values are specified. Each program is discussed in detail in the following sections.

In these programs a general matrix storage convention that permits flexibility and error checking is used. Each matrix is dimensioned with a fixed number of rows, MAX. The last row of the matrix, however, contains information about the matrix, instead of containing matrix elements. The first number in the last row is the number of rows of the matrix that are used; the second number is the number of columns used; and the third element is the matrix name in A format. For example, a 19 by 4 matrix called XJI could be stored in an array dimensioned 35 by 8 as:

		4 columns	4 columns
19 rows	{	Matrix elements	Unused
15 rows	{	-----	-----
Last row	{	19. 4. XJI	Unused

This convention permits a variable-size matrix to be stored in an array of fixed dimension. The matrix manipulation subroutines can also check matrix compatibility by examining the last row before performing operations.

The programs use a standard matrix input format which facilitates data checking. The first card of any matrix to be input is a header card containing the name of the matrix, left-justified, in columns 1 to 4, the number of rows in the matrix, right-justified, in columns 9 to 10, and the number of columns in the matrix, right-justified, in columns 11 to 20. The body of the matrix follows, one row to a card, in an 8F10 format.

Additionally, the abbreviation T is used to denote true and F to denote false. NAMELIST variables follow the FORTRAN convention for type (names beginning with I, J, K, L, M, or N indicate integer variables; all other names indicate real variables), unless stated otherwise. Exceptions to this convention are given in parentheses after the NAMELIST variable.



## MMLE — MODIFIED MAXIMUM LIKELIHOOD ESTIMATION PROGRAM

The MMLE program can be run on most large modern computers with FORTRAN IV compilers. Approximately  $31,000_{10}$  words of core storage are required. If overlay or segmentation is used, this requirement can be reduced to about  $22,000_{10}$ . Overlay and segmentation, however, are machine specific; directives for segmenting the MMLE program on the CDC OPERATING SYSTEM SCOPE 3.4 (ref. 5) are included in appendix A (p. 92) and can be used as a guide for implementation on other systems. Some form of automatic plotting equipment is desirable. The MMLE program plotting routines are written for a CalComp pen plotter (ref. 6). If other plotting equipment is used, it may be necessary to modify the plotting routines. The user must verify whether the routines supplied are compatible with the system being used.

From 4000 to 20,000 words of temporary disk storage are required, depending on the number of data points. This requirement is doubled if plots are made. A tape drive (two if plots are desired) may be substituted for disk storage.

Two types of input data are required for the MMLE program. The measured values contained in time histories of a flight maneuver must be available on cards, tape, or a disk file. These time histories are limited by dimensions in the plotting routines to 1000 time points per maneuver; these dimensions may be changed easily. In addition, the program must be provided information on the flight condition of the maneuver, values of pertinent characteristics of the aircraft, a set of starting estimates of the derivatives, and instructions controlling the activation of different program options.

Listings of the MMLE program and its subroutines are given in appendix A. A sample case is presented in appendix B.

### Input Description

The inputs required for the MMLE program are described in this section. Each program option is explained immediately after the description of the input that controls the option.

*Title card.*— The title card contains any information needed to identify a particular set of data that is appropriate to include in the printed and plotted MMLE output. All 80 columns on this card may be used.

*NAMelist/INPUT/.*— (See appropriate FORTRAN reference manuals for the format for specific machines.) The parameters included in the NAMelist are as follows:

(1) LONG, LATR-(logical) — type of aerodynamic mode to be analyzed. The mode type is indicated by LONG = T or LATR = T for longitudinal or lateral-directional, respectively. Only one type should be set. If neither is set, the type

is determined from the A matrix: LONG if  $A(1,2) > +0.5$ , LATR otherwise. This element is usually +1 in a longitudinal case or sin (ALPHA) in a lateral-directional case.

Items (2) to (11) are related to the input time histories. The signals which are input from the time histories fall into three classes: observations, controls, and extra. The observations form a vector,  $z$ , seven words long; the controls form a vector,  $u$ , four words long; and the extra signals form a vector four words long of quantities not actually used in the estimation process but useful in evaluating the quality of the maneuver. For a longitudinal case,

$$z = [\alpha \ q \ V \ \theta \ a_n \ \dot{q} \ a_x]^* \quad (17)$$

$$u = [\delta_e \ \delta_c \ \delta_1 \ \delta_2]^* \quad (18)$$

$$\text{Extra} = [\varphi \ \text{Altitude} \ \text{Mach number} \ \bar{q}]^* \quad (19)$$

and for a lateral-directional case,

$$z = [\beta \ p \ r \ \varphi \ a_y \ \dot{p} \ \dot{r}]^* \quad (20)$$

$$u = [\delta_a \ \delta_r \ \delta_1 \ \delta_2]^* \quad (21)$$

$$\text{Extra} = [\alpha \ V \ \text{Mach number} \ \bar{q}]^* \quad (22)$$

(2) CARD, TAPE-(logical) – input source for time histories. Set either CARD = T or TAPE = T. Only one of the two variables can be set to true in the NAMELIST. Default condition is TAPE = T.

(3) SPS – sample rate of input time histories (samples per second). If SPS is not set, a default value is computed from the times shown on the time histories. The times of the first two data points are subtracted and the difference rounded to the nearest 5 milliseconds. The reciprocal of this value is then used as the default value for SPS.

(4) THIN-(integer) – thinning factor for input data. If THIN = 1, every point on the file is used; if THIN = 2, every second point is used, and so forth. SPS is the sampling rate of the data before this thinning. Default value of 1 is used.

(5) NCASE – number of disjoint maneuvers to be used in obtaining one set of estimates. If two or more maneuvers were performed at approximately the same flight condition, they may be processed together to obtain a single set of estimates. Each interval will be weighted by the number of time points in the interval. Default value of 1 is used.

(6) SCALE-(seven-word vector) – scale factor for observations. The observations are multiplied by corresponding elements of SCALE when read in to compensate for any scaling errors or sign changes. Default sets all elements of the vector to 1.0.

(7) FIXED-(seven-word vector) – fixed biases for observations. The known biases are added to the corresponding observations after scaling (item (6)) but before any other operations with the data. Default sets all elements of the vector to 0.

(8) DC-(four-word vector) – known biases for controls. These biases are added to the corresponding controls before any operations with the controls. Default sets all elements of the vector to 0.

(9) NREC – number of data words in each record on input tape. This parameter has no meaning if card input is used. The total number of words in each record should be at least NREC + 4, because the first four words in the record contain the time (hours, minutes, seconds, milliseconds) and are not counted as data words. (See data file input section, p. 24.) NREC is limited by program dimensions to  $\leq 100$ . Default value of 15 is used unless BOTH = T (item (11)); then the value of 25 is used instead.

(10) ORDER-(15-word integer vector) – location of desired signals on input tape. This parameter has no meaning if card input is used. The signals  $z$ ,  $u$ , and extra are considered to form a single vector of signals, and ORDER describes a mapping of the data record from the tape onto this vector. The  $I^{\text{th}}$  word in the resulting vector is set equal to the ORDER (I) data word in the tape record. (The first four words in the tape record contain the time and are not counted as data words.) The default is ORDER (I) = I for I = 1, 2, . . . 15, which implies that there is no reordering from the input tape to the program.

(11) BOTH-(logical) – special signal order with both longitudinal and lateral-directional data on the tape. This parameter has no meaning if card input is used. If BOTH = T, the input tape is assumed to contain all the data, both longitudinal and lateral-directional, in a specific order. This order is  $\alpha$ ,  $q$ ,  $V$ ,  $\theta$ ,  $a_n$ ,  $\dot{q}$ ,  $a_x$ ,  $\delta_e$ ,  $\delta_c$ ,  $\delta_1$ ,  $\delta_2$ ,  $\varphi$ , altitude, Mach number,  $\bar{q}$ ,  $\beta$ ,  $p$ ,  $r$ ,  $a_y$ ,  $\dot{p}$ ,  $\dot{r}$ ,  $\delta_a$ ,  $\delta_r$ ,  $\delta_{1_{\text{lateral}}}$ , and  $\delta_{2_{\text{lateral}}}$ , where normally all angular measurements are in degrees, accelerations in  $g$  units, and velocities in feet per second. Also, if BOTH = T, NREC is overridden and set to 25; if the case is lateral-directional, the ORDER array is automatically set to [16 17 18 12 19 20 21 22 23 24 25 1 3 14 15], which overrides any order that may have been read in. Thus if the tape has data in the proper order, BOTH may be set to T and the program will automatically pick off the appropriate signals for the type of case being analyzed. Default condition is F.

Items (12) to (18) specify the form of the plotted output.

(12) PLOTEM-(logical) – time history plots comparing measured and estimated response produced if PLOTEM = T. If PLOTEM = F, no plots are made. If the *a priori* variation option (item (53)) is activated, the related derivative plots will be made instead. Default condition is T.

(13) PLTMAX – maximum error for plotting. If the error sum,  $J$ , of the last or next to last iteration is greater than PLTMAX, time history plots are not made, even

if PLOTEM = T, to avoid exceeding reasonable plotter limits. Instead, the measured time histories are printed to provide hints about the presumed problem. PLTMAX may not be larger than ERRMAX (item (22)) or it will be set equal to ERRMAX by the program. Default value of  $1. \times 10^5$  is used.

(14) INCH-(logical) – plots scaled for inch grid paper if INCH = T; otherwise, for centimeter grid paper. Default condition is F.

(15) ZMIN, ZMAX-(seven-word vectors) – minimum and maximum values on vertical axis for plots comparing measured and estimated observations. The axes are 4 centimeters long (2 inches if INCH = T). If corresponding elements of ZMIN and ZMAX are equal for any signal, automatic scaling will be used on that signal. Default values are all 0 (which implies that automatic scaling is used for the default, since ZMIN = ZMAX).

(16) DCMIN, DCMAX-(eight-word vectors) – minimum and maximum values on vertical axes for plots of controls and extra signals. The comments about ZMIN and ZMAX (item (15)) apply. In addition, if automatic scaling is used for a signal and there is no nonzero point on that signal, the plot of the signal will be omitted. Default values of 0 are used.

(17) NC PLOT – number of controls and extra signals for plotting. Only the first NC PLOT controls and extra signals will be plotted in addition to the observations. This option may be used to reduce plotting of data that may be extraneous for some cases. The value of NC PLOT must be between 1 and 8, inclusive. Default value of 8 is used.

(18) TIMES C – time scale for plots in seconds per centimeter (or seconds per half inch if INCH = T). Default value of 1. is used.

(19) PRINT-(logical) – time histories based on measured data and final computed time histories printed if PRINT = T. Default condition is F.

(20) TEST-(logical) – extra output printed each iteration if TEST = T to facilitate debugging. Extra output includes time histories (in radians), the transition matrix (ref. 8) and its integral, and the first and second gradients of  $J$ . Default condition is F.

(21) NOITER – number of iterations desired. NOITER = 0 is defined as a special case for which the program computes the final time histories using initial estimates of the unknown coefficients; that is, the parameter estimation step is omitted entirely. The measured time histories are always printed when NOITER = 0, regardless of the value of PRINT (item (19)). Default value of 6 is used.

(22) ERRMAX – maximum allowable error sum. If the error sum,  $J$ , at any time becomes greater than ERRMAX, this is taken as an indication that the process is not converging properly. Therefore, iteration will stop and the measured time histories will be printed to provide clues to the reason for the problem. Default value of  $1. \times 10^{20}$  is used.

(23) BOUND – convergence bound. If the error sum,  $J$ , in any iteration changes by less than BOUND times the error of the previous iteration, the process is assumed to have converged and iteration is stopped. Default value of 0.001 is used.

(24) PUNCH-(logical) – punched card output of nondimensional estimates. If PUNCH = T, the final estimates of the nondimensional derivatives are punched on cards along with the confidence levels obtained from the Cramèr-Rao bound. Default condition is F.

(25) PUNCHD-(logical) – punched card output of dimensional estimates. If PUNCHD = T, the final dimensional A and B matrices are punched on cards. These cards can be used to restart the program from the final values. Default condition is F.

(26) NEAT – number of time reductions in computation of transition matrix,  $e^{A\Delta t}$ , and its integral. In typical aircraft uses, a direct series evaluation of  $e^{A\Delta t}$  may become computationally unstable for sample rates less than about 10 samples per second. In such cases, the power series evaluation has been used to compute  $e^{A\tau}$  and its integral, with  $\tau = \frac{\Delta t}{2^{\text{NEAT}}}$ . The desired transition matrices are then obtained after recursive applications of the formulas:

$$e^{At} = \left[ e^{(At)/2} \right]^2 \quad (23)$$

$$\int_0^t e^{As} ds = \left[ e^{(At)/2} + I \right] \int_0^{t/2} e^{As} ds \quad (24)$$

This process provides improved computational stability without increased time or complexity. In general, NEAT should be large enough to make  $\tau \leq 0.05$  second. NEAT = 0 implies direct series computation. Default value of 0 is used.

Items (27) to (48) are related to the geometry of the aircraft and the flight condition. Items (28) to (35) are required only if nondimensional derivatives are of interest. If these items are not entered, very large values of all nondimensional derivatives will be printed as a result of the default values to avoid accidental use of the meaningless nondimensional coefficients.

(27) METRIC-(logical) – unit designation for aircraft data. If METRIC = T, all units are standard SI (MKS) units (meter, kilogram, second); otherwise, U.S. Customary (EGS) units are assumed. Default condition is F. All input data units must be consistent with the system specified.

(28) GROSWT – aircraft gross weight (pounds or newtons). Default value of  $1. \times 10^9$  is used.

(29) IX-(real) – moment of inertia about the X-axis. This parameter is not needed for longitudinal cases (slug-ft<sup>2</sup> or kg-m<sup>2</sup>). Default value of  $1. \times 10^9$  is used.

(30) IY-(real) – moment of inertia about the Y-axis. This parameter is not needed for lateral-directional cases (slug-ft<sup>2</sup> or kg-m<sup>2</sup>). Default value of  $1. \times 10^9$  is used.

(31) IZ-(real) – moment of inertia about the Z-axis. This parameter is not needed for longitudinal cases (slug-ft<sup>2</sup> or kg-m<sup>2</sup>). Default value of  $1. \times 10^9$  is used.

(32) IXZ-(real) – cross-product of inertia between X- and Z-axes. This parameter is not needed for longitudinal cases (slug-ft<sup>2</sup> or kg-m<sup>2</sup>). Default value of 0 is used.

(33) SPAN – wing span (ft or m). Default value of 0.001 is used.

(34) CBAR – reference chord (ft or m). Default value of 0.001 is used.

(35) S – reference wing area (ft<sup>2</sup> or m<sup>2</sup>). Default value of 0.001 is used.

Items (36) to (42) concern instrument locations relative to the center of gravity. Angle-of-attack and angle-of-sideslip vane readings are corrected to the center of gravity by using the angular rates. The system model includes an arbitrary accelerometer location, so that accelerations need not be corrected to the center of gravity. The longitudinal axis locations are positive for instruments forward of the center of gravity, and the normal axis locations are positive for instruments below the center of gravity. All values are in feet or meters, and a default value of 0 is used.

(36) XB – location of angle-of-sideslip vane along the longitudinal axis.

(37) XALF – location of angle-of-attack vane along the longitudinal axis.

(38) ZB – location of angle-of-sideslip vane along the normal axis.

(39) XAY – location of  $a_y$  accelerometer along the longitudinal axis.

(40) ZAY – location of  $a_y$  accelerometer along the normal axis.

(41) XAN – location of  $a_n$  accelerometer along the longitudinal axis.

(42) ZAX – location of  $a_x$  accelerometer along the normal axis.

Items (43) to (46) are not used in the estimation process, but are useful for identifying the flight condition of the maneuver. They are passed to the SUMMARY program for plot identification purposes.

(43) CG – aircraft center of gravity in fraction of chord. Default value of 0.25 is used.

(44) MACH-(real) – average Mach number. If 0, this parameter will be obtained from the input time history. Default value of 0 is used.

(45) ALPHA – average angle of attack. If 999., this parameter will be obtained from the input time history. Default value of 999. is used.

(46) PARAM – any other parameter that might be used to distinguish between flight conditions. PARAM may be used as flap position or wing sweep. Default value of 0 is used.

(47) Q – average dynamic pressure. If 0, this parameter is obtained from the input time history (lb/ft<sup>2</sup> or N/m<sup>2</sup>). Default value of 0 is used.

(48) V – average velocity. If 0, this parameter is obtained from the input time history (ft/sec or m/sec). Default value of 0 is used.

(49) VAR-(three-word logical vector) – option that controls variable bias. The fifth to seventh signals of the observation vector have an unknown bias that is included in the system model. (See p. 12 for the elements of the observation vector.) This bias is determined if the corresponding elements of VAR are T. The initial values of these variable biases are 0, except for the  $a_n$  bias in a longitudinal case, which starts with a value of 1. The bias on a signal that has a D1 weighting of 0 cannot be determined; therefore, any attempt to determine a bias for an unweighted signal will be overridden in the program. Default sets all elements of the vector to T.

(50) ZERO-(four-word logical vector) – option that requires the program to determine variable initial condition. For each element of ZERO that is T, a variable increment to the initial condition is determined for the corresponding state. This increment is added to the measured initial condition to obtain the initial condition used for the computed data. If the variable initial condition is used in conjunction with NCASE > 1 (item (5)), the same increment from the measured value is used for each maneuver in the case. Default sets all elements of the vector to F.

(51) ND1, D1RLX, D1TOL – parameters that affect diagonal D1 determination option. This puts the program into a different mode of operation. A D1 weighting matrix (see matrix input section) should be determined for each airplane at the beginning of its flight program. This option automatically determines the diagonal elements of the D1 matrix based on a particular case and is activated if ND1 > 0. The program executes one run with the initial D1 matrix (described on p. 23) input, or its default, and then applies a simple iterative algorithm ND1 times to determine the proper D1 matrix. Each iteration of this algorithm involves another run through the estimation

loop to obtain a set of weighted relative errors  $(E_k = \frac{D1_{kk}}{t} \int_0^t [z_k(t) - y_k(t)]^2 dt)$ .

The algorithm is designed to find a D1 matrix that results in the weighted error being approximately 1 on each signal being used (as indicated by a nonzero initial estimate of the corresponding D1 element). The motivation for this procedure is discussed in reference 3. The revised estimate of each diagonal element of the D1 matrix is then produced by multiplying the previous estimate by a factor that depends on the previous weighted error of that signal,  $E_k$ , and a relaxation factor,

D1RLX. If  $E_k \geq 1$ , the factor is  $\frac{1}{(E_k - 1)D1RLX + 1}$ ; and if  $E_k < 1$ , the factor is  $\left(\frac{1}{E_k} - 1\right)D1RLX + 1$ . The variable D1TOL will stop this process if the process has converged before ND1 iterations. If, after any iteration, none of the weighted errors are greater than D1TOL or less than  $\frac{1}{D1TOL}$ , a final iteration will be run, and the process will be stopped. The parameter WMAPR (item (52)) will be set to 0 if this option is used, regardless of the MMLE program's input value. If plotting was specified (item (12)), only the time history using the final D1 vector will be plotted. If both the D1 vector determination and the *a priori* variation (item (53)) are activated, the D1 vector will be determined first, and the *a priori* variation will use the final D1 matrix. Default values used are ND1 = 0, D1RLX = 1.2, and D1TOL = 1.4.

Items (52) and (53) are related to the *a priori* feature.

(52) WMAPR — overall weighting factor for *a priori* information. Each element in the *a priori* weighting matrices APRA and APRB (see matrix input section) is multiplied by WMAPR before use. A value of 0 implies that the *a priori* feature is not used in the estimation process. Default value of 0 is used.

(53) NAPR, WFAC — parameters that control *a priori* variation option which puts the program into a different mode. If the *a priori* feature is used, a set of *a priori* weighting matrices should be selected at the beginning of the flight program for each aircraft analyzed. In determining the best weighting matrices to use, it is useful to run the same case with several values of WMAPR (item (52)). Reference 3 describes this process. The option to vary the value of WMAPR is activated if NAPR is greater than 0. The program then runs the entire case a total of NAPR times with different values of WMAPR. The first run is with WMAPR = 0, and the second run is with the value specified for WMAPR by item (52) (if 0 was specified, 0.001 is used instead). For each subsequent run, the value of WMAPR used is WFAC times the value used on the previous run. Time history plots are never produced when this option is used; instead, if PLOTEM = T (item (12)), the final estimates of each of the derivatives are plotted versus WMAPR on a logarithmic scale. The *a priori* estimates, which may be considered as the estimates obtained as WMAPR approaches infinity, are also plotted to the right of the other estimates. These plots may then be used as described in references 3 and 8 to estimate the best values to use for the *a priori* weightings. For these plots to be correct, the NAMELIST variable PUNCH (item (24)) must equal F, because of the order in which the computations are performed. Default values of WFAC = 100. and NAPR = 0 are used.

*Time cards.* — For each of the NCASE (NAMELIST item (5)) time segments to be included, one time card is required. The time cards contain the start and end times for the segment expressed as hours, minutes, seconds, and milliseconds in the format (2(3I2,I3,1X)). The program starts the segment at the first time point greater than or equal to the start time and stops it at the last point less than or equal to the stop time.

*Matrix input.* — Several input matrices are read next in a standard matrix input format. The matrices may be read in any order. Only the A and B matrices must be read in; the others may be read in if the default values are to be changed.



A matrix (4 by 4): The A matrix is the starting estimate of the stability matrix. For a longitudinal three-degree-of-freedom case it should be:

$$\begin{bmatrix} Z_{\alpha} & 1. & Z_V & -\sin(\theta) \cos(\varphi) \frac{g}{V} \\ M_{\alpha} & M_q & M_V & 0. \\ X_{\alpha} & 0. & X_V & -\cos(\theta)g \\ 0. & \cos(\varphi) & 0. & 0. \end{bmatrix}$$

In a two-degree-of-freedom case the third column should be set to 0. For a lateral-directional case the A matrix should be:

$$\begin{bmatrix} Y_{\beta} & \sin(\alpha) & -\cos(\alpha) & \cos(\varphi) \cos(\theta) \frac{g}{V} \\ L_{\beta} & L_p & L_r & 0. \\ N_{\beta} & N_p & N_r & 0. \\ 0. & 1. & \cos(\varphi) \tan(\theta) & 0. \end{bmatrix}$$

Average values of  $\alpha$ ,  $\theta$ ,  $\varphi$ , and  $V$  are used in these matrices.

B matrix (4 by 5 to 4 by 8): The B matrix is the starting estimate of the control matrix. The first four columns are for the control derivatives; the fifth column contains aerodynamic biases (treated as control derivatives, in which the control is defined as a constant value of 1 radian). Usually, only these five columns are required. If NCASE is greater than 1, independent aerodynamic biases may be determined for up to the first four maneuvers when necessitated by trim changes or other factors. In this event, the fifth column's aerodynamic biases are included in every maneuver, the sixth column's biases are included in all maneuvers after the first, the seventh column's biases are included in all maneuvers after the second, and the eighth column's biases are included in all maneuvers after the third. Thus the total aerodynamic bias on the first maneuver would be in column 5; for the bias on the second maneuver, columns 5 and 6 would be added; for the third maneuver, columns 5, 6, and 7 would be added; and for the fourth and all subsequent maneuvers, columns 5, 6, 7, and 8 would be added. For a lateral-directional case the B matrix should then be:

$$\begin{bmatrix} Y_{\delta_a} & Y_{\delta_r} & Y_{\delta_1} & Y_{\delta_2} & Y_0 & Y_{0_2} & Y_{0_3} & Y_{0_4} \\ L_{\delta_a} & L_{\delta_r} & L_{\delta_1} & L_{\delta_2} & L_0 & L_{0_2} & L_{0_3} & L_{0_4} \\ N_{\delta_a} & N_{\delta_r} & N_{\delta_1} & N_{\delta_2} & N_0 & N_{0_2} & N_{0_3} & N_{0_4} \\ 0. & 0. & 0. & 0. & \dot{\varphi}_0 & \dot{\varphi}_{0_2} & \dot{\varphi}_{0_3} & \dot{\varphi}_{0_4} \end{bmatrix}$$

For a longitudinal case the B matrix would be:

$$\begin{bmatrix} Z_{\delta_e} & Z_{\delta_c} & Z_{\delta_1} & Z_{\delta_2} & Z_0 & Z_{0_2} & Z_{0_3} & Z_{0_4} \\ M_{\delta_e} & M_{\delta_c} & M_{\delta_1} & M_{\delta_2} & M_0 & M_{0_2} & M_{0_3} & M_{0_4} \\ X_{\delta_e} & X_{\delta_c} & X_{\delta_1} & X_{\delta_2} & X_0 & X_{0_2} & X_{0_3} & X_{0_4} \\ 0. & 0. & 0. & 0. & \dot{\theta}_0 & \dot{\theta}_{0_2} & \dot{\theta}_{0_3} & \dot{\theta}_{0_4} \end{bmatrix}$$

AA array (4 by 4): The AA array defines which elements in the A matrix are to be determined by the program. Each element in the AA array should be either 1. or 0.. A 1. implies that the corresponding element in the A matrix will be estimated by the program, whereas a 0. implies that it will be held fixed at the starting value. If not read in, the AA array has the following default:

Longitudinal –

$$\begin{bmatrix} 1. & 0. & 0. & 0. \\ 1. & 1. & 0. & 0. \\ 0. & 0. & 0. & 0. \\ 0. & 0. & 0. & 0. \end{bmatrix}$$

Lateral-directional –

$$\begin{bmatrix} 1. & 1. & 0. & 0. \\ 1. & 1. & 1. & 0. \\ 1. & 1. & 1. & 0. \\ 0. & 0. & 0. & 0. \end{bmatrix}$$

BB array (4 by 5 to 4 by 8): The BB array defines which elements in the B matrix are to be determined in the same manner as the AA array defines those in the A matrix. If not read in, the BB array defaults to:

Longitudinal –

$$\begin{bmatrix} 1. & 0. & 0. & 0. & 1. \\ 1. & 0. & 0. & 0. & 1. \\ 0. & 0. & 0. & 0. & 0. \\ 0. & 0. & 0. & 0. & 1. \end{bmatrix}$$

Lateral-directional –

$$\begin{bmatrix} 1. & 1. & 0. & 0. & 1. \\ 1. & 1. & 0. & 0. & 1. \\ 1. & 1. & 0. & 0. & 1. \\ 0. & 0. & 0. & 0. & 1. \end{bmatrix}$$

AR matrix (4 by 4): The AR matrix is the *a priori* stability matrix and contains the *a priori* value of the A matrix. If the *a priori* feature is used, the estimates are weighted toward the AR matrix values. In general, the *a priori* values and the starting values are the same, but it is possible to distinguish between them. If not read in, the AR matrix is set equal to the A matrix.

BR matrix (4 by 5 to 4 by 8): The BR matrix is the *a priori* control matrix and plays a role similar to that of the AR matrix. If not read in, it is set equal to the B matrix.

APRA matrix (4 by 4): The APRA matrix contains *a priori* weightings for the stability matrix and contains the weightings to be assigned to the elements of the AR matrix for the *a priori* option. The program multiplies each relevant element in the APRA matrix by the overall weighting factor, WMAPR (NAMELIST item (52)), and assigns it an appropriate diagonal location in the D2 matrix (eq. (13)). No provision is made for the input of off-diagonal elements of the D2 matrix, although they are provided for in the algorithm. If not read in, the APRA matrix defaults to:

Longitudinal –

$$\begin{bmatrix} 13000. & 0. & 0. & 0. \\ 15. & 800. & 0. & 0. \\ 0. & 0. & 0. & 0. \\ 0. & 0. & 0. & 0. \end{bmatrix}$$

Lateral-directional –

$$\begin{bmatrix} 13000. & 13000. & 13000. & 0. \\ 0.15 & 500. & 5. & 0. \\ 15. & 800. & 800. & 0. \\ 0. & 0. & 0. & 0. \end{bmatrix}$$

APRB matrix (4 by 5 to 4 by 8): The APRB matrix contains *a priori* weightings for the control matrix and plays a role analogous to that of the APRA matrix. If not read in, the APRB matrix defaults to:

Longitudinal –

$$\begin{bmatrix} 13000. & 13000. & 13000. & 13000. & 0. & 0. & 0. & 0. \\ 15. & 15. & 15. & 15. & 0. & 0. & 0. & 0. \\ 0. & 0. & 0. & 0. & 0. & 0. & 0. & 0. \\ 0. & 0. & 0. & 0. & 0. & 0. & 0. & 0. \end{bmatrix}$$

Lateral-directional –

$$\begin{bmatrix} 13000. & 13000. & 13000. & 13000. & 0. & 0. & 0. & 0. \\ 0.15 & 0.15 & 0.15 & 0.15 & 0. & 0. & 0. & 0. \\ 15. & 15. & 15. & 15. & 0. & 0. & 0. & 0. \\ 0. & 0. & 0. & 0. & 0. & 0. & 0. & 0. \end{bmatrix}$$

AP array (3 by 4): The AP array is used in the formation of the observation matrix G of equation (2). For the aircraft identification problem, the observations generally available are either elements of the state vector, their derivatives, or accelerations. If only states and their derivatives are available, the G matrix would be identical to the A matrix. When accelerations are also of interest, the G matrix may still be expressed as a simple function of the A matrix; this function

is specified by the AP array. For example, consider the two-degree-of-freedom longitudinal case:

$$\dot{a} = Z_{\alpha} \alpha + q - \frac{g}{V} \cos(\varphi) \sin(\theta) \theta + Z_{\delta_e} \delta_e + \left( Z_0 + \frac{g}{V} \cos \varphi \cos \theta \right) \quad (25)$$

$$(a_n - a_{n_{bias}}) = -\frac{V}{g} Z_{\alpha} \alpha + 0q - 0\theta + \left( -\frac{V}{g} \right) Z_{\delta_e} \delta_e - \frac{V}{g} \left[ Z_0 + \frac{g}{V} \cos \varphi \cos(\theta) \right] \quad (26)$$

where

$$a_{n_{bias}} = -\cos \varphi \cos \theta + a_{n_{instrument\ bias}}$$

From this example it can be seen that  $(a_n - a_{n_{bias}})$  can be computed like  $\dot{a}$  if appropriate terms are simply multiplied by constant values of  $-\frac{V}{g}$  or 0. Thus each element in the G matrix can be defined as the product of the corresponding element in  $R^{-1}A$  and a constant. These constants form the AP array. This formulation results in a considerable saving of computer time. It should be noted that the accelerometer offsets from the center of gravity (NAMELIST items (39) to (42)) add terms to the G matrix after the basic terms are computed from the AP array. If the AP array is read in, the BP array must also be read in. If not read in, the AP array defaults to the following standard forms:

Longitudinal –

$$\begin{bmatrix} -\frac{V}{g} & 0. & 0. & 0. \\ 1. & 1. & 1. & 1. \\ \frac{1}{g} & 0. & 0. & 0. \end{bmatrix}$$

Lateral-directional –

$$\begin{bmatrix} \frac{V}{g} & 0. & 0. & 0. \\ 1. & 1. & 1. & 1. \\ 1. & 1. & 1. & 1. \end{bmatrix}$$

BP array (3 by 5 to 3 by 8): The BP array plays a role analogous to that of the AP array. It defines the H matrix of equation (2) as a function of the B matrix. Each element in the H matrix is defined as the product of the corresponding elements in  $R^{-1}B$  and the BP array. As in the G matrix, accelerometer offsets from the center of gravity may cause additional terms to be added to the basic H matrix. If either the AP or the BP array is read in, both must be read in. The BP array defaults to:

Longitudinal –

$$\begin{bmatrix} -\frac{V}{g} & -\frac{V}{g} & -\frac{V}{g} & -\frac{V}{g} & -\frac{V}{g} & -\frac{V}{g} & -\frac{V}{g} & -\frac{V}{g} \\ 1. & 1. & 1. & 1. & 1. & 1. & 1. & 1. \\ \frac{1}{g} & \frac{1}{g} & \frac{1}{g} & \frac{1}{g} & \frac{1}{g} & \frac{1}{g} & \frac{1}{g} & \frac{1}{g} \end{bmatrix}$$

Lateral-directional –

$$\begin{bmatrix} \frac{V}{g} & \frac{V}{g} & \frac{V}{g} & \frac{V}{g} & \frac{V}{g} & \frac{V}{g} & \frac{V}{g} & \frac{V}{g} \\ 1. & 1. & 1. & 1. & 1. & 1. & 1. & 1. \\ 1. & 1. & 1. & 1. & 1. & 1. & 1. & 1. \end{bmatrix}$$

R matrix (4 by 4): The R matrix is an acceleration transformation matrix. If not read in, it defaults to the unit matrix for longitudinal cases, or for lateral-directional cases to:

$$\begin{bmatrix} 1. & 0. & 0. & 0. \\ 0. & 1. & -\frac{I_{XZ}}{I_X} & 0. \\ 0. & -\frac{I_{XZ}}{I_Z} & 1. & 0. \\ 0. & 0. & 0. & 1. \end{bmatrix}$$

D1 matrix (5 by 5 to 7 by 7): The D1 matrix is the signal weighting matrix. The diagonal elements are the weightings used for each response signal in the cost functional. The size of this matrix determines the number of signals used in the analysis; therefore, if  $\dot{p}$  and  $\dot{r}$  are not measured for a lateral-directional case, the D1 matrix should be 5 by 5. This reduction will save a significant amount of computer time. If the D1 matrix is diagonal, it should be entered as a vector containing the diagonal elements. The program will then recognize that the matrix is diagonal and take advantage of this in its computations. A vector is indicated by a header card with 0 for the number of columns. The vector is then entered on one card in an 8F10 format. If not read in, the D1 matrix is assumed to be diagonal with the following values:

Longitudinal –

$$[ 30000. \quad 200000. \quad 0. \quad 100000. \quad 2000. ]$$

Lateral –

$$[ 500000. \quad 1500. \quad 1000000. \quad 30000. \quad 5000. ]$$

ENDCASE. – The end of the matrix input is signaled by a card with ENDCASE starting in column 1. If no more cases follow, this card should have simply END instead of ENDCASE.

Card input. – If card input was specified, the input time histories are necessary here. For each time point there should be a record of two cards containing four time words (hours, minutes, seconds, milliseconds), seven observations, four controls, and four extra signals. The order of these quantities is given in NAMELIST item (11). The format is (3I2, I4, 7F10/8F10). Normally, the angular measurements are in degrees, the accelerations in  $g$  units, and the velocities in feet per second.

*Data file input.*— If tape input was specified, the time histories must be on an unformatted data file (either tape or disk). The device number of this file should be specified as 4 by the control cards. This file by default has 4 time words plus 15 data words per record, as in the card input. The length of the records on this file and the order of the parameters (except for the time words) may be changed by the use of the NREC and ORDER parameters (NAMELIST items (9) and (10)); alternatively, the file may be specified to be in the special BOTH form (NAMELIST item (11)). Normally, the angular measurements are in degrees, the accelerations in  $g$  units, and the velocities in feet per second.

## Output Description

Three basic forms of output are available from the MMLE program: printed, plotted (time history or derivative plots), and punched card.

*Printed output.*— The three levels of printed output are controlled by the parameters PRINT and TEST (NAMELIST items (19) and (20)). The basic output is always printed. If PRINT = T, measured and final computed time histories are also printed. If, in addition, TEST = T, time histories in radians, the transition matrices, and the first and second gradients of  $J$  are printed every iteration. The TEST parameter is generally used only for program debugging.

Appendix B presents a listing for a sample case with only the basic output. The first page (p. 112) of the output listing summarizes the input options chosen, and the second page lists the matrices read in. The dimensional and nondimensional starting values are then summarized. An asterisk indicates the values held fixed; the other values are to be determined as unknowns in the program. Each iteration includes a printout of the revised A and B matrices, the integral squared error on each input signal, the weighted errors on each signal, and the total error sum. This iterative loop may terminate in three ways. If the error sum exceeds ERRMAX (NAMELIST item (22)) at any time, the iteration will stop immediately and the input time history will be printed (not included in appendix B). If the maximum number of iterations is reached or the process converges within the range defined by BOUND (NAMELIST item (23)), normal termination will occur. The message "ITERATION TERMINATED, ERROR WITHIN .00100 BOUND" indicates that the convergence bound caused termination in the sample case.

Confidence levels in dimensional and nondimensional form are listed next. These confidence levels are analogous to the standard deviation. Their magnitude indicates the relative confidence to be placed in estimates of the same coefficient from different maneuvers. A small confidence level for a particular derivative estimate indicates that the estimate of the derivative should be very good. Confidence levels are useful in fairing estimated derivative values.

The final page (p. 117) of the first case is a summary of the converged values. The final dimensional and nondimensional derivatives are printed in the same format as the starting values, followed by the final A and B matrices. The final integral squared errors, weighted errors, and total error sum are printed, followed by a summary of the convergence of the error sum.

If either the D1 determination option (NAMELIST item (51)) or the *a priori* variation option (NAMELIST item (53)) is activated, the program prints an appropriate message at this point and begins its second pass through the estimation loop. The output resumes from the top of the third page. This output pattern would be repeated as many times as specified by the option. If more cases follow, the same output pattern is repeated for each case.

*Plotted output.*— If plotting is invoked (NAMELIST item (12)), time history plots like those in appendix B will be produced. On the observation signals, the solid lines represent the flight data and the dotted lines are the computed fits. When plotting is invoked and the *a priori* variation option (NAMELIST item (53)) is being used, time history plots are not produced, but, instead, the derivative plots discussed under that option (not included in appendix B).

*Punched card output.*— If PUNCH = T (NAMELIST item (24)), the nondimensional A and B matrices and confidence levels are punched on cards. These cards are preceded by a header card which contains the characters LATR or LONG followed by the first 35 characters of the title card and the values of MACH, ALPHA, PARAM, and CG. These cards are in the exact format required for the SUMARY plotting program. If the case is longitudinal, a computed  $\delta_{e_{trim}}$  appears in the matrix location for  $C_{m_0}$ , and  $C_Z$  appears in the location for  $C_{Z_0}$ . These quantities are of more interest in this form, although the confidence levels are not readily available. (The confidence levels punched are those for the original  $C_{m_0}$  and  $C_{Z_0}$ .) The equations used to compute these parameters are:

$$\delta_{e_{trim}} = \frac{(C_m + C_{m_0})}{C_{m_{\delta_e}}} \quad (27)$$

$$C_Z = C_{Z_0} + C_{Z_\alpha} \alpha + C_{Z_{\delta_e}} \delta_{e_{trim}} - \cos(\theta) \cos(\varphi) \frac{W}{qS} \quad (28)$$

These equations are valid only for a two-degree-of-freedom case with no lateral-directional cross-coupling terms.

The final dimensional A and B matrices may be output on punched cards if PUNCHD = T (NAMELIST item (25)) is specified. These matrices may be used if it is desired to restart a case from the final values and run additional iterations. If the *a priori* feature is used in the restart, the original A and B matrices should be relabeled AR and BR and inserted (see discussion of AR and BR matrices, pp. 20-21) because the *a priori* values would be different from the new starting values. Any variable bias from the original run should also be subtracted from the data using FIXED (NAMELIST item (7)) in order to start at the same values as the final iteration of the previous run.

## SETUP — PREPROCESSING PROGRAM

One of the most time-consuming portions of the analysis of aircraft stability and control derivatives is the preparation of input data for the derivative estimation program. The preprocessing program, SETUP, automates much of this work and is a key element in the routine processing of a large number of cases. It can produce, at the user's option, the data file and the punched input deck for the MMLE program. Listings of the program and its subroutines are presented in appendix C. A sample case is included in appendix D.

The SETUP program reads a set of predicted derivatives to be interpolated and dimensionalized for the given flight condition. The flight condition may be specified by the user, or if appropriate data were recorded on a flight tape, the program can obtain the flight condition automatically, given only the start and stop times for the case.

When the program is used in the most automated manner, the only inputs required for each case are the start and stop times, the type of case (longitudinal or lateral-directional), and an indication of which controls were used for the particular maneuver if more than one control is relevant. Using the program in this manner requires some preparation, but only at the beginning of the flight program rather than for each case. This distinction is important when several hundred cases are being analyzed, as has been done on several aircraft.

In preparation for the most automated use of the SETUP program, the user must write four small FORTRAN subroutines. Subroutine TAPEIN reads a flight data tape, finds the time interval requested, and places the data and times from the data into two arrays. The sample included in appendix D reads an unformatted tape with time in the first four words. Subroutine RDSET provides any initialization needed for TAPEIN; in the sample case it reads the number of channels on the input tape and the channel numbers of the data needed. Subroutine COND obtains the flight condition if it is to be computed automatically instead of read in manually. The averages of each of the data channels read in are available for use in this subroutine, and the subroutine can compute the required parameters from these averages. The sample obtains ALPHA, THETA, PHI, DETRIM, Q, V, and MACH from the data channel averages. The subroutine will also compute Q and V from knots indicated airspeed and altitude, if preferred. Weight, inertia, and center of gravity are not computed in the example subroutine, although they may be computed in user-supplied versions. Subroutine COND1 reads in any data needed in subroutine COND, for instance, tables of inertia versus fuel weight. This subroutine, as given in appendix C, is a null subroutine.

### Input Description

The input data and the case specifications are described in the following sections.

*Options.*— The options to be used are specified by the following cards. All the options begin in column 1. The cards may appear in any order (except for the START card, as noted). Only the first four characters of each card are checked.



WRITE TAPE — instructs the program to write a data file for the MMLE program. This option automatically invokes the READ TAPE option.

PUNCH DECK — instructs the program to punch a data deck for the MMLE program.

READ TAPE — instructs the program to read an input tape. This option might be specified if input tape data are needed to determine the flight condition for the punched data card deck. This instruction is redundant if WRITE TAPE was specified.

START — signals the end of the options and the start of processing. This card must be the last card in the options section.

*Vehicle characteristics.*— The input segment that starts here and ends at, but does not include, *User-supplied data* (p. 30) is required if PUNCH DECK was specified in the preceding options. If PUNCH DECK was not specified, this segment must not be included.

NAMelist/WIND/: The following parameters may be input in NAMelist format:

(1) NABP — number of angle-of-attack breakpoints for predicted derivatives. Default value of 1 is used.

(2) NMBP — number of Mach number breakpoints for predicted derivatives. Default value of 1 is used.

(3) NBP — number of sets of predicted derivatives. Each set is identified subsequently as either lateral-directional or longitudinal and as having a particular value of the extra identifying parameter PARAM (used if the data are to be separated by some other criterion, such as wing sweep or flap position). Thus if there is one longitudinal and one lateral-directional data set and no additional distinction is made, NBP = 2. Dimensions in the program restrict the value of NBP to less than or equal to 8. Default value of 1 is used.

(4) LATR, LONG—(eight-word logical vectors) — parameters that specify dynamic modes of the predicted derivatives. The type of each set of predicted derivatives should be specified by setting the corresponding element of either LATR or LONG to true. Only one of the variables can be set to true in the NAMelist. Default type for each set is longitudinal.

(5) NCLA, NCLO — number of coefficients per lateral-directional and longitudinal data set, respectively.

(6) CGLA, CGLO — reference center of gravity for lateral-directional and longitudinal predicted derivatives in fraction of reference chord. Default value of 0.25 is used.

(7) MZLA, MZLO — number of signals for the MMLE program to analyze in lateral-directional and longitudinal cases (that is, the length of the D1 vector; see D1 matrix description, p. 23). The values must be between 5 and 7, inclusive. Default value of 5 is used.

(8) WMLA, WMLO – overall *a priori* weighting for lateral-directional and longitudinal cases (WMAPR in MMLE program). If WMLA or WMLO are not entered, the SETUP program will not read the appropriate APRA and APRB matrices discussed subsequently and will use a weighting of 0. If WMLA or WMLO are set to 0, the corresponding APRA and APRB matrices will be read by the SETUP program and punched with the MMLE program card deck, although the weighting on the matrices will still be 0. If WMLA or WMLO is set to a positive value, the APRA and APRB matrices will be read and punched normally. If WMLA or WMLO is set to a negative value, the APRA and APRB matrices will not be read and the absolute value of WMLA or WMLO will be passed to the MMLE program (using the MMLE program's defaults for the APRA and APRB matrices). In all these cases, the lateral-directional usage and longitudinal usage are independent.

(9) DEG, RAD-(logical) – parameters that specify degrees or radians for units of predicted derivatives by setting either DEG = T or RAD = T. Only one of the two variables can be set to true in the NAMELIST. The rotary derivatives are per radian regardless of this option. Default condition is DEG = T.

(10) METRIC-(logical) – parameter that specifies SI (MKS) units if true and U.S. Customary (EGS) units if false. All input data units must be consistent with the system specified. Default condition is F.

(11) BODY, STAB-(logical) – parameters that specify axis system of longitudinal predicted derivatives as body or stability. Only one of the two variables can be set to true in the NAMELIST. (Lateral-directional data are in the body axes system independent of this option.) Default condition is STAB = T.

(12) S – value of reference wing area ( $\text{ft}^2$  or  $\text{m}^2$ ).

(13) SPAN – value of reference wing span (ft or m).

(14) CBAR – value of reference wing chord (ft or m).

(15) SPS – samples per second for data file. If not specified, 0 is passed to the MMLE program which then, by default, determines SPS from the times on the data file.

(16) PUNCH-(logical) – option passed to the MMLE program to control its PUNCH (MMLE NAMELIST item (24)) option to punch cards with final estimates of the nondimensional derivatives and confidence levels. Default condition is F.

(17) XB, XALF, ZB, XAY, ZAY, XAN, ZAX – instrument locations relative to the center of gravity. The meaning of each of these parameters is the same as that given in items (36) to (42) of the MMLE NAMELIST except that, as used here, these values refer to the reference center of gravity for the predicted derivatives instead of the flight center of gravity. If 0 is entered, it is assumed that the signals have been corrected to the flight center of gravity, and no additional correction terms will be used. Default value of 0 is used.

Vehicle name: The vehicle name is specified by up to eight characters, starting in column 1. These eight characters will be used on the title card punched out for

the MMLE deck and will be included on the first line of the output from the SETUP program.

**Lateral-directional weighting matrix:** The lateral-directional D1 matrix is read in as a vector on one card in a 7F10 format. This vector is omitted if no lateral-directional predicted derivatives are read in. If every element is 0, the default in the MMLE program will be used.

**Longitudinal weighting matrix:** The longitudinal D1 matrix is read in as a vector. The comments for the lateral-directional D1 vector apply.

**Lateral-directional APRA and APRB matrices:** The APRA and APRB matrices for lateral-directional cases are in standard matrix input format. As mentioned above, these matrices are omitted if the WMLA parameter was not read in or was set to a negative value.

**Longitudinal APRA and APRB matrices:** The APRA and APRB matrices for longitudinal cases are in standard matrix format. The matrices are omitted if the WMLO parameter was not specified or was negative.

**Predicted derivatives:** NBP sets of predicted derivatives are required in the order specified in item (4) of SETUP NAMELIST/WIND/. Each set consists of data for NCLA or NCLO coefficients, depending on whether the set is lateral-directional or longitudinal. The data for each coefficient may be read as a function of Mach number and angle of attack, or as a function of Mach number only in the following forms.

The data for each coefficient begin with a header card containing the coefficient name in the first four columns and either a 1 or a 2 in column 10; a 1 indicates that the coefficient is a function of Mach number only, a 2 indicates that it is a function of Mach number and angle of attack. The only acceptable coefficient names are: lateral-directional – CYB, CLB, CNB, CLP, CNP, CLR, CNR, CYDA, CLDA, CNDA, CYDR, CLDR, CNDR, CYD1, CLD1, CND1, CYD2, CLD2, CND2; longitudinal (body axes) – CNA, CMA, CAA, CMQ, CNV, CMV, CAV, CNDE, CMDE, CADE, CNDC, CMDC, CADC, CND1, CMD1, CAD1, CND2, CMD2, CAD2, CN, CA; longitudinal (stability axes) – CLA, CMA, CDA, CMQ, CLV, CMV, CDV, CLDE, CMDE, CDDE, CLDC, CMDC, CDDC, CLD1, CMD1, CDD1, CLD2, CMD2, CDD2, CL, CD. The first two characters of each name indicate the force or moment coefficients (for lateral-directional, CY = side force, CL = rolling moment, and CN = yawing moment; for longitudinal, CL = lift force, CD = drag force, CN = normal force, CA = longitudinal force (positive direction is rearward)), and the remaining characters indicate the quantity with respect to which the derivative is taken. (A ~ angle of attack, B ~ angle of sideslip, P, Q, R ~ angular rates, V ~ velocity, DE, DC, DA, DR, D1, and D2 ~ controls.)

If the coefficient is a function of Mach number and angle of attack, the data for each Mach number appear on a separate card, with each card containing the values of the coefficient for the NABP angle-of-attack breakpoints. These cards are in an 8F10 format, and the card entries may be continued on additional cards if needed.

If the coefficient is a function of Mach number only, the values for the NMBP Mach number breakpoints appear on one card in an 8F10 format. As before, this card may be continued if needed.

Angle-of-attack breakpoints: A card containing the NABP values of the angle-of-attack breakpoints in an 8F10 format is necessary. If NABP = 1, this card may be blank.

Mach number breakpoints: A card containing the NMBP values of the Mach number breakpoints in an 8F10 format is necessary. If NMBP = 1, this card may be blank.

Arbitrary parameter breakpoints: A card containing the NBP values of PARAM to distinguish the predicted derivative data sets is necessary. If no distinction other than longitudinal and lateral-directional is used, this card may be blank. The card is in an 8F10 format.

*User-supplied data for subroutine COND1.*— Any input required for subroutine COND1 goes in the input data at this point. With the subroutine supplied, there is none.

*Input tape data.*— The input tape data section should be omitted if the READ TAPE option is not active. Any input required by subroutine RDSET is made here. The subroutine supplied requires a card with the number of data words per record of the input tape; this card is in an I5 format. This is followed by three cards containing the channel numbers of the 40 channels to be used; each of these cards is in a 16I5 format. A 0 indicates a signal not used. The first 25 signals will be put on the MMLE program tape if a tape is written. (The signals should be in the BOTH order defined by item (11) in the MMLE NAMELIST.) The last 15 of the 40 channels are reserved for use in subroutine COND, should they be needed. These last 15 channels are typically used for fuel weight, flap position, or any other quantities useful in identifying the flight condition and vehicle configuration. The SETUP program automatically averages the values of all 40 data channels over the requested time interval and passes these averages to subroutine COND through a labeled common block.

*Case specification.*— The case specification is repeated as many times as necessary, once for each case to be analyzed.

Time card: The start time and end time for the case in hours, minutes, seconds, and milliseconds are required. The format is 2(3I2,I3,1X).

NAMELIST/COND/: The following parameters may be read in NAMELIST/COND/:

(1) LONG, LATR-(logical) — type of case to be analyzed. Set either LONG or LATR to true. Only one of the two variables can be set to true in the NAMELIST.

(2) CASE-(integer) — case number. Default value of 0 is used.

(3) DELTA-(four-word logical vector) – option that specifies which controls were used in the maneuver. A value of T for any element of DELTA indicates that the corresponding control was used. If all four locations are F (default condition), the MMLE program default is used; this default is  $\delta_e$  for longitudinal cases,  $\delta_a$  and  $\delta_r$  for lateral-directional cases. If DELTA is omitted in a case but has been specified in a previous case of the same type (longitudinal or lateral-directional), it will assume the values of the previous case.

(4) FLT-(integer) – flight number. This identification is needed only on the first case.

All the following items may be set in subroutine COND instead of reading them in at this point. The subroutine supplied will set ALPHA, THETA, PHI, DETRIM, Q, V, and MACH if the READ TAPE option is active.

(5) ALPHA – average angle of attack.

(6) THETA – average pitch attitude. Default value of 0 is used.

(7) PHI – average roll attitude. Default value of 0 is used.

(8) Q – average dynamic pressure.

(9) V – average velocity.

(10) MACH-(real) – average Mach number.

(11) PARAM – extra identifying parameter. If nonzero, the predicted derivative data with the same value of PARAM will be used for the derivatives. If there is only one longitudinal data set or one lateral-directional data set, or a longitudinal and a lateral-directional data set, PARAM need not be specified. Default value of 0 is used.

(12) W – aircraft weight (pounds or newtons).

(13) IX, IY, IZ-(real) – moments of inertia (slug-ft<sup>2</sup> or kg-m<sup>2</sup>).

(14) IXZ-(real) – cross-product of inertia (slug-ft<sup>2</sup> or kg-m<sup>2</sup>). Default value of 0 is used.

(15) CG – center of gravity in fraction of chord. Default is the predicted derivative reference value.

(16) DETRIM – trimmed value of  $\delta_e$ . Default value of 0 is used.

Items (17) and (18) are simply for convenience if  $\bar{q}$  and V are not readily available. The subroutine COND supplied may compute  $\bar{q}$  and V from the values of indicated airspeed and altitude, using an approximation to the standard atmosphere.

(17) KIAS-(real) — knots indicated airspeed. If KIAS is nonzero,  $\bar{q}$  and  $V$  will be computed. Default value of 0 is used.

(18) ALT — altitude (ft or m). Default value of 0 is used.

End card: The last card in the data deck contains a -1 in the first two columns to indicate the end of the data.

### Output Description

The two primary outputs of the SETUP program are the MMLE program data tape and the punched card deck. These outputs are described in the MMLE Input Description section. A permanent disk file may be substituted for the data tape, without modifying the program. The punched card deck from SETUP will be ready to run through the MMLE program with the addition of control cards and the substitution of an END card for the last ENDCASE card at the end of the deck.

The printed output includes the predicted derivatives. For each case the data channel averages as passed to subroutine COND are printed if an input tape was read. All matrices punched in the MMLE program card deck are also printed for easy reference. A sample case is presented in appendix D.

### SUMARY — PLOTTING PROGRAM

Data presentation can be a time-consuming portion of the derivative estimation process when a large number of maneuvers are involved. It is still common to laboriously plot derivatives and wind-tunnel data by hand, a procedure which can easily take longer than the entire estimation process. To efficiently utilize available manpower, graphs or data listings should be automatically produced. The SUMARY program produces plots of estimated derivatives and confidence levels as a function of angle of attack and, if desired, provides predicted derivative values for comparison. The program is presented as a prepared package that may be modified to meet users' specific data presentation requirements. Listings of the program and its subroutines are presented in appendix E. A sample case is given in appendix F.

The SUMARY program reads a set of predicted and flight-determined derivatives, and plots specific groups of the data as instructed. Several groups may appear on one plot, indicated by different symbols. The same predicted derivative card deck used for the SETUP program may be used in the SUMARY program, or predicted derivatives may be omitted. The flight-determined derivatives are punched out by the MMLE program in the exact format required for the SUMARY program.

### Input Description

*Title card.*— The title card contains any information needed to identify a particular set of data that is appropriate to include in the printed output. All 80 columns on this card may be used.

NAMelist/WIND/. — Parameters in NAMelist/WIND/ are as follows:

- (1) NABP — number of angle-of-attack breakpoints for predicted derivatives. Default value of 1 is used.
- (2) NMBP — number of Mach number breakpoints for predicted derivatives. Default value of 1 is used.
- (3) NBP — number of sets of predicted derivatives. The definition of a set of predicted derivatives is the same as that in the SETUP program. Default value of 1 is used.
- (4) LONG, LATR-(eight-word logical vectors) — types of each set of predicted derivatives. The type is specified by setting corresponding element of either LONG or LATR to true. Only one of the two variables can be set to true in the NAMelist. Default type for each set is longitudinal.
- (5) NCLA, NCLO — number of coefficients in lateral-directional and longitudinal data sets, respectively. Default value of 0 is used.
- (6) CGLA, CGLO — reference centers of gravity for lateral-directional and longitudinal predicted derivatives in fraction of chord. Default value of 0.25 is used.
- (7) SHIFT-(logical) — parameter that corrects data for center-of-gravity location. If true, the flight  $C_{m_\alpha}$  and  $C_{n_\beta}$  will be corrected to the predicted derivative reference center of gravity. Default condition is F.
- (8) DEG, RAD-(logical) — options that specify degrees or radians for units of predicted derivatives. Only one of the two variables can be set to true in the NAMelist. Rotary derivatives are per radian regardless of this option. Default units are degrees.
- (9) BODY, STAB-(logical) — options that specify body or stability axes for input of predicted derivatives. If STAB = T, longitudinal predicted derivatives are converted from stability to body axes. If BODY = T, no conversion is made. Only one of the two variables can be set to true in the NAMelist. Default condition is STAB = T.
- (10) PRINT-(logical) — option that prints out predicted derivatives, if true. Default condition is F.
- (11) WTPLOT-(logical) — option that plots predicted derivatives, if true. Default condition is T.
- (12) CBAR, SPAN — aircraft reference chord and span, respectively. These quantities are needed only if SHIFT = T and there are lateral-directional data. Default values of CBAR = 0 and SPAN = 10<sup>50</sup> are used.
- (13) AMIN, AMAX — minimum and maximum for values on angle-of-attack axis. Default values of AMIN = 0 and AMAX = 12. are used.

(14) ASCALE — scale for angle-of-attack axis in degrees per centimeter. Default value of 1. is used.

(15) YLEN — length of ordinate axis in centimeters. Default value of 10. is used.

(16) XDIST — X-distance between plots in centimeters. Default value of 10. is used.

(17) CRFACT — factor by which confidence levels are multiplied before plotting. If equal to 0, no confidence levels are plotted. Default value of 1. is used.

(18) NPARAM — variable which distinguishes the two modes of data organization to be used. If NPARAM = 0, flight data points are sorted by Mach number to the nearest Mach number breakpoint. Plots are then produced with the different Mach numbers indicated by different symbols. If NPARAM > 0, Mach number is ignored and the data are sorted by the value of PARAM, the extra identifying parameter, to the nearest PARAM breakpoint. Plots are then produced with different symbols distinguishing these groups. The lowest Mach number of the predicted derivatives is plotted if more than one Mach number breakpoint is specified. Only one predicted derivative curve is plotted. In this case there should be only one set of lateral-directional and one set of longitudinal predicted derivatives; if there is more than one set, only the first will be plotted. Default value of 0 is used.

*Predicted derivatives.*— The NBP sets of predicted derivatives are necessary in exactly the same format required for the SETUP program, including the cards with angle of attack, Mach number, and PARAM breakpoints.

*Flight data.*— The flight data desired are required at this point in the form punched on cards by the MMLE program if PUNCH = T (p. 25).

(1) Header card — TYPE, TITLE, MACH, ALPHA, PARAM, CG in format A4,1X,A35,4F10. TYPE is either LONG or LATR.

(2) A, B, AC, BC matrices in nondimensional form. The AC and BC matrices contain the confidence levels. The fifth column of the B matrix in a longitudinal case should contain  $C_z$  in the first row and  $\delta_{e_{trim}}$  in the second row if they are desired for plotting. These quantities replace the logically expected, but more difficult to interpret, quantities (perturbation  $C_{z_0}$  and  $C_{m_0}$ ) from which they are derived.

*Plotting instructions.*— The end of the flight data and the beginning of the plotting instructions are signaled by a card with PLOT in the first four columns. Then, for each set of plots desired, the following instruction cards are needed:

(1) TYPE, PARM, TOL — TYPE is either LATR or LONG. PARM should equal one of the PARAM breakpoints of the predicted derivatives. The program will then select the corresponding set of predicted derivatives to be used. Flight data points with this same value of PARAM ( $\pm$ TOL) will be selected for plotting. For instance, if PARM = 35. and TOL = 2., a flight point with PARAM = 36. will be plotted, but



a flight point with PARAM = 38. will be rejected. In the special case, PARAM = 0, the first set of predicted derivatives of the correct type (LATR, LONG) is used together with all the flight data. The format of this card is A4,F6,F10.

(2) Up to six cards specifying the derivatives to be plotted and the scales to use. Four plot instructions are included on a card (less may be on the last card). Each plot instruction is of the form DERIV, SMIN, SMAX; DERIV is the derivative name, and SMIN and SMAX are the minimum and maximum values for the ordinate. The valid derivative names are the same as those in the SETUP program for lateral-directional data; for longitudinal data, all the body axis derivative names except CA are valid and the additional name of DE may be used to plot  $\delta_{e_{trim}}$  versus  $\alpha_{trim}$ . If SMIN = SMAX (in particular, if left blank), automatic scaling will be used for the plot. The format of these cards is 4(A4,F6,F10).

*End card.*— The end of the plotting instructions is signaled by a card with END starting in column 1.

### Output Description

The printed output from the SUMMARY program includes the header cards for all flight points read in and a summary of the plotting instructions. The predicted derivatives are printed if PRINT is set to T. In addition, informative messages are provided if no predicted derivatives or flight data are available at a requested condition.

Plots are scaled for centimeter grid paper. Confidence levels are indicated by vertical bars. Predicted derivative data are identified by small symbols that correspond to those in the figure legend, at the beginning and end of each curve. A sample is shown in appendix F.

### CONCLUDING REMARKS

A digital computer program written in FORTRAN IV has been successfully applied by relatively inexperienced personnel to aircraft linear parameter estimation problems with measurement noise but no state noise. This maximum likelihood estimation program includes an option for using *a priori* information and provides estimates of the derivatives and confidence levels. A program to automate the setup work and a program to plot the results have also been written. The three programs form a package which has been used to successfully analyze 1500 maneuvers on 20 aircraft.

*Flight Research Center  
National Aeronautics and Space Administration  
Edwards, Calif., January 22, 1975*

## APPENDIX A

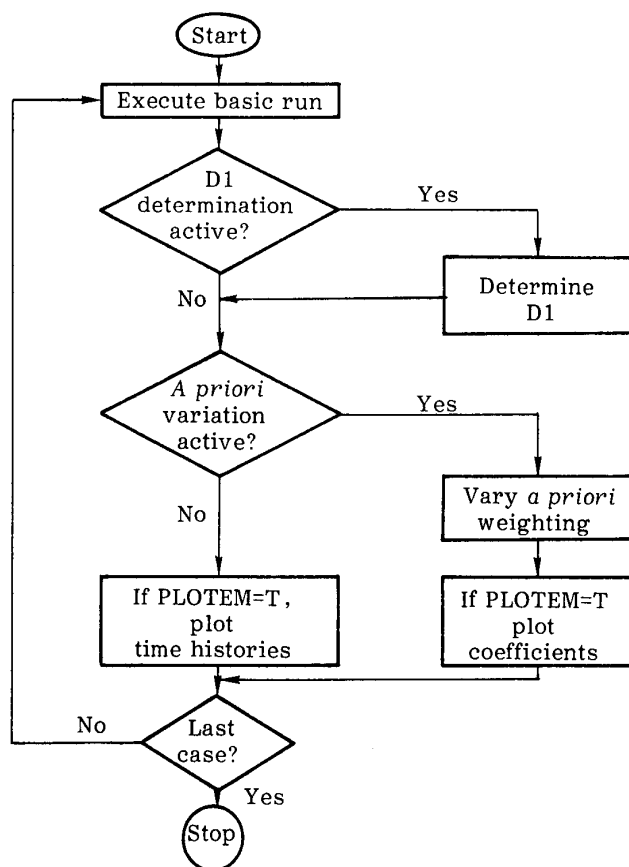
### MMLE PROGRAM AND SUBROUTINES

Listings of the main program and the subroutines used in the MMLE program are presented. The listings are preceded by a brief description, a flow chart, when needed for clarification, and programming notes which explain some of the conventions used and point out items needed to understand the operation of the program.

#### MAIN MMLE PROGRAM

Description: The main MMLE program activates the three operating modes of the program (basic mode, D1 determination mode, and *a priori* variation mode).

Flow chart:



## APPENDIX A — Continued

Programing notes: The PROGRAM card is required on CDC 6000/7000 systems. On an IBM 360/370 system the following DD cards, or equivalent information, are necessary to perform the same function as the PROGRAM card:

```
//GO.FT02F001 DD SYSOUT=B,SPACE=(TRK,10,RLSE),  
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3520)  
//GO.FT03F001 DD SYSOUT=A,SPACE=(TRK,50,RLSE),  
// DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3458)  
//GO.FT04F001 DD DUMMY
```

(Substitute the appropriate DD card for the input file if a tape or disk input is used.)

```
//GO.FT08F001 DD UNIT=SYSDA,DISP=(NEW,DELETE),SPACE=(CYL,(10,2)),  
// DCB=(RECFM=VSB,LRECL=92,BLKSIZE=924),DSN='PLOTTER DATA'  
//GO.FT07F001 DD UNIT=SYSDA,DISP=(NEW,DELETE),SPACE=(CYL,(10,2)),  
// DCB=(RECFM=VSB,LRECL=84,BLKSIZE=844),DSN='INTERNAL'  
//GO.PLOTTAPE DD DUMMY
```

(Substitute the appropriate DD card for the plotter file as used on the particular system. The file name will be either PLOTTAPE or FT13F001, depending on the plotter software used.)

```
//GO.FT01F001 DD*
```

This routine alters PRINT and PLOTEM to suppress any extraneous output during intermediate steps of the D1 determination and the *a priori* variation option.

Important variables —

ND1, NAPR — control the D1 determination and *a priori* variation options as described in MMLE NAMELIST input.

D2 — vector of final weighted relative errors returned from the estimation process.

STORE — storage for final coefficient values during *a priori* variation. It is used to plot these values.

# APPENDIX A – Continued

## Program listing:

PROGRAM MMLE(INPUT,PUNCH,OUTPUT,TAPE4,TAPE7,TAPE8,TAPE13,	MAIN 0
- TAPE1=INPUT,TAPE2=PUNCH,TAPE3=OUTPUT)	MAIN 10
C	MAIN 20
C	MAIN 30
COMMON /ALLOIM/ MAX,MIX	MAIN 40
COMMON /BUF/ BUFFER,YO,THGT	MAIN 50
COMMON /MATRIX/ A,B,AA,BB,AP,BP,D1,RI	MAIN 60
COMMON /COM/ NCASE,MZ,NPTS,NPT,SPS,PRINT,LONG,LATR,PLOTEM,ND1,	MAIN 70
- D1TOL,D1RLX,NAPR,WFAC,WMAPR,ERRSUM,LAST,RATIO	MAIN 80
- DIMENSION NPTS(15),D1(8,7),AHOLD(5,4),	MAIN 90
- BHOLD(5,8),D2(7),A(5,4),B(5,8),AP(4,4),BP(4,8),STORE(14,27)	MAIN 100
- ,BUFFER(1024),RI(5,4)	MAIN 110
- LOGICAL PLOTEM,LONG,LATR,PLT,AA(5,4),BB(5,8),STP,PRINT,PRNT,	MAIN 120
- FIRST,LAST	MAIN 130
FIRST=.TRUE.	MAIN 140
LAST=.FALSE.	MAIN 150
5 REWIND 4	MAIN 160
REWIND 8	MAIN 170
REWIND 7	MAIN 180
CALL EDIT	MAIN 190
IF(ND1.EQ.0.AND.NAPR.LT.1) GO TO 10	MAIN 200
PLT=PLOTEM	MAIN 210
IF(NAPR.GT.0) PLOTEM=.FALSE.	MAIN 220
PRNT=PRINT	MAIN 230
WHOLD=WMAPR	MAIN 240
WMAPR=0.	MAIN 250
MAX=5	MAIN 260
CALL AMAKE(AHOLD,A)	MAIN 270
CALL AMAKE(BHOLD,B)	MAIN 280
C***** BASE RUN	MAIN 290
10 CALL DATA(.TRUE.)	MAIN 300
CALL AGIRL	MAIN 310
IF(ND1.EQ.0) GO TO 15	MAIN 320
PLOTEM=.FALSE.	MAIN 330
PRINT=.FALSE.	MAIN 340
15 CALL OUTPUT(D2)	MAIN 350
IF (ND1.EQ.0) GO TO 100	MAIN 360
C***** D1 DETERMINATION (IF DESIRED)	MAIN 370
TOL=1./D1TOL	MAIN 380
DO 90 I=1,ND1	MAIN 390
STP=.TRUE.	MAIN 400
DO 30 J=1,MZ	MAIN 410
IF(D1 (J,J).NE.0.) GO TO 22	MAIN 420
D2(J)=1.	MAIN 430
GO TO 30	MAIN 440
22 IF(D2(J).GT.D1TOL.OR.D2(J).LT.TCLI) STP=.FALSE.	MAIN 450
IF(D2(J).GT.1.) GO TO 25	MAIN 460
D2(J)=(1./D2(J)-1.)*D1RLX+1.	MAIN 470
GO TO 27	MAIN 480
25 D2(J)=1./((D2(J)-1.)*D1RLX+1.)	MAIN 490
27 D1 (J,J)=D1 (J,J)*D2(J)	MAIN 500
D2(J)=SQRT(D2(J))	MAIN 510
30 CONTINUE	MAIN 520
IF(I.LT.ND1.AND..NOT.STP) GO TO 40	MAIN 530
PLOTEM=PLT	MAIN 540
PRINT=PRNT	MAIN 550
40 WRITE(3,2000)	MAIN 560

# APPENDIX A – Continued

MAX=8	MAIN 570
CALL ASPIT(D1)	MAIN 580
MAX=5	MAIN 590
CALL AMAKE(A,AHOLD)	MAIN 600
CALL AMAKE(B,BHOLD)	MAIN 610
CALL DATA(.FALSE.)	MAIN 620
CALL AGIRL	MAIN 630
CALL OUTPUT(D2)	MAIN 640
IF(STP) GO TO 95	MAIN 650
90 CONTINUE	MAIN 660
95 WRITE(3,2002)	MAIN 670
MAX=8	MAIN 680
CALL ASPIT(D1)	MAIN 690
100 IF(NAPR.GT.0) GO TO 105	MAIN 700
IF(.NOT.PLOTEM) GO TO 200	MAIN 710
CALL THPLOT(FIRST)	MAIN 720
FIRST=.FALSE.	MAIN 730
GO TO 200	MAIN 740
C***** APRIORI VARIATION (IF DESIRED)	MAIN 750
105 PRINT=.FALSE.	MAIN 760
IF(WHOLD.EQ.0.) WHOLD=.001	MAIN 770
WMAPR=WHOLD	MAIN 780
I=0	MAIN 790
110 I=I+1	MAIN 800
JKMM=0	MAIN 810
DO 130 J=1,3	MAIN 820
DO 120 K=1,4	MAIN 830
IF(BB(J,K)) GO TO 120	MAIN 840
JKMM=JKMM+1	MAIN 850
STORE(I,JKMM)=B(J,K)	MAIN 860
120 CONTINUE	MAIN 870
DO 130 K=1,3	MAIN 880
IF(AA(J,K)) GO TO 130	MAIN 890
JKMM=JKMM+1	MAIN 900
STORE(I,JKMM)=A(J,K)	MAIN 910
130 CONTINUE	MAIN 920
STORE(I,JKMM+1)=ERRSUM	MAIN 930
MAX=5	MAIN 940
CALL AMAKE(A,AHOLD)	MAIN 950
CALL AMAKE(B,BHOLD)	MAIN 960
IF(I-NAPR) 140,110,160	MAIN 970
140 WRITE(3,2001)WMAPR	MAIN 980
CALL DATA(.FALSE.)	MAIN 990
CALL AGIRL	MAIN1000
CALL OUTPUT(D2)	MAIN1010
WMAPR=WMAPR*WFAC	MAIN1020
GO TO 110	MAIN1030
160 IF(.NOT.PLT) GO TO 200	MAIN1040
CALL APRPL(STORE,AA,BB,NAPR,WHOLD,WFAC,LONG,FIRST,LAST,RATIO)	MAIN1050
FIRST=.FALSE.	MAIN1060
200 IF(.NOT.LAST) GO TO 5	MAIN1070
IF(.NOT.FIRST) CALL PLOT(0.,0.,999)	MAIN1080
2000 FORMAT(15H001 REVISED TO:)	MAIN1090
2001 FORMAT(12H0WMAPR NOW =,E10.2)	MAIN1100
2002 FORMAT(10H0FINAL D1:)	MAIN1110
STOP	MAIN1120
END	MAIN1130

## APPENDIX A – Continued

### SUBROUTINE EDIT

Description: Subroutine EDIT initializes the program, sets defaults, and reads input options and matrices.

Programing notes: If used with a system that does not support the NAMELIST, some other form of input might be used.

Subroutine MATLD, called at card 1820, sets appropriate elements of ABC to -99999 when reading a matrix. These elements are then tested after all the matrix input has been made to determine what matrix defaults are needed.

The R matrix is inverted at card 2460, since  $R^{-1}$  is the form needed by the rest of the program.

From card 2530 on, the AA and BB matrices are being converted to logical variables and the number of the different types of unknown coefficients to be determined is found. An element in AA or BB is set to false if that element in A or B is to be determined. This may be contrary to the expected convention.

# APPENDIX A — Continued

## Subroutine listing:

	SUBROUTINE EDIT	EDIT 0
C		EDIT 10
C	SETS DEFAULT VALUES AND READS PROGRAM OPTIONS FROM CARDS	EDIT 20
C		EDIT 30
	COMMON /ALLOIM/ MAX,MIX	EDIT 40
	COMMON /TOPLOT/ ZMAX,ZMIN,DCMAX,DCMIN,TIMESC,NCPLLOT	EDIT 50
	COMMON /TOGIRL/JKM,JKMM,JKMM1,ERRMAX,ZEROIN,XT5,BOUND,APR,KI	EDIT 60
-	,VAR,ZERO,APRD,JKV,DIAG	EDIT 70
	COMMON /MATRIX/ A,B,AA,BB,AP,BP,D1,R	EDIT 80
	COMMON /COM/ NCASE,MZ,NPTS,NPTT,SPS,PRINT,LONG,LATR,PLOTEM,ND1,	EDIT 90
-	D1TOL,D1RLX,NAPR,WFAC,WMAFR,ERRSUM,LAST,RATIO	EDIT 100
	COMMON /INFO/ HH,NOITER,MX,MXP1,MU,TEST,XBN,ZBX,IPQR,IXYZ,XT3,MZM,	EDIT 110
-	CORECT,BIASKN,PLTMAX,XT4,ERRVEC,PUNCHO,NEAT	EDIT 120
	COMMON /HEADNG/ LABELS,TITLE,JULIAN	EDIT 130
	COMMON /TOOATA/ S,SPAN,XB,ZB,XAY,CARD,ZAY,APRA,APRB,DC,	EDIT 140
-	XALF,THIN,TAPE,CBAR,APBP,ETC,ETC,FIXED,AR,BR,XAN,ZAX,	EDIT 150
-	SCALE,NREC,ORDER,METRIC,IX,IY,IZ,IXZ,Q,V,GROSWT	EDIT 160
	COMMON /ROUTH/ PUNCH,PARAM,MACH,ALPHA,CG,AC,BC	EDIT 170
	INTEGER STC(15),ETC(15),THIN,ST(4),ET(4),	EDIT 180
-	LABELS(15),LONLAB(15),LATLAB(15),ORDER(15)	EDIT 190
	LOGICAL CARD,TAPE,CORECT,METRIC,APBP,PUNCH,ZEROIN,PUNCHO,	EDIT 200
-	LAA(5,4),LBB(5,8),LONG,LATR,VAR(3),ZERO(4),LAST,	EDIT 210
-	BIASKN,PLOTEM,TEST,PRINT,BOTH,DIAG,INCH	EDIT 220
	REAL IX,IY,IZ,IXZ,MACH,MATRX(8,8),JULIAN,AC(5,4),BC(5,8),LAB(12)	EDIT 230
	DIMENSION A(5,4),B(5,8),TITLE(20),DCMAX(8),DCMIN(8),XT4(3),	EDIT 240
-	AA(5,4),BB(5,8),AP(4,4),BP(4,8),NPTS(15),D1(8,7),APRD(35),	EDIT 250
-	ZMIN(7),ZMAX(7),ERRVEC(20),DC(4),APR(35,35),	EDIT 260
-	XT5(35),AR(5,4),BR(5,8),APRA(5,4),APRB(5,8),ABC(12),FIXED(7),	EDIT 270
-	APRLON(5,4),APRLAT(5,4),BPRLON(5,8),BPRLAT(5,8),TLAT(3),	EDIT 280
-	TLON(3),TYPE(3),SCALE(7),R(5,4),XT3(4),AALAT(5,4),AALON(5,4),	EDIT 290
-	BBLAT(5,8),BBLON(5,8),D1LON(5),D1LAT(5)	EDIT 300
	EQUIVALENCE (AA(1,1),LAA(1,1)),(BB(1,1),LBB(1,1))	EDIT 310
	DATA LONLAB/4HALFA,1HQ,1HV,4HTHET,2HAN,4HQDOT,2HAX,2HDE,2HDC,	EDIT 320
-	3HDC1,3HDC2,3HPHI,3HALT,4HMACH,4HQBAR/,LATLAB/4HBETA,1HP,	EDIT 330
-	1HR,3HPHI,2HAY,4HPDOT,4HRDOT,2HDA,2HDR,3HDC1,3HDC2,4HALFA,	EDIT 340
-	1HV,4HMACH,4HQBAR/,LAB/1FA,1HB,2HAA,2HBB,2HAR,2HBR,4HAPRA,	EDIT 350
-	4HAPRB,2HD1,2HAP,2HBP,1HR/,SUML/3HSUM/,TLAT/4HLATE,3HRAL,	EDIT 360
-	1H/,TLON/4HLONG,4HITUO,4HINAL/,AALAT/3*1.,0.,4.,3*1.,0.,4.,	EDIT 370
-	0.,1.,1.,7*0./,BBLAT/3*1.,0.,4.,3*1.,0.,8.,10*0.,4*1.,16*0./,	EDIT 380
-	AALON/1.,1.,0.,0.,4.,0.,1.,0.,0.,4.,10*0./,BBLON/1.,1.,0.,0.,	EDIT 390
-	4.,4*0.,8.,10*0.,1.,1.,0.,1.,16*0./,D1LON/30000.,200000.,0.,	EDIT 400
-	100000.,2000./,APRLON/13000.,15.,2*0.,4.,0.,800.,2*0.,4.,	EDIT 410
-	10*0./,APRLAT/13000.,15,15.,0.,4.,13000.,500.,800.,0.,4.,	EDIT 420
-	13000.,5.,800.,7*0./,BPRLAT/13000.,15,15.,0.,4.,13000.,15,	EDIT 430
-	15.,0.,8.,13000.,15,15.,2*0.,13000.,15,15.,22*0./,	EDIT 440
-	BPRLON/13000.,15.,2*0.,4.,13000.,15.,2*0.,8.,13000.,15.,3*0.,	EDIT 450
-	13000.,15.,23*0./,D1LAT/500000.,1500.,1000000.,30000.,5000./	EDIT 460
	NAMELIST /INPUT/ GROSWT,Q,S,SPAN,CBAR,V,IX,IY,IZ,IXZ,PUNCHO,	EDIT 470
-	XB,ZB,XAY,ZAY,XALF,XAN,ZAX,WMAFR,PLTMAX,NEAT,	EDIT 480
-	CG,MACH,ALPHA,PARAM,SPS,NCASE,NOITER,TEST,PLOTEM,TIMESC,	EDIT 490
-	PUNCH,THIN,LONG,LATR,WFAC,ND1,CARD,TAPE,BOUND,ERRMAX,	EDIT 500
-	METRIC,PRINT,NAPR,D1RLX,D1TOL,FIXED,VAR,DC,INCH,	EDIT 510
-	ZERO,SCALE,ZMIN,ZMAX,DCMIN,DCMAX,NREC,ORDER,BOTH,NCPLLOT	EDIT 520
	JULIAN=DATE(JULIAN)	EDIT 530
	APR(35,3)=SUML	EDIT 540
	READ (1,2000) TITLE	EDIT 550
	WRITE (3,2005) TITLE,JULIAN	EDIT 560

# APPENDIX A – Continued

```

C***** DEFAULTS
      NCPLT=0
      V=0.
      Q=0.
      MACH=0.
      PUNCHD=.FALSE.
      NEAT=0
      NREC=15
      METRIC=.FALSE.
      BOTH=.FALSE.
      DO 14 I=1,15
14    ORDER(I)=I
      DO 10 I=1,8
      DCMIN(I)=0.
10    DCMAX(I)=0.
      DO 13 I=1,12
13    ABC(I)=LAB(I)
      CORECT=.FALSE.
      CARD=.FALSE.
      TAPE=.TRUE.
      ZEROIN=.FALSE.
      BIASKN=.FALSE.
      PLOTE=.TRUE.
      TEST=.FALSE.
      LONG=.FALSE.
      LATR=.FALSE.
      DIAG=.TRUE.
      PLTMAX=1.E+05
      ERRMAX=1.E+20
      PUNCH=.FALSE.
      PARAM = 0.
      CG = .25
      XB=0.
      ZB=0.
      XAY=0.
      ZAY=0.
      THIN=1
      D1(8,1)=5.
      D1(8,2)=5.
      MAX=8
      CALL AZOT(D1)
      MAX=5
      MIX=5
      R(5,1)=4.
      R(5,2)=4.
      R(5,3)=ABC(12)
      CALL AZOT(R)
      DO 136 I=1,4
      R(I,1)=1.
      ZERO(I)=.FALSE.
136  DC(I) = 0.
      XALF=0.
      ALPHA=999.
      PRINT=.FALSE.
      DO 137 I=1,7
      ZMIN(I)=0.
      ZMAX(I)=0.

```

```

EDIT 570
EDIT 580
EDIT 590
EDIT 600
EDIT 610
EDIT 620
EDIT 630
EDIT 640
EDIT 650
EDIT 660
EDIT 670
EDIT 680
EDIT 690
EDIT 700
EDIT 710
EDIT 720
EDIT 730
EDIT 740
EDIT 750
EDIT 760
EDIT 770
EDIT 780
EDIT 790
EDIT 800
EDIT 810
EDIT 820
EDIT 830
EDIT 840
EDIT 850
EDIT 860
EDIT 870
EDIT 880
EDIT 890
EDIT 900
EDIT 910
EDIT 920
EDIT 930
EDIT 940
EDIT 950
EDIT 960
EDIT 970
EDIT 980
EDIT 990
EDIT1000
EDIT1010
EDIT1020
EDIT1030
EDIT1040
EDIT1050
EDIT1060
EDIT1070
EDIT1080
EDIT1090
EDIT1100
EDIT1110
EDIT1120
EDIT1130

```



# APPENDIX A – Continued

```

      FIXED(I)=0.
137 SCALE(I)=1.
      XAN=0.
      ZAX=0.
      BOUND=.001
      SPS=0.
      WMAPR=0.
      NOITER=6
      NCASE=1
      NI=35
      TIMESC=1.
      DO 11 I=1,3
      VAR(I)=.TRUE.
11 TYPE(I)=TLAT(I)
      S=.001
      SPAN=.001
      CBAR=.001
      GROSWT=1.E+09
      IY=1.E+09
      IX=1.E+09
      IZ=1.E+09
      IX7=0.
      NO1=0
      NAPR=0
      WFAC=100.
      D1RLX=1.2
      D1TOL=1.4
      INCH=.FALSE.
      RATIO=.7874
C***** READ PROGRAM OPTIONS
      READ (1,INPUT)
      IF(INCH) RATIO=1.
      IF(NOITER.EQ.0) FUNCH=.FALSE.
      IF(NOITER.EQ.0) PUNCHD=.FALSE.
      PLTMAX=AMIN1(PLTMAX,ERRMAX)
      IF(CARD) TAPE=.FALSE.
      ATHIN=THIN
      IF(SPS.NE.0.) HH=ATHIN/SPS
      IF(ROTH) NREC=25
      IF (LONG) GO TO 5
      DO 2 I=1,15
2 LABELS(I)=LATLAB(I)
      GO TO 8
5 DO 6 I=1,15
6 LABELS(I)=LONLAB(I)
      DO 12 I=1,3
12 TYPE(I)=TLON(I)
8 CONTINUE
      ZEROIN = ZERO(1).OR.ZERO(2).OR.ZERO(3).OR.ZERO(4)
      BIASKN = VAR(1).OR.VAR(2).OR.VAR(3)
      WRITE(3,2009)TYPE,CARD,TAPE,SPS,THIN,NREC,BOTH
      WRITE(3,2010) WMAPR,NEAT,NOITER,BOUND,ERRMAX
      IF(NO1.NE.0) WRITE(3,2006)NC1,C1RLX,D1TOL
      IF(NAPR.NE.0) WRITE(3,2008)NAPR,WMAPR,WFAC
      WRITE(3,2011)PLOTEN,PLTMAX,NCPLT,TIMESC,PRINT,TEST,PUNCH,PUNCHD
      WRITE(3,2012)METRIC,Q,V,MACH,ALPHA,CG,PARAM,S,SPAN,CBAR,IX,IY,IZ,
      IXZ,GROSWT,XALF,XAN,XB,XAY,ZB,ZAY

```

```

EDIT1140
EDIT1150
EDIT1160
EDIT1170
EDIT1180
EDIT1190
EDIT1200
EDIT1210
EDIT1220
EDIT1230
EDIT1240
EDIT1250
EDIT1260
EDIT1270
EDIT1280
EDIT1290
EDIT1300
EDIT1310
EDIT1320
EDIT1330
EDIT1340
EDIT1350
EDIT1360
EDIT1370
EDIT1380
EDIT1390
EDIT1400
EDIT1410
EDIT1420
EDIT1430
EDIT1440
EDIT1450
EDIT1460
EDIT1470
EDIT1480
EDIT1490
EDIT1500
EDIT1510
EDIT1520
EDIT1530
EDIT1540
EDIT1550
EDIT1560
EDIT1570
EDIT1580
EDIT1590
EDIT1600
EDIT1610
EDIT1620
EDIT1630
EDIT1640
EDIT1650
EDIT1660
EDIT1670
EDUT1680
EDIT1690
EDIT1700

```

# APPENDIX A — Continued

```

WRITE(3,2013) LABELS,VAR,ZERO,FIXED,DC,SCALE
IF(PLOTEM) WRITE(3,2001) ZMIN,DCMIN,ZMA,DCMAX
SPS=SPS/ATHIN
DO 100 I=1,NCASE
READ (1,1000) ST,ET
STC(I)=ST(4)+1000*(ST(3)+60*ST(2)+3600*ST(1))
ETC(I)=ET(4)+1000*(ET(3)+60*ET(2)+3600*ET(1))
100 WRITE(3,2002) I,ST,ET
C***** READ MATRICES
WRITE(3,2003) TITLE,JULIAN
WRITE(3,2004)
MAX=8
101 CALL MATLD(MATRX,ABC,ILD)
IF(IABS(ILD).EQ.999) GO TO 108
IF(ILD.EQ.9) DIAG=.FALSE.
IF(ILD.EQ.1) CALL MAK(A,MATRX,5)
IF(ILD.EQ.2) CALL MAK(B,MATRX,5)
IF(ILD.EQ.3) CALL MAK(AA,MATRX,5)
IF(ILD.EQ.4) CALL MAK(BB,MATRX,5)
IF(ILD.EQ.5) CALL MAK(AR,MATRX,5)
IF(ILD.EQ.6) CALL MAK(BR,MATRX,5)
IF(ILD.EQ.7) CALL MAK(APRA,MATRX,5)
IF(ILD.EQ.8) CALL MAK(APRB,MATRX,5)
IF(IABS(ILD).EQ.9) CALL MAK(D1,MATRX,8)
IF(ILD.EQ.10) CALL MAK(AP,MATRX,4)
IF(ILD.EQ.11) CALL MAK(BP,MATRX,4)
IF(ILD.EQ.12) CALL MAK(R,MATRX,5)
GO TO 101
108 MAX=5
MZ=D1(8,1)
APBP=.FALSE.
IF(ABC(10).EQ.-99999. .AND. ABC(11).EQ.-99999.) APBP=.TRUE.
IF(LATR.OR.LONG) GO TO 117
IF(A(1,2).GT. .5) GO TO 113
LATR=.TRUE.
GO TO 117
113 LONG=.TRUE.
DO 114 I=1,12
114 LABELS(I)=LONLAB(I)
WRITE(3,2007)
117 IF(ILD.EQ.-999) LAST=.TRUE.
IF(ABC(5).NE.-99999.) CALL AMAKE(AR,A)
IF(ABC(6).NE.-99999.) CALL AMAKE(BR,B)
IF(LONG) GO TO 121
IF(ABC(9).EQ.-99999.) GO TO 119
DO 118 I=1,5
118 D1(I,I)=D1LAT(I)
119 IF(ABC(7).NE.-99999.) CALL AMAKE(APRA,APRLAT)
IF(ABC(8).NE.-99999.) CALL AMAKE(APRB,BPRLAT)
IF(ABC(3).NE.-99999.) CALL AMAKE(AA,AALAT)
IF(ABC(4).NE.-99999.) CALL AMAKE(BB,BBLAT)
IF(XB.NE.0. .OR.ZB.NE.0. .OR.XAY.NE.0. .OR.ZAY.NE.0.) CORECT=.TRUE.
IF(ABC(12).EQ.-99999.) GO TO 123
R(2,3)=-IXZ/IX
R(3,2)=-IXZ/IZ
IF(TEST) CALL ASPIT(R)
123 IF(.NOT.BOTH) GO TO 122

```

```

EDIT1710
EDIT1720
EDIT1730
EDIT1740
EDIT1750
EDIT1760
EDIT1770
EDIT1780
EDIT1790
EDIT1800
EDIT1810
EDIT1820
EDIT1830
EDIT1840
EDIT1850
EDIT1860
EDIT1870
EDIT1880
EDIT1890
EDIT1900
EDIT1910
EDIT1920
EDIT1930
EDIT1940
EDIT1950
EDIT1960
EDIT1970
EDIT1980
EDIT1990
EDIT2000
EDIT2010
EDIT2020
EDIT2030
EDIT2040
EDIT2050
EDIT2060
EDIT2070
EDIT2080
EDIT2090
EDIT2100
EDIT2110
EDIT2120
EDIT2130
EDIT2140
EDIT2150
EDIT2160
EDIT2170
EDIT2180
EDIT2190
EDIT2200
EDIT2210
EDIT2220
EDIT2230
EDIT2240
EDIT2250
EDIT2260
EDIT2270

```

# APPENDIX A -- Continued

```

DO 7 I=1,3                                EDIT2280
7 ORDER(I)=I+15                            EDIT2290
ORDER(4)=12                               EDIT2300
DO 9 I=5,11                               EDIT2310
9 ORDER(I)=I+14                           EDIT2320
ORDER(12)=1                               EDIT2330
ORDER(13)=3                               EDIT2340
GO TO 122                                  EDIT2350
121 IF(ABC(7).NE.-99999.) CALL AMAKE(APRA,APRLON) EDIT2360
IF(ABC(8).NE.-99999.) CALL AMAKE(APRB,BPRLON) EDIT2370
IF(ABC(3).NE.-99999.) CALL AMAKE(AA,AALON) EDIT2380
IF(ABC(4).NE.-99999.) CALL AMAKE(BB,BBLON) EDIT2390
IF(XALF.NE.0. .OR. XAN.NE.0. .OR. ZAX.NE.0.) CORECT=.TRUE. EDIT2400
IF(ABC(9).EQ.-99999.) GO TO 122           EDIT2410
DO 124 I=1,5                              EDIT2420
124 D1(I,I)=D1LON(I)                      EDIT2430
C***** COMPUTE SIZE OF SYSTEM              EDIT2440
C***** AA AND BB TO LOGICAL VARIABLES      EDIT2450
122 CALL INV(R,MAX)                        EDIT2460
MX=A(MAX,2)                               EDIT2470
MU=B(MAX,2)                               EDIT2480
MXP1=MX+1                                 EDIT2490
MZM=MZ-MX                                EDIT2500
DO 150 I=MXP1,MZ                           EDIT2510
150 IF(D1(I,I).EQ.0.) VAR(I-MX)=.FALSE.    EDIT2520
JKMM1=0                                    EDIT2530
DO 120 I=1,MX                              EDIT2540
DO 110 J=1,MX                              EDIT2550
IF(AA(I,J)) 107,106,107                   EDIT2560
106 LAA(I,J)=.TRUE.                        EDIT2570
GO TO 110                                  EDIT2580
107 LAA(I,J)=.FALSE.                       EDIT2590
JKMM1=JKMM1+1                             EDIT2600
110 CONTINUE                              EDIT2610
DO 120 J=1,MU                              EDIT2620
IF(BB(I,J)) 112,111,112                   EDIT2630
111 LBB(I,J)=.TRUE.                        EDIT2640
GO TO 120                                  EDIT2650
112 LBB(I,J)=.FALSE.                       EDIT2660
JKMM1=JKMM1+1                             EDIT2670
120 CONTINUE                              EDIT2680
JKMM=JKMM1                                EDIT2690
DO 125 I=1,MX                              EDIT2700
125 IF(ZERO(I)) JKMM1=JKMM1+1              EDIT2710
JKV=JKMM1                                 EDIT2720
DO 126 I=1,MZM                             EDIT2730
126 IF(VAR(I)) JKMM1=JKMM1+1              EDIT2740
JKM=JKMM1+1                               EDIT2750
APR(35,1)=JKMM1                           EDIT2760
APR(35,2)=JKM                             EDIT2770
RETURN                                     EDIT2780
1000 FORMAT(2(3I2,I3,1X))                 EDIT2790
2000 FORMAT(20A4)                          EDIT2800
2001 FORMAT(13H PLOT LIMITS/5X,7HMINIMUM,15F8.2/5X,7HMAXIMUM,15F8.2) EDIT2810
2002 FORMAT(/10H0 MANEUVER,I4,12H START TIME,4I5,11H STOP TIME,4I5) EDIT2820
2003 FORMAT(11H1,26X,20A4,13X,A10)         EDIT2830
2004 FORMAT(/18H0 INPUT MATRICES :I)       EDIT2840

```

# APPENDIX A – Continued

```

2005 FORMAT(1H1,20X,20A4,10X,A1)/40X,14HNEWTON-RAPHSON,          EDIT2850
- 28H DIGITAL DERIVATIVE MATCHING/60X,10H1 APR 1974)             EDIT2860
2006 FORMAT(28H001 WILL BE DETERMINED USING,I3,                   EDIT2870
- 28H PASSES. RELAXATION FACTOR =,F5,2,13H TOLERANCE =,F5,2)      EDIT2880
2007 FORMAT(46H THE A MATRIX INDICATES CASE IS LONGITUDINAL.     EDIT2890
- 57HLABELS ABOVE ARE WRONG. APPROPRIATE CORRECTIONS NOW MADE.)  EDIT2900
2008 FORMAT(23H0HMAPR WILL BE RUN WITH,I3,25H VALUES. FIRST 0., THEN,EDIT2910
- E9,2,27H. THEREAFTER MULTIPLYING BY,E9,2)                      EDIT2920
2009 FORMAT( 50H0INPUT DATA (I INDICATES TRUE OR YES, F INDICATES , EDIT2930
- 12HFALSE OR NO)/1H0,4X,3A4,5H CASE/16H DATA SOURCE,         EDIT2940
- 10H CARD? ,L1,8X,6HTAPE? ,L1/5X,12H0ATA RATE IS,F5,0,         EDIT2950
- 57H SAMPLES/SECOND ON SOURCE FILE (IF 0, DETERMINED FROM TIM,EDIT2960
- 22HES ON THE SOURCE FILE)/10X,26H0DIVIDED BY THINNING FACTOR, EDIT2970
- 3H OF,I3/5X,14H0N INPUT TAPE,I4,                               EDIT2980
- 56H DATA WORDS PER RECORD. SPECIAL SIGNAL ORDER DEFAULT? , EDIT2990
- L1)                                                              EDIT3000
2010 FORMAT(/16H0PROGRAM OPTIONS/24H0 APRIORI WEIGHTING =,E8,2,  EDIT3010
- 13X,I3,22H TIME HALVINGS IN EAT./                               EDIT3020
- 5X,12HITERATIONS =,I3,32H (ITERATION WILL STOP IF ERROR ,    EDIT3030
- 36HSUM CHANGES BY LESS THAN A FACTOR OF,E9,2,1H)/5X,         EDIT3040
- 49HCASE WILL BE STOPPEC IF ERROR SUM IS GREATER THAN,E9,2)    EDIT3050
2011 FORMAT(/7H00OUTPUT/12H0 PLOTS? ,L1,25H (NO PLOTS UNLESS FINAL ,EDIT3060
- 22HERROR SUM IS LESS THAN,E9,3,1H)/10X,                        EDIT3070
- 52HNUMBER OF CONTROLS AND EXTRA SIGNALS TO BE PLOTTED =,I3/   EDIT3080
- 10X,24HSECONDS PER CENTIMETER =,F5,2/5X,                      EDIT3090
- 50HPRINTED FLIGHT AND FINAL COMPUTED TIME HISTORIES? ,L1/5X,  EDIT3100
- 57H0EXTRA CUTPUT OF INTERMEDIATE STEPS FOR A DIAGNOSTIC AID? ,EDIT3110
- L1/5X,51HPUNCHED FINAL NON-DIMENSIONAL DERIVATIVES AND CONF,EDIT3120
- 14H0ENCE LEVELS? ,L1/5X,26HPUNCHED FINAL DIMENSIONAL ,      EDIT3130
- 10HMATRICES? ,L1)                                              EDIT3140
2012 FORMAT(/54H0FLIGHT CONDITION AND VEHICLE CHACTERISTICS (0. INOICA,EDIT3150
- 55HTES VALUE OBTAINED FROM TIME HISTORY CN QBAR,V OR MACH),    EDIT3160
- /44X,49H(MACH,ALPHA,CG AND PARAM ARE FOR REFERENCE ONLY, ,     EDIT3170
- 20HNOT USED IN PROGRAM)/5X,14HMETRIC UNITS? ,L1/5X,          EDIT3180
- 18H0YNAMIC PRESSURE =,F11,1,6X,10HVELOCITY =,F7,1/5X,         EDIT3190
- 6HMAC =,F6,3,23X,7HALPHA =,F7,2,22H (IF 999. , OBTAINED ,    EDIT3200
- 18HFROM TIME HISTCRY)/5X,19H0CENTER OF GRAVITY =,F6,3,10X,    EDIT3210
- 29H0THER IDENTIFYING PARAMETER =,E10,3/5X,11H0WING AREA =,    EDIT3220
- F7,1,17X,6HSPAN =,F7,2,5X,7HCHORD =,F6,2/5X,4HIX =,F9,1,22X, EDIT3230
- 4HIY =,F10,1,4X,4HIZ =,F10,1,4X,5HIXZ =,F8,1/5X,8HWEIGHT =,  EDIT3240
- F9,1/5X,26HINSTRUMENT OFFSETS FROM CG/                         EDIT3250
- 10X,53HX-DIRECTION OFFSETS (+ = INSTRUMENT IS FORWARD OF CG)/EDIT3260
- 14X,5HALPHA,F8,3,4H AN,F8,3/14X,4HBETA,F9,3,4H AY,F8,3/      EDIT3270
- 10X,49HZ-DIRECTION OFFSETS (+ = INSTRUMENT IS BELOW CG)/      EDIT3280
- 14X,4HBETA,F9,3,4H AY,F8,3)                                     EDIT3290
2313 FORMAT(26H0SIGNAL SCALING AND BIASES/9H SIGNALS,7X,14A8,A4/  EDIT3300
- 10H VAR BIAS,32X,3(7X,L1)/11H VAR I.C. ,6X,L1,3(7X,L1)/     EDIT3310
- 12H FIXED BIAS,11F8,2/12H SCALE FACT,7F8,2)                  EDIT3320
END                                                                EDIT3330

```

## APPENDIX A – Continued

### SUBROUTINE DATA

Description: Subroutine DATA reads the input time histories, performs any scaling and biasing required, and completes the program initialization. Averages of several time histories are obtained for use as default values for input parameters not set.

Programing notes: Comment cards separate major subroutine sections. If this is an intermediate step in the D1 determination or the *a priori* variation option, most of the subroutine is skipped since those sections were executed in the first step; this is true when the formal parameter IN is false.

Important variables –

X – vector containing one time point of the input time histories in degrees.

Z, DCR – vectors containing the input observations and controls in radians.

C – matrix containing factors for nondimensionalizing derivatives.

APR – matrix containing any off-diagonal *a priori* weightings. These weightings would be stored in the upper triangular portion of APR. There are no terms inserted here, but if such terms are desired, they may be inserted and the rest of the program will treat them properly. This matrix is referred to elsewhere in the program as SUM, and the lower triangular portion and the diagonal will be used to store other information.

APRD – vector containing the diagonal *a priori* weightings.

# APPENDIX A – Continued

## Subroutine listing:

C	SUBROUTINE DATA(IN)	DATA	0
C		DATA	10
C	READS TIME HISTORIES, PERFORMS VARIOUS INITIALIZATION	DATA	20
C		DATA	30
	COMMON /ALLOIM/ MAX,MIX	DATA	40
	COMMON /COM/ NCASE,MZ,NPTS,NPTT,SPS,PRINT,LONG,LATR,PLOTEM,ND1,	DATA	50
-	D1TOL,D1RLX,NAPR,WFAC,WHAPR,ERRSUM,LAST,RATIO	DATA	60
	COMMON /MATRIX/ A,B,AA,BB,AP,BP,D1,RI	DATA	70
	COMMON /TOGIRL/JKM,JKMM,JKMM1,ERRMAX,ZEROIN,XT5,BOUND,APR,NI	DATA	80
-	,BIASK,ZERO,APRD,JKV,DIAG	DATA	90
	COMMON /INFO/ HH,NOITER,MX,MXP1,MU,TEST,XBN,ZBX,IPQR,IXYZ,XT3,MZM,	DATA	100
-	CORECT,BIASKN,PLTMAX,XT4,ERRVEC,PUNCHD,NEAT	DATA	110
	COMMON /DIMENS/ C,E,MQS,THETN	DATA	120
	COMMON /HEADNG/ LABELS,TITLE,JULIAN	DATA	130
	COMMON /TODATA/ S,SPAN,XB,ZB,XAY,CARD,ZAY,APRA,APRB,DCBIAS,	DATA	140
-	XALF,THIN,TAPE,CBAR,APBP,STC,ETC,BIAS,AR,BR,XAN,ZAX,	DATA	150
-	SCALE,NREC,ORDER,METRIC,AIX,AIY,AIZ,AIXZ,Q,V,GROSWT	DATA	160
	COMMON /ROUTH/ PUNCH ,PARAM,MACH,ALPHA,CG,AC,BC	DATA	170
	DIMENSION A(5,4),B(5,8),TITLE(20),XT4(3),APRD(35),RECORD(100),	DATA	180
-	AA(5,4),BB(5,8),X(15),Z(7),E(3,8), AP(4,4),BP(4,8),	DATA	190
-	EXTRA(4), DCR(8), NPTS(15),D1(8,7),DC(4),	DATA	200
-	C(3,8),ERRVEC(20),APR(35,35),XT3(4),RI(5,4),	DATA	210
-	XT5(35),AR(5,4),BR(5,8),APRA(5,4),APRB(5,8),AC(5,4),BC(5,8)	DATA	220
	INTEGER T(4),ORDER(15),THIN,STC(15),ETC(15)	DATA	230
	REAL DCBIAS(4),CALIB(7),BIAS(7),LABELS(15),MACH,SCALE(7)	DATA	240
	LOGICAL CORECT,METRIC,CARD,PLOTEM,APBP,AA,BB,TAPE,LAST,DIAG,	DATA	250
-	BIASKN,ZEROIN,TEST,LONG,LATR,PRINT,IN,BIASK(3),ZERO(4),	DATA	260
-	PUNCHD,PRNT	DATA	270
	EQUIVALENCE(X(8),DC(1)),(X(12),EXTRA(1))	DATA	280
	DATA STAR/1H*/ ,BLANK/1H /	DATA	290
	PRNT=PRINT,OR.(NOITER.EQ.0)	DATA	300
	G=32.172	DATA	310
	IF(METRIC) G=9.80665	DATA	320
	RAD=57.2958	DATA	330
	LINE=50	DATA	340
	DO 5 I=1,3	DATA	350
5	XT4(I)=0.	DATA	360
	DO 10 I=1,7	DATA	370
	CALIB(I)=1./RAD	DATA	380
10	Z(I)=0.	DATA	390
	CALIB(5)=1.	DATA	400
	DO 20 I=4,8	DATA	410
20	DCR(I)=0.	DATA	420
	IF(.NOT.LONG) GO TO 50	DATA	430
	XT4(1)=1.	DATA	440
	CALIB(3)=1.	DATA	450
	CALIB(7)=1.	DATA	460
50	CONTINUE	DATA	470
C*****	READ INPUT TIME HISTORY	DATA	480
	IF(.NOT.IN) GO TO 505	DATA	490
	IF(PRNT) WRITE(3,2001)	DATA	500
	NPTT=0	DATA	510
	AMACH=0.	DATA	520
	ALFA=0.	DATA	530
	AV=0.	DATA	540
	AQBAR=0.	DATA	550
	PHI=0.	DATA	560

# APPENDIX A — Continued

THETA=0.	DATA 570
VEL=V	DATA 580
DO 500 I11=1,NCASE	DATA 590
ISTMS=STC(I11)	DATA 600
IETMS=ETC(I11)	DATA 610
ITHIN=THIN-1	DATA 620
NPTS(I11)=0	DATA 630
IF(I11.LE.4) DCR(I11+4)=1.	DATA 640
260 IF (TAPE) GO TO 240	DATA 650
READ (1,1001) T,X	DATA 660
GO TO 250	DATA 670
240 READ (4) T,(RECORD(I),I=1,NREC)	DATA 680
250 IF ((T(4)+1000*(T(3)+60*T(2)+3600*T(1))).LT.ISTMS) GO TO 260	DATA 690
ITST=T(4)	DATA 700
IF(.NOT.TAPE) GO TO 300	DATA 710
DO 270 I=1,15	DATA 720
270 X(I)=RECORD(ORDER(I))	DATA 730
300 ITM=T(4)+1000*(T(3)+60*T(2)+3600*T(1))	DATA 740
IF(ITM.GT.IETMS) GO TO 430	DATA 750
ITHIN=ITHIN+1	DATA 760
IF(MOD(ITHIN,THIN).NE.0) GO TO 385	DATA 770
NPTS(I11) = NPTS(I11) + 1	DATA 780
IF(NPTS(1).NE. 2.OR. SPS.NE.0.) GO TO 309	DATA 790
I=T(4)-ITST	DATA 800
IF(I.LT.0) I=I+1000	DATA 810
HH=((I+2)/5)*5	DATA 820
HH=HH/1000.	DATA 830
SPS=1./HH	DATA 840
C***** ADD BIASES AND SCALE FACTORS	DATA 850
309 DO 310 I=1,4	DATA 860
DC(I)=DC(I)+DCBIAS(I)	DATA 870
310 DCR(I)=DC(I)/RAD	DATA 880
DO 315 I=1,MZ	DATA 890
315 X(I)=X(I)*SCALE(I)+BIAS(I)	DATA 900
AMACH=AMACH+EXTRA(3)	DATA 910
AQBAR=AQBAR+EXTRA(4)	DATA 920
IF (LONG) GO TO 350	DATA 930
IF(.NOT.CORECT) GO TO 340	DATA 940
IF( V.EQ.0.) VEL=EXTRA(2)	DATA 950
X(1)=X(1)-(XB*X(3)-ZB*X(2))/VEL	DATA 960
340 ALFA=ALFA+EXTRA(1)	DATA 970
AV=AV+EXTRA(2)	DATA 980
GO TO 360	DATA 990
350 IF(.NOT.CORECT) GO TO 355	DATA1000
IF( V.EQ.0.) VEL=X(3)	DATA1010
X(1)=X(1)+XALF*X(2)/VEL	DATA1020
355 ALFA=ALFA+X(1)	DATA1030
AV=AV+X(3)	DATA1040
PHI=PHI+EXTRA(1)	DATA1050
THETA=THETA+X(4)	DATA1060
360 DO 365 I=1,MZ	DATA1070
365 Z(I)=X(I)*CALIB(I)	DATA1080
ITIME=T(4)+1000*(T(3)+100*T(2)+10000*T(1))	DATA1090
WRITE (7) ITIME,Z,DCR,EXTRA	DATA1100
IF(.NOT.PRNT) GO TO 375	DATA1110
IF(MOD(LINE,50).EQ.0)	DATA1120
-WRITE(3,2003) TITLE,JULIAN,GROSWT,AIX,AIZ,AIXZ,AIY,Q,V,LABELS	DATA1130

# APPENDIX A — Continued

WRITE(3,2010) T,X	DATA1140
LINE=LINE+1	DATA1150
375 IF (ITM.EQ.IETMS) GO TO 430	DATA1160
385 IF (CARD) GO TO 400	DATA1170
READ (4) T,(RECORD(I),I=1,NREC)	DATA1180
DO 390 I=1,15	DATA1190
390 X(I)=RECORD(ORDER(I))	DATA1200
GO TO 300	DATA1210
400 READ (1,1001) T,X	DATA1220
GO TO 300	DATA1230
430 IF (NPTS(I11).GT.0) GO TO 435	DATA1240
WRITE(3,2000) I11	DATA1250
STOP	DATA1260
435 NPTT=NPTT+NPTS(I11)	DATA1270
WRITE(3,2007) I11,NPTS(I11)	DATA1280
500 CONTINUE	DATA1290
ANPT=FLOAT(NPTT)	DATA1300
IF (MACH.EQ.0.) MACH=AMACH/ANPT	DATA1310
IF (ALPHA.EQ.999.) ALPHA=ALFA/ANPT	DATA1320
IF (V.EQ.0.) V=AV/ANPT	DATA1330
IF (Q.EQ.0.) Q=AQBAR/ANPT	DATA1340
VOG=V/G	DATA1350
AM=GROSWT*VOG/(Q*S)	DATA1360
V2=2.*V	DATA1370
IF (LONG) GO TO 170	DATA1380
C***** LATERAL SETUP	DATA1390
XAN=-ZAY	DATA1400
ZAX=XAY	DATA1410
IPQR=3	DATA1420
IXYZ=1	DATA1430
P1=VOG	DATA1440
P3=1.	DATA1450
AP3=1.	DATA1460
QSB=Q*S*SPAN	DATA1470
QSB8=QSB*SPAN	DATA1480
C(1,2)=1.	DATA1490
C(2,2)=V2*AIX/QSB8	DATA1500
C(3,2)=V2*AIZ/QSB8	DATA1510
C(1,3)=0.	DATA1520
C(2,3)=C(2,2)	DATA1530
C(3,3)=C(3,2)	DATA1540
C(1,1)=AM/RAD	DATA1550
C(2,1)=AIX/(QSB*RAD)	DATA1560
C(3,1)=AIZ/(QSB*RAD)	DATA1570
DO 160 I=1,3	DATA1580
C(I,8)=C(I,1)*RAD	DATA1590
DO 160 J=4,7	DATA1600
160 C(I,J)=C(I,1)	DATA1610
GO TO 200	DATA1620
C***** LONGITUDINAL SETUP	DATA1630
170 QSCI=Q*S*CBAR/AY	DATA1640
THETA=THETA/ANPT	DATA1650
WQS=COS(THETA/RAD)*COS(PHI/(RAD*ANPT))*GROSWT/(Q*S)	DATA1660
IPQR=2	DATA1670
IXYZ=3	DATA1680
P1=-VOG	DATA1690
P3=1./G	DATA1700



# APPENDIX A — Continued

```

AP3=J.
C(1,1)=AM/RAD
C(2,1)=1./(QSCI*PAD)
C(3,1)=C(1,1)/V
C(1,2)=0.
C(2,2)=V2/(QSCI*CBAR)
C(3,2)=C(1,2)
DO 180 I=1,3
C(I,8)=C(I,1)*RAD
C(I,3)=C(I,8)*V/2.
DO 180 J=4,7
180 C(I,J)=C(I,1)
THETN=THETA*C(1,1)
C SET E=99*99 IF DERIVATIVE IS FIXED, OTHERWISE E=99 99
200 DO 220 I=1,3
DO 210 J=1,3
E(I,J)=STAR
IF(.NOT.AA(I,J)) E(I,J)=BLANK
210 CONTINUE
DO 220 J=4,8
K=J-3
E(I,J)=STAR
IF(.NOT.BB(I,K)) E(I,J)=BLANK
220 CONTINUE
MAX=8
C***** FORM AP AND BP IF NOT READ IN
IF (APBP) GO TO 129
DO 112 J=1,MU
BP(1,J)=P1
BP(2,J)=1.
112 BP(3,J)=P3
DO 114 J=1,MX
AP(1,J)=0.
AP(2,J)=1.
114 AP(3,J)=AP3
AP(1,1)=P1
AP(3,1)=P3
129 CONTINUE
XBN=XAN/G
ZBX=ZAX/G
C***** STORE APRIORI WEIGHTINGS
505 MAX=35
CALL AZOT(APR)
DO 510 I=1,35
APR0(I)=0.
510 XT5(I)=0.
IF(WMAPR.EQ.0.) RETURN
K=0
DO 525 I=1,MX
DO 520 J=1,MU
IF(BB(I,J)) GO TO 520
K=K+1
XT5(K)=B(I,J)-BR(I,J)
APR0(K)=APRB(I,J)*WMAPR
520 CONTINUE
DO 525 J=1,MX
IF(AA(I,J)) GO TO 525

```

```

DATA1710
DATA1720
DATA1730
DATA1740
DATA1750
DATA1760
DATA1770
DATA1780
DATA1790
DATA1800
DATA1810
DATA1820
DATA1830
DATA1840
DATA1850
DATA1860
DATA1870
DATA1880
DATA1890
DATA1900
DATA1910
DATA1920
DATA1930
DATA1940
DATA1950
DATA1960
DATA1970
DATA1980
DATA1990
DATA2000
DATA2010
DATA2020
DATA2030
DATA2040
DATA2050
DATA2060
DATA2070
DATA2080
DATA2090
DATA2100
DATA2110
DATA2120
DATA2130
DATA2140
DATA2150
DATA2160
DATA2170
DATA2180
DATA2190
DATA2200
DATA2210
DATA2220
DATA2230
DATA2240
DATA2250
DATA2260
DATA2270

```

# APPENDIX A — Continued

```

      K=K+1                                DATA2280
      XT5(K)=A(I,J)-AR(I,J)                DATA2290
      APRD(K)=APRA(I,J)*WMAPR              DATA2300
525  CONTINUE                             DATA2310
1001 FORMAT(3I2,I4,7F10.4/8F10.4)        DATA2320
2000 FORMAT(14H0TIME INTERVAL,I3,10H NOT FOUND) DATA2330
2001 FORMAT(55H0INPUT TIME HISTORY WITH BIASES AND SCALE FACTORS APPLI,DATA2340
-      38HED AND VANE CORRECTIONS ADDED FOLLOWS.) DATA2350
2003 FORMAT(1H1,26X,20A4,13X,A10/4HGM =,F8.1,6H IX =,F9.1,6H IZ =, DATA2360
-      F10.1,7H IXZ =,F7.1,6H IY =,F9.1,8H QBAR =,F7.2,5H V =, DATA2370
-      F8.2/5X,4HTIME,6X,14A8,A4) DATA2380
2007 FORMAT(1H0,40X,35HTOTAL NUMBER OF POINTS FOR MANEUVER,I3,2H =,I6) DATA2390
2010 FORMAT(1X,3I2,I3,2X,12F8.3,F8.1,F8.3,F8.2) DATA2400
      RETURN                               DATA2410
      END                                  DATA2420

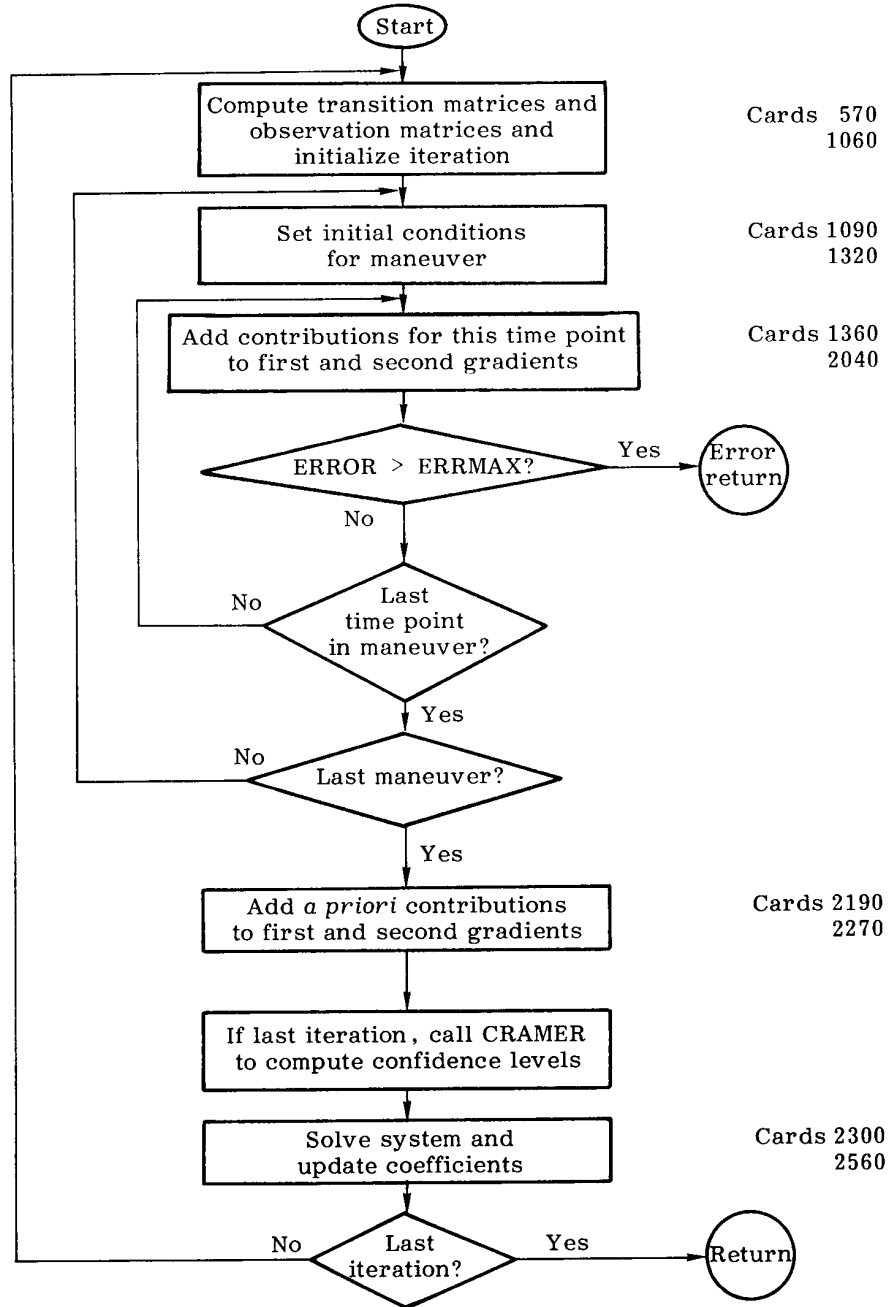
```

# APPENDIX A – Continued

## SUBROUTINE AGIRL

Description: Subroutine AGIRL performs the parameter estimation. Almost all the routine is skipped if NOITER = 0.

Flow chart:



## APPENDIX A – Continued

Programing notes: For derivation of the form of the first and second gradients, see reference 3.

Important variables –

SUM – contains second gradient in lower triangular and diagonal locations, and off-diagonal *a priori* weightings in upper triangular. Diagonal *a priori* weightings are in APRD. The first gradient appears as an extra column in SUM (the JKM<sup>th</sup> column). The SUM matrix is printed each iteration when TEST = T.

$$XJI = \nabla_c (z_i - y_i)^*$$

$$RIA = R^{-1}A$$

$$RIB = R^{-1}B$$

$$PHI1 = e^{R^{-1}A\Delta t}$$

$$APHI = \left( \int_0^{\Delta t} e^{R^{-1}A\tau} d\tau \right) R^{-1}$$

$$BPHI = (APHI)(B)$$

AAP, BBP – observation matrices formed from A and AP or B and BP, with any terms for accelerometer offset from the center of gravity added. (These matrices are referred to as G and H in the derivation.)

RIAP – array of partial derivatives of AAP with respect to A.

$$RIAP(I, J, K) = \frac{\partial AAP(I, K)}{\partial A(J, K)}.$$

RIBP – array of partial derivatives of BBP with respect to B.

$$RIBP(I, J, K) = \frac{\partial BBP(I, K)}{\partial B(J, K)}.$$

Z, U – measured values of observations and controls.

XT1, XT2 – computed values for observations.

XT3 – variable initial conditions on the states.

XT4 – variable bias on the observations other than states.

XT5 – difference between the estimated coefficients and the *a priori* values.

PB – solution vector for the change in the estimates of the coefficients.

MX – number of states.

MZ – number of observations.

# APPENDIX A – Continued

## Subroutine listing:

	SUBROUTINE AGIRL	AGIR 0
C		AGIR 10
C	CORE SUBROUTINE - ITERATIVE LOCP	AGIR 20
C		AGIR 30
	COMMON /ALLODIM/ MAX,MIX	AGIR 40
	COMMON /COM/ NCASE,MZ,NPTS,NPTT,SPS,PRINT,LONG,LATR,PLOTEM,ND1,	AGIR 50
	- D1TOL,D1RLX,NAPR,WFAC,WMAFR,ERRSUM,LAST,RATIO	AGIR 60
	COMMON /TOGIRL/JKM,JKMM,JKMM1,ERRMAX,ZEROIN,XT5,BOUND,SUM,NI	AGIR 70
	- ,BIASK,ZERO,APRD,JKV,DIAG	AGIR 80
	COMMON /INFO/ HH,NOITER,MX,MXP1,MU,TEST,XAN,ZAX,IPQR,IXYZ,XT3,MZM,	AGIR 90
	- CORECT,BIASKN,PLTMAX,XT4,ERRVEC,PUNCH,NEAT	AGIR 100
	COMMON /HEADING/ LABELS,TITLE,JULIAN	AGIR 110
	COMMON /MATRIX/ A,B,AA,BB,AP,BP,D1,RI	AGIR 120
	COMMON /ROUTH/ PUNCH,PARAM,MACH,ALP,CG,AC,BC	AGIR 130
	COMMON /DIMENS/ C,CC,E,WQS,THETN	AGIR 140
	REAL XT3(4),XT4(3),XT5(35),PB(35), APRC(35),LAEELS(15)	AGIR 150
	REAL U12(8),U23(8),BPHI(5,8),EXTRA(4),AC(5,4),BC(5,8)	AGIR 160
	LOGICAL AA,BB,TEST,ZEROIN,BIASKN,CORECT,LATR,ERSTOP,PUNCH	AGIR 170
	- ,ZERO(4),BIASK(3),PRINT,LAST,DIAG,E(24),PUNCH,PLOTEM	AGIR 180
	DIMENSION A( 5,4 ), B( 5,8 ), SUM(35,35),PHI1( 5,4 ), U( 8,3 ),	AGIR 190
	- AA( 5,4 ),BB( 5,8 ),RI(5,4), APhi( 5,4 ), Z( 8,3 ),	AGIR 200
	- AP( 4,4 ),BP( 4,8 ), XJI(35,8 ),DUM1( 5,4 ),D1( 8,7 ),	AGIR 210
	- XT12(4),AAP(3,4),BBP(3,8),RIA(5,4),RIB(5,8),	AGIR 220
	- XT1(7),NPTS(15),ERRVEC(20),XT2(7),D2(8),TITLE(20),XT6(4),	AGIR 230
	- RIBP(4,4,8),RIAP(4,4,4),XJID1(35,7),C(3,3),CC(3,5)	AGIR 240
	EQUIVALENCE (APHI(5,3),APHIL),(PHI1(5,3),PHI1L),(BPHI(5,3),BPHIL)	AGIR 250
	DATA PHI1L/4HPHI1/,APHIL/4HAPHI/,BPHIL/4HPHIB/	AGIR 260
	ANPT=FLOAT(NPTT)	AGIR 270
	ERMN=ERRMAX*ANPT	AGIR 280
	EN=1.E+50	AGIR 290
	ERSTOP=.FALSE.	AGIR 300
	DO 7 I=1,JKMM1	AGIR 310
	7 PB(I)=0.	AGIR 320
	DO 2 I = 1,MX	AGIR 330
	2 XT3(I)=0.	AGIR 340
	IF (NOITER.EQ.0) GO TO 600	AGIR 350
	WRITE (3,1003)TITLE,JULIAN,MACH,ALP,PARAM,CG	AGIR 360
	CALL DERIV(LONG)	AGIR 370
	DO 320 I=1,MX	AGIR 380
	DO 320 J=1,MX	AGIR 390
	DO 310 K=1,MU	AGIR 400
	310 RIBP(I,J,K)=RI(I,J)*BP(I,K)	AGIR 410
	DO 320 K=1,MX	AGIR 420
	320 RIAP(I,J,K)=RI(I,J)*AP(I,K)	AGIR 430
C	TERMS FOR ACCELEROMETER OFFSET FROM CG	AGIR 440
	IF(.NOT.CORECT) GO TO 350	AGIR 450
	DO 340 J=1,MX	AGIR 460
	DO 330 K=1,MU	AGIR 470
	RIBP(1,J,K)=RIBP(1,J,K)+XAN*RI(2,J)	AGIR 480
	330 RIBP(IXYZ,J,K)=RIBP(IXYZ,J,K)+ZAX*RI(IPQR,J)	AGIR 490
	DO 340 K=1,MX	AGIR 500
	RIAP(1,J,K)=RIAP(1,J,K)+XAN*RI(2,J)	AGIR 510
	340 RIAP(IXYZ,J,K)=RIAP(IXYZ,J,K)+ZAX*RI(IPQR,J)	AGIR 520
	350 CONTINUE	AGIR 530
	WRITE (3,103)JKMM1	AGIR 540
C	***** ITERATION LOOP	AGIR 550
	DO 32 LL = 1,NOITER	AGIR 560

# APPENDIX A – Continued

MAX = 5	AGIR 570
CALL ASPIT(A)	AGIR 580
CALL ASPIT(B)	AGIR 590
CALL AMULT(RI,A,PIA)	AGIR 600
CALL AMULT(RI,E,RIB)	AGIR 610
C COMPUTE A*AP AND B*BP	AGIR 620
DO 45 I=1,3	AGIR 630
DO 40 J=1,MX	AGIR 640
40 AAP(I,J)=RIA(I,J)*AP(I,J)	AGIR 650
DO 45 J=1,MU	AGIR 660
45 BBP(I,J)=RIB(I,J)*BP(I,J)	AGIR 670
IF(.NOT.CORECT) GO TO 50	AGIR 680
DO 46 J=1,MX	AGIR 690
AAP(I,J)=AAP(I,J)+XAN*RIA(2,J)	AGIR 700
46 AAP(IXYZ,J)=AAP(IXYZ,J)+ZAX*RIA(IPQR,J)	AGIR 710
DO 47 J=1,MU	AGIR 720
BBP(I,J)=BBP(I,J)+XAN*RIB(2,J)	AGIR 730
47 BBP(IXYZ,J)=BBP(IXYZ,J)+ZAX*RIB(IPQR,J)	AGIR 740
50 REWIND 7	AGIR 750
CALL AEAT(RIA,HH,PHI1,APHI,DUM1,SUM,NEAT)	AGIR 760
CALL AMULT(APHI,RI,DUM1)	AGIR 770
CALL AMAKE(APHI,DUM1)	AGIR 780
CALL AMULT(APHI,B,BPHI)	AGIR 790
IF(.NOT.TEST) GO TO 51	AGIR 800
CALL ASPIT(PHI1)	AGIR 810
CALL ASPIT(APHI)	AGIR 820
CALL ASPIT(BPHI)	AGIR 830
51 DO 53 I=1,MX	AGIR 840
DO 53 J=1,I	AGIR 850
TEMP=PHI1(I,J)	AGIR 860
PHI1(I,J)=PHI1(J,I)	AGIR 870
53 PHI1(J,I)=TEMP	AGIR 880
MAX = NI	AGIR 890
DO 60 I=1,JKM	AGIR 900
DO 60 J=1,I	AGIR 910
60 SUM(I,J)=0.	AGIR 920
DO 52 I=1,8	AGIR 930
52 DZ(I) = 0.0	AGIR 940
C VARIABLE BIAS	AGIR 950
IF(.NOT.BIASKN) GO TO 3	AGIR 960
IBIAS=JKV	AGIR 970
DO 16 I = 1,MZM	AGIR 980
IF(.NOT.BIASK(I)) GO TO 16	AGIR 990
IBIAS = IBIAS + 1	AGIR1000
DO 15 J = 1,MZ	AGIR1010
15 XJI(IBIAS,J)=0.	AGIR1020
XJI(IBIAS,I+MX)=1.	AGIR1030
16 CONTINUE	AGIR1040
WRITE(3,1001)(LABELS(I),I=MX+1,MZ)	AGIR1050
WRITE(3,102)(XT4(I),I=1,MZM)	AGIR1060
C***** CASE LOOP	AGIR1070
3 DO 26 LM = 1,NCASE	AGIR1080
NNM1=NPTS(LM)-1	AGIR1090
XJI(NI,1)=JKV	AGIR1100
XJI(NI,2)=MX	AGIR1110
CALL AZOT(XJI)	AGIR1120
READ(7) IT,XT1,(U(K,1),K=1,8),EXTRA	AGIR1130

# APPENDIX A — Continued

C	READ (7) IT,XT2,(U(K,2),K=1,8),EXTRA	AGIR1140
	VARIABLE INITIAL CONDITION	AGIR1150
	IF(.NOT.ZEROIN) GO TO 6	AGIR1160
	IC=JKHM	AGIR1170
	DO 4 I = 1,MX	AGIR1180
	IF(.NOT.ZERO(I)) GO TO 4	AGIR1190
	IC = IC + 1	AGIR1200
	XJI(IC,I)=1.	AGIR1210
	XT1(I) = XT1(I) + XT3(I)	AGIR1220
	XT2(I) = XT2(I) + XT3(I)	AGIR1230
4	CONTINUE	AGIR1240
	IF(LM.NE.1) GO TO 6	AGIR1250
	WRITE(3,1001) (LABELS(I),I=1,MX)	AGIR1260
	WRITE(3,108) (XT3(I),I=1,MX)	AGIR1270
6	DO 8 I=1,MZ	AGIR1280
	Z(I,1) = XT1(I)	AGIR1290
8	Z(I,2) = XT2(I)	AGIR1300
	IF(TEST) WRITE(3,111) (XT1(I),I=1,MZ)	AGIR1310
	IF(TEST) WRITE(3,111) (XT2(I),I=1,MZ)	AGIR1320
C*****	TIME LOOP	AGIR1330
C*****	COMPUTE GRADIENT AND HESSIAN	AGIR1340
	DO 10025 IP = 2,NNM1	AGIR1350
	READ (7) IT,(Z(K,3),K=1,7),(U(J,3),J=1,8),EXTRA	AGIR1360
	IF(LL.EQ.1) GO TO 203	AGIR1370
	DO 201 I=1,MX	AGIR1380
	XT12(I)=.5*(XT1(I)+XT2(I))	AGIR1390
201	XT6(I)=XT2(I)	AGIR1400
	GO TO 205	AGIR1410
203	DO 204 I=1,MX	AGIR1420
	XT12(I)=.5*(Z(I,2)+Z(I,1))	AGIR1430
	XT6(I)=Z(I,2)	AGIR1440
	Z(I,1) = Z(I,2)	AGIR1450
204	Z(I,2) = Z(I,3)	AGIR1460
205	CONTINUE	AGIR1470
	DO 206 I=1,MU	AGIR1480
	U12(I)=.5*(U(I,1)+U(I,2))	AGIR1490
	U23(I)=.5*(U(I,2)+U(I,3))	AGIR1500
	U(I,1)=U(I,2)	AGIR1510
206	U(I,2)=U(I,3)	AGIR1520
	DO 210 J=MXP1,MZ	AGIR1530
	DO 210 JK=1,JKV	AGIR1540
210	XJI(JK,J) = 0.0	AGIR1550
	DO 11 I = 1,MX	AGIR1560
	XT1(I)=XT2(I)	AGIR1570
11	XT2(I)=0.	AGIR1580
	CALL AMULT(XJI,PHI1,XJID1)	AGIR1590
	CALL AMAKE(XJI,XJID1)	AGIR1600
	JK = 0	AGIR1610
	DO 14 J = 1,MX	AGIR1620
	DO 12 K = 1,MU	AGIR1630
	XT2(J)=XT2(J)+8PHI(J,K)*U23(K)	AGIR1640
	IF (8B(J,K)) GO TO 12	AGIR1650
	JK = JK + 1	AGIR1660
	DO 115 I=1,MX	AGIR1670
	XJI(JK,I+MX)=RIBP(I,J,K)*U(K,1)	AGIR1680
115	XJI(JK,I)=XJI(JK,I)+U12(K)*APHI(I,J)	AGIR1690
12	CONTINUE	AGIR1700

# APPENDIX A — Continued

```

DO 14 K = 1,MX
XT2(J)=XT2(J)+PHI1(K,J)*XT1(K)
IF(AA(J,K)) GO TO 14
JK = JK + 1
DO 125 I=1,MX
XJI(JK,I+MX)=PIAP(I,J,K)*XT6(K)
125 XJI(JK,I)=XJI(JK,I)+XT12(K)*APHI(I,J)
14 CONTINUE
DO 19 L = MXP1,MZ
LMMX=L-MX
DO 17 JK=1,JKV
DO 17 K = 1,MX
17 XJI(JK,L)=XJI(JK,L) + XJI(JK,K)*AAP(LMMX,K)
XT2(L)=XT4(LMMX)
DO 18 K = 1,MU
18 XT2(L)=XT2(L)+BBP(LMMX,K)*U(K,2)
DO 19 K = 1,MX
19 XT2(L)=XT2(L)+AAP(LMMX,K)*XT2(K)
DO 20 J = 1,MZ
XJI(JKM,J) = Z(J,3) - XT2(J)
20 D2(J) = XJI(JKM,J)*2 + D2(J)
IF(TEST) WRITE(3,111)(XT2(I),I=1,MZ)
IF(DIAG) GO TO 62
MIX=8
XJI(NI,1)=JKM
XJI(NI,2)=MZ
CALL AMULT(XJI,D1,XJID1)
XJI(NI,1)=JKV
XJI(NI,2)=MX
MIX=5
GO TO 63
62 CALL DMULT(XJI,D1,XJID1,JKM,MZ)
63 CALL SUMULT(XJI,XJID1,SUM,JKM,MZ)
IF(SUM(JKM,JKM).GT.ERMX) GO TO 510
10025 CONTINUE
26 CONTINUE
C***** END OF TIME AND CASE LOOPS
ERRSUM=SUM(JKM,JKM)/ANPT
ERRVEC(LL)=ERRSUM
WRITE(3,104)ERRSUM
IF(ABS((EN-ERRSUM)/EN).LT.BOUND) ERSTOP=.TRUE.
EN=ERRSUM
DO 64 I=1,MZ
XT1(I)=D2(I)/ANPT
64 D2(I)=XT1(I)*D1(I,I)
WRITE(3,105)(XT1(I),I=1,MZ)
WRITE(3,106)(D2(I),I=1,MZ)
C***** SOLUTION OF SYSTEM
DO 28 I =1,JKMM1
XT5(I) = XT5(I) + P8(I)
SUM(I,JKM)=SUM(JKM,I)-XT5(I)*APRO(I)
SUM(I,I)=SUM(I,I)+APRO(I)
IM1=I-1
IF(IM1.EQ.0) GO TO 28
DO 27 J=1,IM1
27 SUM(I,J)=SUM(I,J)+SUM(J,I)
28 CONTINUE

```



## APPENDIX A – Continued

<pre> IF (TEST) CALL ASPIT(SUM) IF (ERSTOP.OR.(LL.EQ.NOITER)) CALL CRAPER(SUM,APRO,MU,MZ,ERFSUM) CALL SOLVE(SUM,PR) IF (TEST) WRITE(3,107)(PB(I),I=1,JKMM1) C***** UPDATE COEFFICIENTS IJ = 0 DO 31 I = 1,MX DO 30 J = 1,MU IF (BB(I,J) ) GO TO 30 IJ = IJ + 1 B(I,J) = PB(IJ) + B(I,J) 30 CONTINUE DO 31 J = 1,MX IF (AA(I,J) ) GO TO 31 IJ = IJ + 1 A(I,J) = PB(IJ) + A(I,J) 31 CONTINUE IF (.NOT.ZEROIN) GO TO 35 DO 34 I=1,MX IF (.NOT.ZERO(I)) GO TO 34 IJ=IJ+1 XT3(I)=XT3(I)+PB(IJ) 34 CONTINUE 35 IF (.NOT.BIASKN ) GO TO 37 DO 36 I=1,MZM IF (.NOT.BIASK(I)) GO TO 36 IJ=IJ+1 XT4(I) = XT4(I) + PB(IJ) 36 CONTINUE 37 WRITE(3,101)LL IF (ERSTOP) GO TO 38 32 CONTINUE C***** END OF ITERATION LOOP GO TO 500 38 WRITE(3,110)ROUND NOITER=LL 500 MAX=5 WRITE(3,2003) CALL ASPIT(AC) CALL ASPIT(BC) WRITE(3,2006) DO 508 I=1,3 DO 507 J=1,3 507 AC(I,J)=AC(I,J)*C(I,J) DO 508 J=1,5 508 BC(I,J)=BC(I,J)*CC(I,J) CALL ASPIT(AC) CALL ASPIT(BC) RETURN 510 WRITE(3,2001)ERRMAX NOITER=LL ERRVEC(LL)=ERRMAX 101 FORMAT(/50X,16HITERATION NUMBER,I4,10H COMPLETED) 102 FORMAT(15H VARIABLE BIAS ,3E12.4) 103 FORMAT(1H+,100X,20HNUMBER OF UNKNOWNNS =,I3/1H0,20X, - 23HENTERING ITERATION LOOP/25H0 DIMENSIONAL DERIVATIVE , - 39HMATRICES PER RADIAN. BIASES IN RADIAN.//) </pre>	<pre> AGIR2280 AGIR2290 AGIR2300 AGIR2310 AGIR2320 AGIR2330 AGIR2340 AGIR2350 AGIR2360 AGIR2370 AGIR2380 AGIR2390 AGIR2400 AGIR2410 AGIR2420 AGIR2430 AGIR2440 AGIR2450 AGIR2460 AGIR2470 AGIR2480 AGIR2490 AGIR2500 AGIR2510 AGIR2520 AGIR2530 AGIR2540 AGIR2550 AGIR2560 AGIR2570 AGIR2580 AGIR2590 AGIR2600 AGIR2610 AGIR2620 AGIR2630 AGIR2640 AGIR2650 AGIR2660 AGIR2670 AGIR2680 AGIR2690 AGIR2700 AGIR2710 AGIR2720 AGIR2730 AGIR2740 AGIR2750 AGIR2760 AGIR2770 AGIR2780 AGIR2790 AGIR2800 AGIR2810 AGIR2820 AGIR2830 AGIR2840 </pre>
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## APPENDIX A – Continued

104 FORMAT(95X,20HWEIGHTED ERROR SUM =,E12.4)	AGIR2850
105 FORMAT(7H ERRORS/1X,11E12.4)	AGIR2860
106 FORMAT(16H WEIGHTED ERRORS/1X,11E12.4)	AGIR2870
107 FORMAT(12H PB VECTOR =,10E12.4/(12X,10E12.4))	AGIR2880
108 FORMAT(15H VARIABLE IC ,4E12.4)	AGIR2890
110 FORMAT(37H0 ITERATION TERMINATING, ERROR WITHIN,F9.6,8H BOUND.)	AGIR2900
111 FORMAT(1X,7E12.4)	AGIR2910
1000 FORMAT(1H1,26X,20A4,13X,A10/1H0,10X,15HSTARTING VALUES,5X,	AGIR2920
- 6HMACH =,F6.3,5X,7HALPHA =,F7.2,5X,7HPARAM =,F10.4,5X,	AGIR2930
- 4HCG =,F6.3)	AGIR2940
1001 FORMAT(15X,7A12)	AGIR2950
2001 FORMAT(40H0ITERATION TERMINATING. MAXIMUM ERROR OF,E10.2,	AGIR2960
- 9H EXCEEDED/27H0INPUT TIME HISTORY FOLLOWS)	AGIR2970
2003 FORMAT(45H0CONFIDENCE LEVELS FOR NEXT TO LAST ITERATION/	AGIR2980
- 5X,13H(DIMENSIONAL)/)	AGIR2990
2006 FORMAT(22H0 (NON-DIMENSIONAL))	AGIR3000
600 RETURN	AGIR3010
END	AGIR3020

## APPENDIX A – Continued

### SUBROUTINE OUTPUT

Description: Subroutine OUTPUT provides the final output in several forms. The time histories are computed with the final derivative estimates and may be printed or written on a file for plotting. Final derivative estimates are also printed and, if requested, punched on cards. An error exit section to print the input time history is entered if PLTMAX or ERRMAX was exceeded.

Programing notes: Time history data for plotting are written on unit 8. The time histories are always computed to determine the final error sum, even if neither printout nor plots are requested. Most variable names are similar to those in subroutine AGIRL. ERRVEC contains the error sum from each iteration in AGIRL for the convergence summary.

# APPENDIX A – Continued

## Subroutine listing:

```

SUBROUTINE OUTPUT(D2)
C
C COMPUTES FINAL TIME HISTORY, OUTPUT MODES AS SPECIFIED
C
COMMON /ALLOIM/ MAX,MIX
COMMON /MATRIX/ A,B,AA,BB,AP,BP,D1,RI
COMMON /COM/ NCASE,MZ,NPTS,NPTT,SPS,PRINT,LONG,LATR,PLOTEM,ND1,
- DITOL,D1RLX,NAPR,WFAC,WMAFR,ERRSUM,LAST,RATIO
COMMON /INFO/ HH,NOITER,MX,MXP1,MU,TEST,XAN,ZAX,IPQR,IXYZ,XT3,MZ1,
- CORECT,RIASKN,PLTMAX,XT4,ERRVEC,PUNCHD,NEAT
COMMON/HEADNG/ LABELS,TITLE,JULIAN
COMMON /DIMENS/ C,CG,E,WQS,THETN
COMMON /ROUTH/ PUNCH,PARAM,MACH,ALP,CG,AC,BC
DIMENSION A(5,4),B(5,8),AA(5,4),BB(5,8),AP(4,4),BP(4,8),D1(8,7),
- XT4(3),NPTS(15),PHI1(5,4),APHI(5,4),DUM1(5,4),
- XT1(7),XT2(7),D2(7),Z(7),BJI(4),TITLE(20),U1(8),U2(8),
- ERRVEC(20),AAP(3,4),BBP(3,8),XT6(7),U(4),AC(5,4),BC(5,8)
LOGICAL TEST,CORECT,BIASKN,LATR,PUNCH,PLOTEM,E(24),PRINT,LAST,
- OUTPT,PUNCHD,LONG
REAL CALIB(7),LABELS(15),MACH,C(3,3),CG(3,5),U3(4),Y(7),BIASD(4)
- ,RI(5,4),RIA(5,4),RI8(5,8),EXTRA(4),EXTR1(4),XT3(4)
DATA PHI1L/4HPHI1/,APHIL/4HAPHI/,ALAT/4HLATR/,ALON/4HLONG/
RAD=57.2958
DO 5 I=1,7
5 CALIB(I)=1./RAD
CALIB(5)=1.
IF(LATR) GO TO 7
CALIB(3)=1.
CALIB(7)=1.
7 IF(NOITER.EQ.0) GO TO 8
IF(ERRVEC(NOITER).GE.PLTMAX) GO TO 450
8 PHI1(5,3)=PHI1L
APHI(5,3)=APHIL
OUTPT=PRINT.OR.PLOTEM
REWIND 7
MAX=5
WRITE(3,1000)TITLE,JULIAN
WRITE(3,2000)MACH,ALP,PARAM,CG
CALL DERIV(LONG)
DO 10 I=1,MZM
10 BIASD(I)=XT4(I)/CALIB(I+MX)
IF(BIASKN) WRITE(3,1003)(XT4(I),I=1,MZM)
C***** FINAL TIME HISTORY
CALL AMULT(RI,A,RIA)
CALL AMULT(RI,B,RI8)
CALL AEAT(RIA,HH,PHI1,APHI,DUM1,BBP,NEAT)
CALL AMULT(APHI,PI,DUM1)
CALL AMAKE(APHI,DUM1)
IF(.NOT.TEST) GO TO 60
CALL ASPIT(APHI)
CALL ASPIT(PHI1)
60 DO 70 I=1,MZ
70 D2(I)=0.
DO 55 I=1,3
DO 52 J=1,MX
52 AAP(I,J)=RIA(I,J)*AP(I,J)
DO 55 J=1,MU

```

# APPENDIX A – Continued

```

55 BBP(I,J)=RIB(I,J)*BP(I,J)                                OUTPUT 570
   IF(.NOT.CORECT) GO TO 69                                   OUTPUT 580
   DO 61 J=1,MX                                              OUTPUT 590
     AAP(I,J)=AAP(I,J)+RIA(2,J)*XAN                          OUTPUT 600
61 AAP(IXYZ,J)=AAP(IXYZ,J)+ZAX*RIA(IPQR,J)                  OUTPUT 610
   DO 62 J=1,MU                                              OUTPUT 620
     BBP(1,J)=BBP(1,J)+XAN*RIB(2,J)                          OUTPUT 630
62 BBP(IXYZ,J)=BBP(IXYZ,J)+ZAX*RIB(IPQR,J)                  OUTPUT 640
69 CONTINUE                                                  OUTPUT 650
   ERRSUM=0.                                                 OUTPUT 660
C***** CASE LOOP                                           OUTPUT 670
   DO 200 LM=1,NCASE                                         OUTPUT 680
     NNM1=NPTS(LM)-1                                         OUTPUT 690
     READ (7) IT,XT6,U2,EXTRA                                OUTPUT 700
     READ (7) IT1,XT2,U1,EXTR1                               OUTPUT 710
     DO 75 I=1,MX                                             OUTPUT 720
       Y(I)=XT6(I)+XT3(I)                                     OUTPUT 730
75 XT1(I)=XT2(I)+XT3(I)                                       OUTPUT 740
       IF(.NOT.OUTPUT) GO TO 95                               OUTPUT 750
       DO 76 I=MXP1,MZ                                         OUTPUT 760
         Y(I)=XT6(I)                                           OUTPUT 770
76 XT1(I)=XT2(I)                                               OUTPUT 780
       DO 80 I=1,MZ                                           OUTPUT 790
         Z(I) = XT6(I)/CALIB(I)                                OUTPUT 800
         Y(I)=Y(I)/CALIB(I)                                    OUTPUT 810
         XT2(I)=XT2(I)/CALIB(I)                                OUTPUT 820
80 XT6(I) = XT1(I)/CALIB(I)                                    OUTPUT 830
       DO 91 I=1,4                                             OUTPUT 840
         U3(I)=U2(I)*RAD                                         OUTPUT 850
91 U(I)=U1(I)*RAD                                             OUTPUT 860
       IF(.NOT.PRINT) GO TO 93                                  OUTPUT 870
       WRITE(3,1000)TITLE,JULIAN                               OUTPUT 880
       IF(LM.EQ.1) WRITE(3,2005)                                OUTPUT 890
       WRITE(3,2004)(LABELS(I),I=1,MZ)                         OUTPUT 900
       WRITE(3,113)IT,(7(I),I=1,MZ)                             OUTPUT 910
       WRITE(3,113)IT1,(XT6(I),I=1,MZ)                         OUTPUT 920
       LINE=2                                                   OUTPUT 930
       IF(.NOT.PLOTEN) GO TO 95                                 OUTPUT 940
93 WRITE (8) Y,Z,U3,EXTRA                                     OUTPUT 950
       WRITE (8) XT6,XT2,U,EXTR1                                OUTPUT 960
C***** TIME LOOP                                           OUTPUT 970
95 DO 200 IP=2,NNM1                                           OUTPUT 980
     READ (7) IT,Z,U2,EXTRA                                   OUTPUT 990
     DO 110 I=1,MX                                             OUTPUT1000
       BJ1(I)=0.                                               OUTPUT1010
       XT2(I)=0.                                               OUTPUT1020
     DO 110 J=1,MU                                             OUTPUT1030
       BJ1(I)=BJ1(I)+B(I,J)*(U2(J)+U1(J))*0.5                 OUTPUT1040
     DO 120 J=1,MX                                             OUTPUT1050
     DO 120 K=1,MX                                             OUTPUT1060
120 XT2(J) = XT2(J) + BJ1(K)*APHI(J,K) + XT1(K)*PHI1(J,K)   OUTPUT1070
     DO 140 L=MXP1,MZ                                         OUTPUT1080
       LMMX=L-MX                                              OUTPUT1090
       XT2(L)=XT4(LMMX)                                       OUTPUT1100
     DO 130 K=1,MU                                             OUTPUT1110
130 XT2(L) = XT2(L) + U2(K)*BBP(LMMX,K)                     OUTPUT1120
     DO 140 K=1,MX                                             OUTPUT1130

```

# APPENDIX A – Continued

```

140 XT2(L) = XT2(L) + XT2(K)*AAP(LMX,K)
    DO 150 J=1,MZ
    XT1(J) = XT2(J)
150 D2(J) = D2(J) + (Z(J)-XT2(J))**2
    IF(.NOT.OUTPT) GO TO 195
    DO 170 I=1,MZ
    Z(I)=Z(I)/CALIB(I)
170 Y(I)=XT2(I)/CALIB(I)
    DO 191 I=1,4
191 U(I)=U2(I)*RAD
    IF(PLOTEM) WRITE (8) Y,Z,U,EXTRA
    IF(.NOT.PRINT) GO TO 195
    IF(LINE .LT. 50) GO TO 190
    LINE = 0
    WRITE(3,1000)TITLE,JULIAN
    WRITE(3,2004)(LABELS(I),I=1,MZ)
190 LINE = LINE+1
    WRITE(3,113)IT,(Y(I),I=1,MZ)
195 DO 200 K=1,MU
    U1(K) = U2(K)
200 CONTINUE
C***** END LOOPS
    WRITE(3,2002)
    CALL ASPIT(A)
    CALL ASPIT(B)
C***** PUNCHED OUPUT AS DESIRED
    IF(.NOT.PUNCHD) GO TO 300
    CALL PLOP(A)
    CALL PLOP(B)
300 IF(.NOT.PUNCH) GO TO 400
    DO 320 I=1,3
    DO 310 J=1,3
310 A (I,J)=A (I,J)*C(I,J)
    DO 320 J=1,5
320 B (I,J)=B (I,J)*CC(I,J)
    A(5,1)=3.
    B(5,1)=3.
    TYPE=ALAT
    IF(.NOT.LONG) GO TO 330
    TYPE=ALON
C DETRIM AND CZ (GOOD ONLY FOR 2 DEGREE OF FREEDOM WITH NO EXTRA
C CONTROLS.)
    B(2,5)=-(A(2,1)*ALP+B(2,5))/B(2,1)
    B(1,5)=B(1,5)+A(1,1)*ALP+B(1,1)*B(2,5)-WQS
330 WRITE(2,2001)TYPE,(TITLE(I),I=1,9),MACH,ALP,PARAM,CG
    CALL PLOP(A)
    CALL PLOP(B)
    CALL PLOP(AC)
    CALL PLOP(BC)
400 IF(.NOT.BIASKN) GO TO 209
    WRITE(3,1004)(LABELS(I),I=MXP1,MZ)
    WRITE(3,1003)(BIASD(I),I=1,MZM)
209 DO 210 I=1,MZ
    XT1(I)=D2(I)/FLOAT(NPTT)
    D2(I)=XT1(I)*D1(I,I)
210 ERRSUM = ERRSUM + D2(I)
    WRITE(3,1001)ERRSUM

```

OUTP1140  
 OUTP1150  
 OUTP1160  
 OUTP1170  
 OUTP1180  
 OUTP1190  
 OUTP1200  
 OUTP1210  
 OUTP1220  
 OUTP1230  
 OUTP1240  
 OUTP1250  
 OUTP1260  
 OUTP1270  
 OUTP1280  
 OUTP1290  
 OUTP1300  
 OUTP1310  
 OUTP1320  
 OUTP1330  
 OUTP1340  
 OUTP1350  
 OUTP1360  
 OUTP1370  
 OUTP1380  
 OUTP1390  
 OUTP1400  
 OUTP1410  
 OUTP1420  
 OUTP1430  
 OUTP1440  
 OUTP1450  
 OUTP1460  
 OUTP1470  
 OUTP1480  
 OUTP1490  
 OUTP1500  
 OUTP1510  
 OUTP1520  
 OUTP1530  
 OUTP1540  
 OUTP1550  
 OUTP1560  
 OUTP1570  
 OUTP1580  
 OUTP1590  
 OUTP1600  
 OUTP1610  
 OUTP1620  
 OUTP1630  
 OUTP1640  
 OUTP1650  
 OUTP1660  
 OUTP1670  
 OUTP1680  
 OUTP1690  
 OUTP1700

# APPENDIX A – Continued

```

WRITE(3,100)
WRITE(3,105)(XT1(I),I=1,MZ)
WRITE(3,106)
WRITE(3,105)(D2(I),I=1,MZ)
IF(NOITER.NE.0) WRITE(3,108)(ERRVEC(I),I=1,NOITER),ERRSUM
IF(ERRSUM.LT.PLTMAX .OR. .NOT.PLOTEM) RETURN
450 WRITE(3,1002)PLTMAX
WRITE(3,1000)TITLE,JULIAN
WRITE(3,2004)(LABELS(I),I=1,MZ)
PLOTEM=.FALSE.
REWIND 7
DO 500 I=1,NPTT
READ (7) IT,Z,U,EXTRA
DO 460 J=1,7
460 Z(J)=Z(J)/CALIB(J)
DO 470 J=1,4
470 U(J)=U(J)*RAD
500 WRITE(3,113)IT,Z,U
100 FORMAT(7H ERRORS)
105 FORMAT (1X,11E12.4)
106 FORMAT(16H WEIGHTED ERRORS)
108 FORMAT(1H0,62X,6HEPERRORS/(1X,13F10.2))
113 FORMAT(2X,I12,11F10.4)
1000 FORMAT(1H1,26X,20A4,13X,A10/)
1001 FORMAT(90X,20HWEIGHTED ERROR SUM =,E12.4)
1002 FORMAT(55H0DATA WILL NOT BE PLOTTED BECAUSE THE ERROR SUM EXCEEDS,
- 24H THE MAXIMUM PERMISSIBLE,E10.2/
- 27H0INPUT TIME HISTORY FOLLOWS)
1003 FORMAT(15H VARIABLE BIAS ,4E12.4)
1004 FORMAT(8H0DEGREES,7X,4A12)
2000 FORMAT(1H0,10X,12HFINAL VALUES,5X,6HMACH =,F6.3,5X,7HALPHA =,F7.2,
- 5X,7HPARAM =,F10.4,5X,4HCG =,F6.3)
2001 FORMAT(A4,1X,8A4,A3,4F10.3)
2032 FORMAT(27H FINAL DIMENSIONAL MATRICES)
2004 FORMAT(1H0,5X,4HTIME,10X,7A10/)
2005 FORMAT(20H OUTPUT TIME HISTORY)
RETURN
END

```

```

OUTP1710
OUTP1720
OUTP1730
OUTP1740
OUTP1750
OUTP1760
OUTP1770
OUTP1780
OUTP1790
OUTP1800
OUTP1810
OUTP1820
OUTP1830
OUTP1840
OUTP1850
OUTP1860
OUTP1870
OUTP1880
OUTP1890
OUTP1900
OUTP1910
OUTP1920
OUTP1930
OUTP1940
OUTP1950
OUTP1960
OUTP1970
OUTP1980
OUTP1990
OUTP2000
OUTP2010
OUTP2020
OUTP2030
OUTP2040
OUTP2050
OUTP2060
OUTP2070
OUTP2080

```

## APPENDIX A — Continued

### SUBROUTINE THPLOT

Description: Subroutine THPLOT plots measured and computed time histories of observations and measured time histories of controls and extra signals.

Programing notes: The comment cards show how to decrease the run time in some instances at the cost of some storage. At present, two time histories at a time are read from the disk and plotted. Dimensions may be increased as indicated to permit more than two to be handled simultaneously, resulting in fewer disk accesses. With reasonably efficient disk units, the saving is not a significant portion of the program execution time. The limitation of 1000 points per maneuver arises from the dimensioning of X,XX,XXX and TIME as 1002. (The extra two locations are used for scaling information.) Program size may be reduced or the permissible maneuver length increased by changing this value. The special treatment of the title (plotting groups of four characters in a DO loop instead of using only one call to SYMBOL) is needed for compatibility with machines that use different word lengths.



# APPENDIX A — Continued

## Subroutine listing:

	SUBROUTINE THPLOT(FIRST)	THPL 0
C		THPL 10
C	PLOTS TIME HISTORIES	THPL 20
C		THPL 30
	COMMON /9UF/ BUFFER,YO,THGT	THPL 40
	COMMON /COM/ NCASE,MZ,NPTS,NPTT,SPS,PRINT,LONG,LATR,PLOTEM,N01,	THPL 50
-	D1TOL,D1RLX,NAPR,WFAC,WMAPR,ERRSUM,LAST,RATIO	THPL 60
	COMMON /TOPLOT/ XMAX,XMIN,DCMAX,DCMIN,TIMESC,NC	THPL 70
	COMMON /HEADNG/ LABELS,TITLE,JULIAN	THPL 80
	COMMON /LINCOM/ HGT	THPL 90
	DIMENSION DCMAX(8),DCMIN(8),XMAX(7),XMIN(7),NPTS(15),TITLE(20),	THPL 100
-	BUFFER(1024),TIME(1002),XXX(1002,2),X(1002,1),XX(1002,1),	THPL 110
-	Z(7),DC(8),ZZ(7),LABELS(15),MBCD(30)	THPL 120
	LOGICAL LONG,FIRST,LAST	THPL 130
	EQUIVALENCE (X(1,1),XXX(1,1)),(XX(1,1),XXX(1,2))	THPL 140
	DATA MBCD/3HDEG,3HD/S,3HF/S,3HDEG,3HG'S,4HD/S2,3HG'S,	THPL 150
-	5*3HDEG,2HFT/1H ,3HPSF,3HCEG,2*3HC/S,3HDEG,3HG'S,2*4HD/S2,	THPL 160
-	5*3HDEG,4HFT/S,1H ,3HPSF/	THPL 170
	NCH=1	THPL 180
C*****	FOR A DIRECT DECREASE IN RUN TIME AT THE COST OF	THPL 190
C	STORAGE, NCH MAY BE INCREASED (UP TO 7). THEN THE	THPL 200
C	FOLLOWING DIMENSIONS AND EQUIVALENCE MUST BE	THPL 210
C	CHANGED.	THPL 220
C	DIMENSION X(1002,NCH),XX(1002,NCH),XXX(1002,2*NCH)	THPL 230
C*****	EQUIVALENCE (XX(1,1),XXX(1,NCH+1))	THPL 240
	NBUF=1024	THPL 250
	TIMSC2=TIMESC*2.	THPL 260
	X0=5.	THPL 270
	HGT=.01	THPL 280
	NIP=0	THPL 290
	TSI=SPS*TIMSC2	THPL 300
	ITHIN=-MAX1(TSI/20.,1.)	THPL 310
	REWIND 8	THPL 320
	IF(.NOT.FIRST) GO TO 10	THPL 330
	CALL PLOTS(BUFFER,NBUF,13)	THPL 340
	CALL FACTOR(RATIO)	THPL 350
	YO=12.	THPL 360
	IF(RATIO.EQ.1.) YO=9.5	THPL 370
	THGT=.12/RATIO	THPL 380
C*****	LABELS AND TITLES	THPL 390
10	Y75=YO+.375	THPL 400
	IF (LONG) GO TO 50	THPL 410
	DO 20 I=1,15	THPL 420
20	MBCD(I)=MBCD(I+15)	THPL 430
50	DO 200 I=1,NCASE	THPL 440
	CALL PLOT(X0,0.,-3)	THPL 450
	CALL SYMBOL(-1.5,YO,THGT,TITLE(1),270.,4)	THPL 460
	DO 55 J=2,20	THPL 470
55	CALL SYMBOL(-1.5,999.,THGT,TITLE(J),270.,4)	THPL 480
	IF(NCASE.EQ.1) GO TO 57	THPL 490
	CALL SYMBOL(-2.,YO,THGT,8HMANEUVER,270.,8)	THPL 500
	YO15=YO-1.5	THPL 510
	CALL NUMBER(-2.,YO15,THGT,FLOAT(I),270.,-1)	THPL 520
57	CALL PLTDAT(-2.5,YO)	THPL 530
C*****	FORM TIME VECTOR AND PLOT TIME AXIS	THPL 540
	NPTS=NPTS(I)	THPL 550
	NP1=NPTS+1	THPL 560

# APPENDIX A – Continued

NP2=NOPTS+2	THPL 570
DO 60 J=1,NOPTS	THPL 580
60 TIME(J)=J	THPL 590
TIME(NP1)=Y0*TSI+1.	THPL 600
TIME(NP2)=-TSI	THPL 610
TLN=FLOAT(NOPTS)/TSI	THPL 620
CALL AXIS(0.,Y0,4HTIME,-4,TLN,270.,0.,TIMSC2)	THPL 630
XORG=.5	THPL 640
C ***** PLOT STATE TIME HISTORIES	THPL 650
ICHAN0=0	THPL 660
NCHAN=NCH	THPL 670
DO 120 K=1,7	THPL 680
IF(K.EQ.1) GO TO 90	THPL 690
ICHAN0=ICHAN0+NCHAN	THPL 700
IF(ICHAN0+NCHAN.LE.MZ) GO TO 70	THPL 710
IF(ICHAN0.GE.MZ) GO TO 125	THPL 720
NCHAN=MZ-ICHAN0	THPL 730
70 REWIND 8	THPL 740
IF(I.EQ.1) GO TO 90	THPL 750
DO 80 J=1,NIP	THPL 760
80 READ (8)	THPL 770
90 DO 130 J=1,NOPTS	THPL 780
READ (8) ZZ,Z,DC	THPL 790
DO 100 L=1,NCHAN	THPL 800
X(J,L)=Z(L+ICHAN0)	THPL 810
100 XX(J,L)=ZZ(L+ICHAN0)	THPL 820
DO 110 L=1,NCHAN	THPL 830
ICHAN=ICHAN0+L	THPL 840
SCAL=(XMAX(ICHAN)-XMIN(ICHAN))*5	THPL 850
XMN=XMIN(ICHAN)	THPL 860
IF(SCAL.NE.0.) GO TO 105	THPL 870
CALL SCALES(X(1,L),2.,NOPTS,.FALSE.)	THPL 880
CALL SCALES(XX(1,L),2.,NOPTS,.FALSE.)	THPL 890
SCAL=AMAX1(XX(NP2,L),X(NP2,L))	THPL 900
IF(SCAL.EQ.-999.) GO TO 110	THPL 910
XMN=X(NP1,L)	THPL 920
IF(XX(NP2,L).GT.X(NP2,L)) XMN=XX(NP1,L)	THPL 930
105 CALL SYMBOL(XORG+1.,Y75.,125,LABELS(ICHAN),0,4)	THPL 940
CALL AXIS(XORG,Y0,MBCD(ICHAN),4,2.,0.,XMN,SCAL)	THPL 950
X(NP1,L)=XMN-XORG*SCAL	THPL 960
XX(NP1,L)=X(NP1,L)	THPL 970
X(NP2,L)=SCAL	THPL 980
XX(NP2,L)=SCAL	THPL 990
CALL LINES(X(1,L),TIME,NOPTS,1,1,1)	THPL1000
CALL LINES(XX(1,L),TIME,NOPTS,ITHIN,-2,75)	THPL1010
XORG=XORG+2.5	THPL1020
110 CONTINUE	THPL1030
120 CONTINUE	THPL1040
C ***** PLOT CONTROL TIME HISTORIES	THPL1050
125 NCH2=NCHAN*2	THPL1060
IF(NCH2.GT.NC) NCH2=NC	THPL1070
ICHAN2=-NCH2	THPL1080
DO 160 K=1,4	THPL1090
ICHAN2=ICHAN0+NCH2	THPL1100
IF(ICHAN2.GE.NC) GO TO 170	THPL1110
IF(ICHAN2+NCH2.GT.NC) NCH2=NC-ICHAN2	THPL1120
REWIND 8	THPL1130

# APPENDIX A – Continued

IF(I.EQ. 1) GO TO 140	THPL1140
DO 130 J=1,NIP	THPL1150
130 READ (8)	THPL1160
DO 150 J=1,NOPTS	THPL1170
140 READ (8) ZZ,Z,DC	THPL1180
DO 150 L=1,NCH2	THPL1190
150 XXX(J,L)=DC(L+ICHANJ)	THPL1200
DO 160 L=1,NCH2	THPL1210
J=L+ICHAN0	THPL1220
M=J+7	THPL1230
SCAL =(DCMAX(J)-DCMIN(J))* .5	THPL1240
DCMN=DCMIN(J)	THPL1250
IF(SCAL.NE.0.) GO TO 155	THPL1260
CALL SCALES(XXX(1,L),2.,NOPTS,.TRUE.)	THPL1270
IF(XXX(NP2,L).EQ.-999.) GO TO 160	THPL1280
IF(XXX(NP2,L).GE..4 .OR. J.EQ.7) GO TO 153	THPL1290
XXX(NP2,L)=10.	THPL1300
XXX(NP1,L)=-10.	THPL1310
153 SCAL=XXX(NP2,L)	THPL1320
DCMN=XXX(NP1,L)	THPL1330
155 CALL SYMBOL (XCRG+1.,Y75.,.125,LABELS(M),J,4)	THPL1340
CALL AXIS(XORG,YO,MBCD(M),4,2.,0.,DCMN,SCAL)	THPL1350
XXX(NP1,L)=DCMN-XORG*SCAL	THPL1360
XXX(NP2,L)=SCAL	THPL1370
CALL LINES(XXX(1,L),TIME,NOPTS,1, 0,1)	THPL1380
XORG=XORG+2.5	THPL1390
160 CONTINUE	THPL1400
170 NIP=NIP+NOPTS	THPL1410
XO=XORG+5.	THPL1420
200 CONTINUE	THPL1430
CALL PLOT(XO,0.,-3)	THPL1440
RETURN	THPL1450
END	THPL1460

# APPENDIX A — Continued

## SUBROUTINE APRPLT

Description: Subroutine APRPLT plots the variation of the derivatives with *a priori* weighting. It may be used when the *a priori* variation option is active. The information to be plotted is in the matrix STORE.

### Subroutine listing:

```

SUBROUTINE APRPLT(STORE,AA,BB,NAPR,WHOLD,WFAC,LONG,FIRST,LAST,
-      RATIO)
C
C   PLOTS DERIVATIVES FOR APRIORI VARIATION
C
COMMON /BUF/ BUFFER,YO,THGT
COMMON/HEADNG/ LABELS,TITLE,JULIAN
COMMON /LINCOM/ HGT
LOGICAL AA(5,4),BB(5,8),LONG,FIRST,LAST
REAL STORE(14,27),ALABLO(3,3),ALABLA(3,3),BLABLO(3,4),BLABLA(3,4),APRP 0
-      BUFFER(1024),WMAPR(14),LABELS(15),TITLE(20)
APRP 10
DATA ALABLA/2HYB,2HLB,2HNB,2HYP,2HLP,2HNP,2HYR,2HLR,2HNR/,BLABLA/
APRP 20
-      3HYDA,3HLDA,3HND,3HYDR,3HLDR,3HNR,4HYDC1,4HLDC1,4HND1,
APRP 30
-      4HYDC2,4HLDC2,4HND2/,ALAELO/2HZA,2HMA,2HXA,2HZQ,2HMQ,2HXO,
APRP 40
-      2HZU,2HMU,2HXU/,BLABLO/3H7DE,3HME,3HXDE,3HZOC,3HMC,3HXDC,
APRP 50
-      4HZDC1,4HMC1,4HXDC1,4HZOC2,4HMC2,4HXDC2/
APRP 60
HGT=.07
APRP 70
NBUF=1024
APRP 80
JK=0
APRP 90
NPT=NAPR+1
APRP 100
NPT1=NPT+1
APRP 110
NPT2=NPT+2
APRP 120
IF(.NOT.FIRST) GO TO 5
APRP 130
CALL PLOTS(BUFFER,NBUF,13)
APRP 140
CALL FACTOR(RATIO)
APRP 150
YO=12.
APRP 160
IF(RATIO.EQ.1.) YO=9.5
APRP 170
THGT=.12/RATIO
APRP 180
5 CALL PLOT(0.,YC,-3)
APRP 190
CALL SYMBOL(-1.5,0.,THGT,TITLE(1),270.,4)
APRP 200
DO 7 J=2,20
APRP 210
7 CALL SYMBOL(-1.5,999.,THGT,TITLE(J),270.,4)
APRP 220
CALL PLTDAT(-4.,.5)
APRP 230
WMAPR(1)=-1.
APRP 240
DO 10 I=1,NAPR
APRP 250
10 WMAPR(I+1)=WMAPR(I)-1.
APRP 260
WMAPR(NPT1)=0.
APRP 270
WMAPR(NPT2)=1.
APRP 280
CALL NUMBER(-.5,-1.,.1,0.,270.,0)
APRP 290
Y=-.75
APRP 300
IF(NAPR.LT.2) GO TO 220
APRP 310
NAPR1=NAPR-1
APRP 320
W=WHOLD
APRP 330
DO 210 I=1,NAPR1
APRP 340
Y=Y-1.
APRP 350
CALL NUMBER(-.5,Y,.1,W,270.,3)
APRP 360
210 W=W*WFAC
APRP 370
220 CONTINUE
APRP 380
CALL SYMBOL(-1.,Y/2.,.125,5WMAPR,270.,5)
APRP 390
DO 200 I=1,3
APRP 400
DO 100 J=1,4
APRP 410
IF(99(I,J)) GO TO 100
APRP 420
JK=JK+1
APRP 430
CALL SCALES(STORE(1,JK),3.,NPT,.FALSE.)
APRP 440
DER=BLABLA(I,J)
APRP 450
IF(LONG) DER=BLABLO(I,J)
APRP 460
CALL AXIS(0.,0.,DER,4,3.,0.,STORE(NPT1,JK),STORE(NPT2,JK))
APRP 470
APRP 480
APRP 490
APRP 500
APRP 510
APRP 520
APRP 530
APRP 540
APRP 550
APRP 560

```

## APPENDIX A – Continued

	CALL LINES(STORE(1,JK),WMAFR,NPT,1,1,1)	APRP 570
	CALL PLOT(3.5,0.,-3)	APRP 580
100	CONTINUE	APRP 590
	DO 200 J=1,3	APRP 600
	IF(AA(I,J)) GO TO 200	APRP 610
	JK=JK+1	APRP 620
	CALL SCALES(STORE(1,JK),3.,NPT,.FALSE.)	APRP 630
	DER=ALABLA(I,J)	APRP 640
	IF(LONG) DER=ALABLO(I,J)	APRP 650
	CALL AXIS(3.,0.,DER, 4,3.,0.,STORE(NPT1,JK),STORE(NPT2,JK))	APRP 660
	CALL LINES(STORE(1,JK),WMAFR,NPT,1,1,1)	APRP 670
	CALL PLOT(3.5,0.,-3)	APRP 680
200	CONTINUE	APRP 690
	WMAFR(NPT)=WMAFR(NPT1)	APRP 700
	WMAFR(NPT1)=WMAFR(NPT2)	APRP 710
	NPT2=NPT1	APRP 720
	NPT1=NPT	APRP 730
	NPT=NAPR	APRP 740
	JK=JK+1	APRP 750
	CALL SCALES(STORE(1,JK),3.,NPT,.FALSE.)	APRP 760
	CALL AXIS(0.,0.,5HERROR,5,3.,0.,STORE(NPT1,JK),STORE(NPT2,JK))	APRP 770
	CALL LINES(STORE(1,JK),WMAFR,NPT,1,1,1)	APRP 780
	CALL PLOT(5.,-12.,-3)	APRP 790
	RETURN	APRP 800
	END	APRP 810

## APPENDIX A — Continued

### SUBROUTINE MATLD

**Description:** Subroutine MATLD reads matrices from cards and identifies the matrices.

**Programing notes:** ABC contains the names of the matrices that may be read in. The program compares the name read with elements of ABC to determine which matrix is being input. The characters END are taken as an indication that this is the last case; any other word not identifiable as a valid matrix name signals the end of a case, implying more cases to follow. The values of ILD and ABC indicate the status of the matrix input.

**Subroutine listing:**

C	SUBROUTINE MATLD(MATRX,ABC,ILD)	MATL 0
C	LOADS IN MATRICES - DETERMINES WHICH MATRIX IS BEING READ	MATL 10
C	PASSES STATUS INFORMATION BACK TO NREDIT	MATL 20
C	REAL MATRX(8,8),ABC(12)	MATL 30
	DATA END/3HEND/	MATL 40
	ILD=-999	MATL 50
	READ (1,1000) MATRX(8,3),II,JJ	MATL 60
	IF(MATRX(8,3).EQ.END) RETURN	MATL 70
	DO 10 I=1,12	MATL 80
	IF(MATRX(8,3).NE.ABC(I)) GO TO 10	MATL 90
	ABC(I)=-99999.	MATL 100
	ILD=I	MATL 110
	GO TO 20	MATL 120
10	CONTINUE	MATL 130
	ILD=999	MATL 140
	RETURN	MATL 150
20	MATRX(8,1)=II	MATL 160
	IF(JJ.NE.0) GO TO 25	MATL 170
C	DIAGONAL MATRIX	MATL 180
	ILD=-ILD	MATL 190
	MATRX(8,2)=MATRX(8,1)	MATL 200
	CALL AZOT(MATRX)	MATL 210
	READ (1,1001) (MATRX(I,I),I=1,II)	MATL 220
	RETURN	MATL 230
C	FULL MATRIX	MATL 240
25	MATRX(8,2)=JJ	MATL 250
	DO 30 I=1,II	MATL 260
30	READ (1,1001) (MATRX(I,J),J=1,JJ)	MATL 270
	RETURN	MATL 280
1000	FORMAT(A4,4X,I2,I10)	MATL 290
1001	FORMAT(8F10.4)	MATL 300
	END	MATL 310
		MATL 320
		MATL 330

## APPENDIX A — Continued

### SUBROUTINE MAK

Description: Subroutine MAK moves an input matrix from its temporary location in MATRX to its proper location in X. Subroutines MATLD and EDIT have determined what the proper location is for each matrix.

Subroutine listing:

SUBROUTINE MAK(X,MATRX,MAX)	MAK	0
REAL X(MAX,1),MATRX(8,8)	MAK	10
CALL ASPIT(MATRX)	MAK	20
X(MAX,3)=MATRX(8,3)	MAK	30
X(MAX,1)=MATRX(8,1)	MAK	40
X(MAX,2)=MATRX(8,2)	MAK	50
II=MATRX(8,1)	MAK	60
JJ=MATRX(8,2)	MAK	70
DO 10 I=1,II	MAK	80
DO 10 J=1,JJ	MAK	90
10 X(I,J)=MATRX(I,J)	MAK	100
RETURN	MAK	110
END	MAK	120

# APPENDIX A — Continued

## SUBROUTINE DERIV

Description: Subroutine DERIV prints dimensional and nondimensional derivatives with labels. Arrays E and EE contain the characters " " or "\*" to indicate, when printed, that a particular derivative is either varying or fixed, respectively.

### Subroutine listing:

```

SUBROUTINE DERIV(LONG)
C PRINT DIMENSIONAL AND NON-DIMENSIONAL DERIVATIVES
COMMON /HEADNG/ LABELS,TITLE,JULIAN
COMMON /MATRIX/ A,B,AA,BB,AP,BF,D1,RI
COMMON /DIMENS/ C,CC,E,EE,WQS,THETN
DIMENSION C(3,3),CC(3,5),A(5,4),B(5,8),AP(4,4),AA(5,4),BB(5,8),
- BP(4,8),AN(3,4),BN(3,5),E(3,3),EE(3,5),D1(8,7)
REAL RI(5,4),LABELS(15),TITLE(20),LAB(3),LONLAB(3),LATLAB(3)
LOGICAL LONG
DATA F/1H /,G/1HC/,LATLAB/1HY,1HL,1HN/,LONLAB/1HN,1HM,1HA/
DO 10 I=1,3
LAB(I)=LATLAB(I)
DO 5 J=1,4
5 AN(I,J)=A(I,J)
DO 10 J=1,5
10 BN(I,J)=B(I,J)
IF(.NOT.LONG) GO TO 20
DO 15 I=1,3
LAB(I)=LONLAB(I)
AN(1,I)=-AN(1,I)
15 AN(3,I)=-AN(3,I)
DO 17 I=1,5
BN(1,I)=-BN(1,I)
17 BN(3,I)=-BN(3,I)
C WRITE DIMENSIONAL DERIVATIVES
20 WRITE(3,107)
WRITE(3,106)(LABELS(I),I=1,3),(LABELS(J),J=8,11)
WRITE(3,103)
- (F,LAB(I),(AN(I,J),E(I,J),J=1,3),(BN(I,J),EE(I,J),J=1,5),I=1,3)
C NON-DIMENSIONALIZE
DO 29 I=1,3
DO 25 J=1,5
25 BN(I,J)=BN(I,J)*CC(I,J)
DO 29 J=1,3
29 AN(I,J)=AN(I,J)*C(I,J)
IF(.NOT.LONG) AN(1,2)=0.
WRITE(3,101)
WRITE(3,106)(LABELS(I),I=1,3),(LABELS(J),J=8,11)
WRITE(3,103)
- (G,LAB(I),(AN(I,J),E(I,J),J=1,3),(BN(I,J),EE(I,J),J=1,5),I=1,3)
WRITE(3,108)
101 FORMAT(48HNON-DIMENSIONAL DERIVATIVES / DEG (ROTARY /RAD))
103 FORMAT(11X,2A1,8(F14.6,A1,1X))
106 FORMAT(7(11X,A5),11X,7HDELTA-0)
107 FORMAT(39HDIMENSIONAL DERIVATIVES / SEC / SEC**2)
108 FORMAT(/40X,50H( * ; INDICATES DERIVATIVE HELD FIXED DURING MATCH)
RETURN
END
DERI 0
DERI 10
DERI 20
DERI 30
DERI 40
DERI 50
DERI 60
DERI 70
DERI 80
DERI 90
DERI 100
DERI 110
DERI 120
DERI 130
DERI 140
DERI 150
DERI 160
DERI 170
DERI 180
DERI 190
DERI 200
DERI 210
DERI 220
DERI 230
DERI 240
DERI 250
DERI 260
DERI 270
DERI 280
DERI 290
DERI 300
DERI 310
DERI 320
DERI 330
DERI 340
DERI 350
DERI 360
DERI 370
DERI 380
DERI 390
DERI 400
DERI 410
DERI 420
DERI 430
DERI 440
DERI 450
DERI 460
DERI 470

```



## APPENDIX A — Continued

### SUBROUTINE CRAMER

Description: Subroutine CRAMER computes confidence levels based on Cramér-Rao bounds.

Programing notes: The comment cards trace the steps of the subroutine. Note the manipulation of the SUM matrix required to store the second gradient (Hessian) with the *a priori* terms included, while also using the second gradient without the *a priori* terms for the confidence level computation.

Subroutine listing:

C	SUBROUTINE CRAMER(SUM, APRD, MU, MZ, ERRSUM)	GRAM 0
C	COMPUTES CRAMER RAO BOUNDS (CONFIDENCE LEVELS)	GRAM 10
C	COMMON /ALLODIM/ MAX, MIX	GRAM 20
	COMMON /MATRIX/ A, B, AA, BB, AP, BP, D1, RI	GRAM 30
	COMMON /ROUTH/ PUNCH, PARAM, MACH, ALP, CC, AC, BC	GRAM 40
	DIMENSION A(5,4), B(5,8), AA(5,4), BB(5,8), AP(4,4), BP(4,8), D1(8,7),	GRAM 50
	SUM(35,35), AC(5,4), BC(5,8), APRD(35), RI(5,4)	GRAM 60
	LOGICAL AA, BB, PUNCH	GRAM 70
	DATA ACL/2HAC/, BCL/2HBC/	GRAM 80
	AC(5,1)=3.	GRAM 90
	AC(5,2)=3.	GRAM 100
	BC(5,1)=3.	GRAM 110
	BC(5,2)=5.	GRAM 120
	AC(5,3)=ACL	GRAM 130
	BC(5,3)=BCL	GRAM 140
	JKMM1=SUM(MAX,1)	GRAM 150
	JK2=JKMM1-1	GRAM 160
	C***** SUBTRACT OUT APRIORI CONTRIBUTION TO HESSIAN	GRAM 170
	C***** STORE COMPLETE HESSIAN TEMPORARILY IN	GRAM 180
	C***** APRIORI LOCATIONS (UPPER TRIANGULAR) SINCE LAST	GRAM 190
	C***** USE HAS BEEN MADE OF IT.	GRAM 200
	TEMP=SUM(JKMM1, JKMM1)	GRAM 210
	SUM(JKMM1, JKMM1)=SUM(JKMM1, JKMM1)-APRD(JKMM1)	GRAM 220
	APRD(JKMM1)=TEMP	GRAM 230
	DO 10 I=1, JK2	GRAM 240
	TEMP=SUM(I, I)	GRAM 250
	SUM(I, I)=SUM(I, I)-APRD(I)	GRAM 260
	APRD(I)=TEMP	GRAM 270
	IP1=I+1	GRAM 280
	DO 10 J=IP1, JKMM1	GRAM 290
	TEMP=SUM(J, I)	GRAM 300
	SUM(J, I)=SUM(J, I)-SUM(I, J)	GRAM 310
	10 SUM(I, J)=TEMP	GRAM 320
	C***** OBTAIN DIAGONAL ELEMENTS OF INVERSE	GRAM 330
	CALL DIAGIN(SUM)	GRAM 340
	C***** COMPUTE BOUNDS	GRAM 350
	WTS = 0.0	GRAM 360
	DO 30029 I = 1, M7	GRAM 370
	IF (D1(I, I).NE.0.0) WTS = WTS + 1.0	GRAM 380
	30029 CONTINUE	GRAM 390
	COEFF = ERRSUM / WTS	GRAM 400
	L=0	GRAM 410
	DO 71 I=1, 3	GRAM 420
	DO 60 J=1, MU	GRAM 430
	BC(I, J)=0.	GRAM 440
	IF (BB(I, J) ) GO TO 60	GRAM 450
	L=L+1	GRAM 460
	BC(I, J)=SQRT(ABS(SUM(L, L))*COEFF)	GRAM 470
	60 CONTINUE	GRAM 480
	DO 70 J=1, 3	GRAM 490
	AC(I, J)=0.	GRAM 500
	IF (AA(I, J) ) GO TO 70	GRAM 510
	L=L+1	GRAM 520
	AC(I, J)=SQRT(ABS(SUM(L, L))*COEFF)	GRAM 530
	70 CONTINUE	GRAM 540
		GRAM 550
		GRAM 560

# APPENDIX A — Continued

IF(.NOT.AA(I,4)) L=L+1	GRAM 570
71 CONTINUE	GRAM 580
C***** RESTORE COMPLETE HESSIAN TO LOWER TRIANGULAR PART	GRAM 590
SUM(JKMH1,JKMH1)=APRD(JKMH1)	GRAM 600
DO 80 I=1,JK2	GRAM 610
SUM(I,I)=APRD(I)	GRAM 620
IP1=I+1	GRAM 630
DO 80 J=IP1,JKMH1	GRAM 640
80 SUM(J,I)=SUM(I,J)	GRAM 650
RETURN	GRAM 660
END	GRAM 670

## APPENDIX A – Continued

### SUBROUTINE AEAT

Description: Subroutine AEAT computes  $e^{A\Delta t}$  and  $\int_0^{\Delta t} e^{A\tau} d\tau$  using the Taylor series expansion.

Programing notes: The computational method used when NEAT  $\neq 0$  is described in the NAMELIST option NEAT (item (26), p. 15). The two matrices desired are returned as PHI and APhi. A2 and A3 are temporary scratch storage.

Subroutine listing:

SUBROUTINE AEAT(A,TT,PHI,APHI,A2,A3,NEAT)	AEAT 0
COMMON /ALLOIM/ MAX,MIX	AEAT 10
DIMENSION A(1),PHI(1),A2(1),APHI(1),A3(1)	AEAT 20
MAX2 = MAX * 2	AEAT 30
II=A(MAX)	AEAT 40
PHI(MAX)=A(MAX)	AEAT 50
PHI(MAX2)=A(MAX)	AEAT 60
T=TT/(2.**NEAT)	AEAT 70
CALL AZOT(PHI)	AEAT 80
CALL AMAKE(APHI,PHI)	AEAT 90
MI=-MAX	AEAT 110
DO 1 I = 1,II	AEAT 120
MI=MI+MAX	AEAT 130
PHI(MI + I) = 1.	AEAT 140
1 CONTINUE	AEAT 150
CALL AMAKE(A2,PHI)	AEAT 160
G = 1.0	AEAT 170
DO 2 I=1,10	AEAT 180
BB = I	AEAT 190
G = G*T/BB	AEAT 200
CALL AADD(1.,APHI,G,A2,APHI)	AEAT 210
CALL AMULT(A,A2,A3)	AEAT 220
CALL AMAKE(A2,A3)	AEAT 230
CALL AADD(1.,PHI,G,A2,PHI)	AEAT 240
2 CONTINUE	AEAT 250
IF(NEAT.EQ.0) RETURN	AEAT 260
DO 20 I=1,NEAT	AEAT 270
CALL AMAKE(A2,PHI)	AEAT 280
CALL AMULT(A2,A2,PHI)	AEAT 290
MI=-MAX	AEAT 300
DO 10 J=1,II	AEAT 310
MI=MI+MAX	AEAT 320
10 A2(MI+J)=A2(MI+J)+1.	AEAT 330
CALL AMULT(A2,APHI,A3)	AEAT 340
CALL AMAKE(APHI,A3)	AEAT 350
20 CONTINUE	AEAT 360
RETURN	AEAT 370
END	AEAT 380

## APPENDIX A — Continued

### SUBROUTINE AMULT

Description: Subroutine AMULT computes  $C = A*B$ . The quantity C cannot be the same matrix as either A or B.

Subroutine listing:

SUBROUTINE AMULT(A,B,C)	AMUL 0
COMMON /ALLOIM/ MAX,MIX	AMUL 10
REAL A(1),B(1),C(1)	AMUL 20
MAX2=MAX*2	AMUL 30
MIX2=MIX*2	AMUL 40
II=A(MAX)	AMUL 50
C(MAX)=A(MAX)	AMUL 60
JJ=A(MAX2)	AMUL 70
KK=B(MIX2)	AMUL 80
C(MAX2)=B(MIX2)	AMUL 90
JE=(JJ-1)*MAX	AMUL 100
KE=(KK-1)*MAX	AMUL 110
DO 20 I=1,II	AMUL 120
KEND=KE+I	AMUL 130
JEND=JE+I	AMUL 140
L=1	AMUL 150
DO 20 K=I,KEND,MAX	AMUL 160
C(K)=0.	AMUL 170
JB=L	AMUL 180
DO 10 J=I,JEND,MAX	AMUL 190
C(K)=A(J)*B(JB)+C(K)	AMUL 200
10 JB=JB+1	AMUL 210
20 L=L+MIX	AMUL 220
RETURN	AMUL 230
END	AMUL 240

## APPENDIX A – Continued

### SUBROUTINE DMULT

Description: Subroutine DMULT multiplies XJI by a diagonal matrix D1.

Subroutine listing:

SUBROUTINE DMULT(XJI,D1,XJID1,JKM,MZ)	DMUL 0
REAL XJI(35,8),XJID1(35,7),D1(8,7)	DMUL 10
DO 10 I=1,MZ	DMUL 20
DO 10 J=1,JKM	DMUL 30
10 XJID1(J,I)=XJI(J,I)*D1(I,I)	DMUL 40
RETURN	DMUL 50
END	DMUL 60

### SUBROUTINE SUMULT

Description: Subroutine SUMULT adds the term  $XJID1 * XJI^*$  to the SUM matrix. Only the lower triangular elements are accumulated because the result must always be symmetrical.

Subroutine listing:

SUBROUTINE SUMULT(XJI,XJID1,SUM,JKM,MZ)	SUMU 0
REAL XJI(35,8),XJID1(35,7),SUM(35,35)	SUMU 10
DO 10 I=1,JKM	SUMU 20
DO 10 J=1,I	SUMU 30
DO 10 K=1,MZ	SUMU 40
10 SUM(I,J)=SUM(I,J)+XJID1(I,K)*XJI(J,K)	SUMU 50
RETURN	SUMU 60
END	SUMU 70

## APPENDIX A — Continued

### SUBROUTINE PLOP

Description: Subroutine PLOP punches a matrix on cards.

Subroutine listing:

SUBROUTINE PLOP(X)	PLOP 0
COMMON /ALLOIM/ MAX,MIX	PLOP 10
DIMENSION X(1)	PLOP 20
102 FORMAT (8F10.6)	PLOP 30
103 FORMAT(A4,4X,I2,I10)	PLOP 40
MAX2=MAX+MAX	PLOP 50
MAX3=MAX2+MAX	PLOP 60
II=X(MAX)	PLOP 70
JJ=X(MAX2)	PLOP 80
WRITE(2,103)X(MAX3),II,JJ	PLOP 90
KE=(JJ-1)*MAX	PLOP 100
DO 2 I=1,II	PLOP 110
KEND=I+KE	PLOP 120
2 WRITE(2,102) (X(K),K=I,KEND,MAX)	PLOP 130
RETURN	PLOP 140
END	PLOP 150

### SUBROUTINE ASPIT

Description: Subroutine ASPIT prints a matrix.

Subroutine listing:

SUBROUTINE ASPIT(X)	ASPI 0
C WRITES OUT MATRICES	ASPI 10
COMMON /ALLOIM/ MAX,MIX	ASPI 20
DIMENSION X(1)	ASPI 30
100 FORMAT(1X,A4,30X,I3,4H 8Y,I3)	ASPI 40
101 FORMAT (12X,10E12.4)	ASPI 50
MAX2 = MAX * 2	ASPI 60
MAX3=MAX2+MAX	ASPI 70
II=X(MAX)	ASPI 80
JJ=X(MAX2)	ASPI 90
WRITE(3,100)X(MAX3),II,JJ	ASPI 100
KE=(JJ-1)*MAX	ASPI 110
DO 1 I =1,II	ASPI 120
KEND=I+KE	ASPI 130
1 WRITE(3,101) (X(K),K=I,KEND,MAX)	ASPI 140
RETURN	ASPI 150
END	ASPI 160

## APPENDIX A – Continued

### SUBROUTINE AADD

Description: Subroutine AADD adds scalar multiples of two matrices.  
 $Z = g*X + h*Y$  with  $g = 1$ .

Subroutine listing:

C	SUBROUTINE AADD (G,X,H,Y,Z)	AADD	0
	SPECIALIZED VERSION FOR NR ASSUMES G=1.	AADD	10
	COMMON /ALLOIM/ MAX,MIX	AADD	20
	DIMENSION X(1),Y(1),Z(1)	AADD	30
	MAX2 = MAX * 2	AADD	40
	II = X(MAX)	AADD	50
	JJ = X(MAX2)	AADD	60
	JEND=(JJ-1)*MAX+1	AADD	70
	IIM1=II-1	AADD	80
	DO 53 J=1,JEND,MAX	AADD	90
	KEND=J+IIM1	AADD	100
	DO 53 K=J,KEND	AADD	110
53	Z(K)=X(K)+H*Y(K)	AADD	120
	Z(MAX)=X(MAX)	AADD	130
	Z(MAX2)=X(MAX2)	AADD	140
	RETURN	AADD	150
	END	AADD	160

### SUBROUTINE AZOT

Description: Subroutine AZOT sets all elements of a matrix to 0.

Subroutine listing:

	SUBROUTINE AZOT(X)	AZOT	0
	COMMON /ALLOIM/ MAX,MIX	AZOT	10
	DIMENSION X(1)	AZOT	20
	MAX2 = MAX * 2	AZOT	30
	IIM1=X(MAX)-1.	AZOT	40
	JJM1=X(MAX2)-1.	AZOT	50
	LEND=JJM1*MAX+1	AZOT	60
	DO 1 L=1,LEND,MAX	AZOT	70
	KEND=L+IIM1	AZOT	80
	DO 1 K=L,KEND	AZOT	90
1	X(K)=0.	AZOT	100
	RETURN	AZOT	110
	END	AZOT	120

## APPENDIX A — Continued

### SUBROUTINE AMAKE

Description: Subroutine AMAKE moves the matrix Y into X.

Subroutine listing:

SUBROUTINE AMAKE(X,Y)	AMAK	0
COMMON /ALLOIM/ MAX,MIX	AMAK	10
DIMENSION X(1),Y(1)	AMAK	20
MAX2 = MAX * 2	AMAK	30
IIM1=Y(MAX)-1.	AMAK	40
JJM1=Y(MAX2)-1.	AMAK	50
LEND=JJM1*MAX+1	AMAK	60
DO 1 L=1,LEND,MAX	AMAK	70
KEND=L+IIM1	AMAK	80
DO 1 K=L,KEND	AMAK	90
1 X(K)=Y(K)	AMAK	100
X(MAX)=Y(MAX)	AMAK	110
X(MAX2)=Y(MAX2)	AMAK	120
RETURN	AMAK	130
END	AMAK	140

### SUBROUTINE INV

Description: Subroutine INV inverts a general matrix in place.

Programing notes: Gauss elimination is used here; there is no pivoting, since this subroutine will be called only for a well-conditioned, near-diagonal matrix (the R matrix). See reference 9 for a discussion of this method.

Subroutine listing:

SUBROUTINE INV(A,MAX)	INV	0
C INVERTS A GENERAL MATRIX IN PLACE	INV	10
C NO PIVOTING (DIAGONAL ELEMENTS MUST BE NON-ZERO)	INV	20
DIMENSION A(MAX,1)	INV	30
N=A(MAX,1)	INV	40
DO 80 K=1,N	INV	50
BIGA=A(K,K)	INV	60
DO 50 I=1,N	INV	70
IF(I.EQ.K) GO TO 50	INV	80
A(I,K)=-A(I,K)/BIGA	INV	90
50 CONTINUE	INV	100
DO 60 I=1,N	INV	110
IF(I.EQ.K) GO TO 60	INV	120
DO 55 J=1,N	INV	130
IF (J.EQ.K) GO TO 55	INV	140
A(I,J)=A(I,J)+A(I,K)*A(K,J)	INV	150
55 CONTINUE	INV	160
60 CONTINUE	INV	170
DO 70 J=1,N	INV	180
IF(J.EQ.K) GO TO 70	INV	190
A(K,J)=A(K,J)/BIGA	INV	200
70 CONTINUE	INV	210
80 A(K,K)=1./BIGA	INV	220
RETURN	INV	230
END	INV	240



## APPENDIX A – Continued

### SUBROUTINE SOLVE

Description: Subroutine SOLVE solves the system of linear equations,  $Ax = b$ , where A is symmetrical. It uses Cholesky's matrix decomposition. (See programing notes for subroutine REDUCE.) Only the lower triangular and diagonal elements of A are used.

Programing notes: The  $b$  vector is assumed to be stored as the  $N + 1$  column of A, where N is the dimension of the system.

Subroutine listing:

SUBROUTINE SOLVE(A,X)	SOLV   0
C	SOLV   10
C      SOLVES SYSTEM AX=B (A SYMMETRIC, B STORED IN N+1 COLUMN OF A)	SOLV   20
C	SOLV   30
REAL A(35,1),X(35)	SOLV   40
CALL REDUCE (A)	SOLV   50
N=A(35,1)	SOLV   60
NM1=N-1	SOLV   70
NP1=N+1	SOLV   80
C***** MULTIPLY (L)*(B)	SOLV   90
DO 70 I=2,N	SOLV 100
X(I)=A(I,NP1)	SOLV 110
IM1=I-1	SOLV 120
DO 70 J=1,IM1	SOLV 130
70 X(I)=X(I)+A(I,J)*A(J,NP1)	SOLV 140
C***** MULTIPLY BY (DI)	SOLV 150
A(1,NP1)=A(1,NP1)/A(1,1)	SOLV 160
DO 80 I=2,N	SOLV 170
80 A(I,NP1)=X(I)/A(I,I)	SOLV 180
C***** MULTIPLY BY (L*) TO FORM (L*)*(DI)*(L)*(B)	SOLV 190
DO 90 I=1,NM1	SOLV 200
X(I)=A(I,NP1)	SOLV 210
IP1=I+1	SOLV 220
DO 90 J=IP1,N	SOLV 230
90 X(I)=X(I)+A(J,I)*A(J,NP1)	SOLV 240
X(N)=A(N,NP1)	SOLV 250
RETURN	SOLV 260
END	SOLV 270

## APPENDIX A – Continued

### SUBROUTINE DIAGIN

Description: Subroutine DIAGIN obtains the diagonal elements of the inverse of a symmetric matrix. It uses Cholesky's decomposition of the matrix. (See subroutine REDUCE programming notes.)

Subroutine listing:

	SUBROUTINE DIAGIN(A)	DIAG 0
C		DIAG 10
C	FIND DIAGONAL ELEMENTS OF A INVERSE FOR SYMMETRIC A	DIAG 20
C		DIAG 30
	REAL A(35,1)	DIAG 40
	CALL REDUCE (A)	DIAG 50
	N=A(35,1)	DIAG 60
	NM1=N-1	DIAG 70
	DO 90 I=1,NM1	DIAG 80
	A(I,I)=1./A(I,I)	DIAG 90
	IP1=I+1	DIAG 100
	DO 90 J=IP1,N	DIAG 110
90	A(I,I)=A(I,I)+A(J,I)**2/A(J,J)	DIAG 120
	A(N,N)=1./A(N,N)	DIAG 130
	RETURN	DIAG 140
	END	DIAG 150

## APPENDIX A — Continued

### SUBROUTINE REDUCE

Description: Subroutine REDUCE factors a symmetric matrix A by Cholesky's matrix decomposition.

Programing notes: The matrix is factored into  $L^{-1}DL^{-1*}$ , where L is the lower diagonal with unity diagonal elements, and D is diagonal. The lower diagonal, L, is returned in the lower triangular locations of A, except for the diagonal locations, which contain D.

Subroutine listing:

C	SUBROUTINE REDUCE(A)	REDU	0
C		REDU	10
C	REDUCES SYMMETRIC MATRIX A STORED IN LOWER TRIANGULAR LOCATIONS	REDU	20
C	TO THE FORM (LI)*(D)*(LI*) WHERE L IS A LOWER TRIANGULAR MATRIX	REDU	30
C	WITH UNITY DIAGONAL TERMS, D IS A DIAGONAL MATRIX,	REDU	40
C	I DENOTES INVERSE AND * TRANSPOSE	REDU	50
C		REDU	60
	REAL A(35,1)	REDU	70
	N=A(35,1)	REDU	80
	NM1=N-1	REDU	90
	DO 20 K=1,NM1	REDU	100
	KP1=K+1	REDU	110
	KM1=K-1	REDU	120
	AKKI=1./A(K,K)	REDU	130
	DO 20 I=KP1,N	REDU	140
	AKKIK=A(I,K)*AKKI	REDU	150
	DO 10 J=I,N	REDU	160
	10 A(J,I)=A(J,I)-AKKIK*A(J,K)	REDU	170
	A(I,K)=-AKKIK	REDU	180
	IF(KM1.EQ.0) GO TO 20	REDU	190
	DO 15 J=1,KM1	REDU	200
	15 A(I,J)=A(I,J)-AKKIK*A(K,J)	REDU	210
	20 CONTINUE	REDU	220
	C***** L IS NOW STORED IN LOWER TRIANGULAR PART OF A	REDU	230
	C***** EXCEPT FOR DIAGONAL, WHICH CONTAINS D	REDU	240
	RETURN	REDU	250
	END	REDU	260

## APPENDIX A — Continued

### SUBROUTINE SCALES

**Description:** Subroutine SCALES determines scales for plotting the vector X on an axis S inches long. If the formal parameter ZERO is true, 0 must be included in the scale.

**Programing notes:** The minimum value on the axis is returned in location X(N + 1), and the scale in units per inch is returned in location X(N + 2). The only scales permitted are 2, 4, and 10 units per inch times a multiple of 10. A -999. is returned to indicate that all values of X are the same.

Subroutine listing:

SUBROUTINE SCALES(X,S,N,ZERO)	SCAL 0
LOGICAL ZERO	SCAL 10
REAL X(1),FAC(3)	SCAL 20
DATA FAC/2.,4.,10./	SCAL 30
XMAX=X(1)	SCAL 40
XMIN=X(1)	SCAL 50
IF(.NOT.ZERO) GO TO 10	SCAL 60
XMAX=0.	SCAL 70
XMIN=0.	SCAL 80
10 DO 20 I=1,N	SCAL 90
XMAX=AMAX1(XMAX,X(I))	SCAL 100
20 XMIN=AMIN1(XMIN,X(I))	SCAL 110
A=XMAX-XMIN	SCAL 120
IF(A.NE.0.) GO TO 30	SCAL 130
SCALE=-999.	SCAL 140
GO TO 100	SCAL 150
30 B=A/S	SCAL 160
J=IFIX(ABS(ALOG10(B)))	SCAL 170
IF(B.LT.1.) J=-J-1	SCAL 180
FACT=10.**J	SCAL 190
B=B/FACT	SCAL 200
DO 50 I=1,3	SCAL 210
SCALE=FACT*FAC(I)	SCAL 220
AMIN=XMIN-AMOD(XMIN,SCALE)	SCAL 230
IF(AMIN.GT.XMIN) AMIN=AMIN-SCALE	SCAL 240
IF((XMAX-AMIN).LE.SCALE*S) GO TO 100	SCAL 250
50 CONTINUE	SCAL 260
SCALE=10.*FACT*FAC(1)	SCAL 270
AMIN=XMIN-AMOD(XMIN,SCALE)	SCAL 280
IF(AMIN.GT.XMIN) AMIN=AMIN-SCALE	SCAL 290
100 X(N+1)=AMIN	SCAL 300
X(N+2)=SCALE	SCAL 310
RETURN	SCAL 320
END	SCAL 330

## APPENDIX A — Continued

### SUBROUTINE LINES

Description: Subroutine LINES plots solid or dashed lines or symbols of the X-axis versus the Y-axis.

Programing notes: The quantities X and Y are assumed to have scaling information in locations NPT + 1 and NPT + 2 as placed there by subroutine SCALES or other sources. Every ISKIP point of the data is used, and the sign of ISKIP determines whether the plot is to be made starting from the lower numbered locations in the arrays (positive sign) or the higher numbered locations (negative sign). If JSKIP = 0, a solid line is plotted; if positive, a solid line is plotted with symbols every JSKIP<sup>th</sup> point. If JSKIP = -1, only symbols are plotted. A dashed line may be plotted using JSKIP = -2. The quantity L indicates the symbol to be plotted if relevant, and HGT gives its height.

Subroutine listing:

	SUBROUTINE LINES(X,Y,NPT,ISKIP,JSKIP,L)	LINE 0
C	ISKIP=+ PLOT FORWARD,- BACKWARDS	LINE 10
C	JSKIP= 0 LINE ONLY,+ LINE AND SYMBOLS, - SYMBOLS ONLY OR DASHED	LINE 20
	COMMON /LINCOM/ HGT	LINE 30
	REAL X(1),Y(1)	LINE 40
	LOGICAL SYMB	LINE 50
	IF (ABS(HGT-.5).GE.,.5) HGT=.07	LINE 60
	XMIN=X(NPT+1)	LINE 70
	YMIN=Y(NPT+1)	LINE 80
	DX=X(NPT+2)	LINE 90
	DY=Y(NPT+2)	LINE 100
	IS=ABS(ISKIP)	LINE 110
	N=(NPT-1)/IS+1	LINE 120
	NA=1	LINE 130
	IF (ISKIP.LT.,3) NA=IS*(N-1)+1	LINE 140
	JMOD=MAX0(IABS(JSKIP),1)*IS	LINE 150
	SYMB=.TRUE.	LINE 160
	IF (JSKIP.EQ.,0) SYMB=.FALSE.	LINE 170
	IL=-2	LINE 180
	IF (JSKIP.LT.,0) IL=-1	LINE 190
	CALL PLOT((X(NA)-XMIN)/DX,(Y(NA)-YMIN)/DY,3)	LINE 200
	DO 50 I=1,N	LINE 210
	IF (SYMB.AND.,MOD(NA-1,JMOD).EQ.,0) GO TO 30	LINE 220
	CALL PLOT((X(NA)-XMIN)/DX,(Y(NA)-YMIN)/DY,2)	LINE 230
	GO TO 50	LINE 240
30	CALL SYMBOL((X(NA)-XMIN)/DX,(Y(NA)-YMIN)/DY,HGT,L,0,IL)	LINE 250
50	NA=NA+ISKIP	LINE 260
	RETURN	LINE 270
	END	LINE 280

## APPENDIX A — Continued

### SUBROUTINE PLTDAT

Description: Subroutine PLTDAT is used to identify plots. It is machine specific for the date and time software. The subroutine may be altered to reflect the form of plot identification desired (or a null subroutine may be used).

#### Subroutine listing:

	SUBROUTINE PLTDAT(X,Y)	PLTD	0
	PLTD DATE AND TIME FOR PLOT IDENTIFICATION	PLTD	10
C	MACHINE SPECIFIC FOR DATE AND TIME SOFTWARE	PLTD	20
C	CALL SYMBOL(X,Y,.1,DATE(JULIAN),0,.10)	PLTD	30
	CALL SYMBOL(999.,Y,.1,TIME(SECOND),0,.10)	PLTD	40
	RETURN	PLTD	50
	END	PLTD	60

### FUNCTION TIME

Description: FUNCTION TIME is a dummy function to substitute for the TIME function available on CDC 6000/7000 systems. If using such a system, FUNCTION TIME may be removed; for other systems it may be rewritten to properly access the system time, or it may be retained. It is called only from subroutine PLTDAT.

#### Function listing:

	FUNCTION TIME(ARG)	ME(A	0
	DUMMY SUBROUTINE IF TIME NOT AVAILABLE	ME(A	10
C	DATA BLNK/1H /	ME(A	20
	ARG=BLNK	ME(A	30
	TIME=BLNK	ME(A	40
	RETURN	ME(A	50
	END	ME(A	60

### FUNCTION DATE

Description: FUNCTION DATE is a dummy function to substitute for the DATE function available on CDC 6000/7000 systems. As with FUNCTION TIME, FUNCTION DATE should be removed if using such a system and should be either rewritten or retained when used on other systems. It is called from subroutine PLTDAT and EDIT.

#### Function listing:

	FUNCTION DATE(ARG)	TE(A	0
	DUMMY SUBROUTINE IF DATE NOT AVAILABLE	TE(A	10
C	DATA BLNK/1H /	TE(A	20
	ARG=BLNK	TE(A	30
	DATE=BLNK	TE(A	40
	RETURN	TE(A	50
	END	TE(A	60

## APPENDIX A — Continued

### ASSEMBLER LANGUAGE SUBROUTINES

Since the program spends a large part of its time in matrix multiplication, the execution time may be reduced considerably by writing the two small matrix multiplication subroutines AMULT and SUMULT in efficient assembler language code. In the following listings these two subroutines are written in COMPASS for use on CDC systems. These particular subroutines should be usable on any 6000 or 7000 series CDC system with the FORTRAN EXTENDED compiler. (The RUN compiler has different subroutine linkage conventions.) The use of these subroutines in place of the FORTRAN routines will speed up the program by 20 percent to 25 percent. If extensive use on other systems is anticipated, it may be advisable to make assembler versions for them. Some FORTRAN optimizers may be efficient enough to negate the gain realized; the 20 percent to 25 percent improvement mentioned, however, is referenced to the highest level of optimization available with a CDC FORTRAN 4.0 compiler.

# APPENDIX A — Continued

## ASSEMBLY SUBROUTINE AMULT

Subroutine listing:

			IDENT	AMULT	
			ENTRY	AMULT	
			USE	CODE	
			USE	/ALLOIM/	
0		1	MAX	BSS 1	
1		1	MAM	BSS 1	
			USE	CODE	
0	0400400000 +		AMULT	EQ AMULT+400000B	
1	5140000000 C		SA4	MAX	
	5150000001 C		SA5	MAM	
2	63240		SB2	X4	MAX
	63350		SB3	X5	MAM
	6110777776		SB1	-1	-1
3	55211		SA2	A1-B1	B
	55321		SA3	A2-B1	C
	66421		SB4	B2+B1	MAX-1
	66631		SB6	B3+B1	MAM-1
4	53414		SA4	X1+B4	A(MAX,1)
	53526		SA5	X2+B6	B(MAM,1)
	10644		SB6	X4	
	53634		SA6	X3+B4	=C(MAX,1)
5	26444		UX4	B4,X4	
	22444		LX4	B4,X4	
	63541		SB5	X4+B1	II-1
	26555		UX5	B6,X5	
6	22565		LX5	B6,X5	
	63750		SB7	X5	JJ
	54553		SA5	A5+B3	B(MAM,2)
	10655		SB6	X5	
7	54662		SA6	A6+B2	=C(MAX,2)
	26045		UX0	B4,X5	
	22040		LX0	B4,X0	KK
	66410		SB4	B1	I=C FOR FIRST K
10	67441		SB4	B4-B1	I=I+1
	73714		SX7	X1+B4	
	66600		SB6	B0	J=0
	76600		SX6	B0	
11	93470		SA4	X7	A
	53526		SA5	X2+B6	B
	40445		FX4	X4*X5	A*B
	30664		FX6	X6*X4	+C
12	73772		SX7	X7+B2	STEP A
	67661		SB6	B6-B1	J=J+1
	0767000011 +		LT	B6,B7,LOOPJ	
13	24606		NX6	X6	
	53634		SA6	X3+B4	=C
	0745000010 +		LT	B4,B5,LOOPIK	
14	66410		SB4	B1	I=0
	73001		SX0	X0+B1	K=K+1
	73223		SX2	X2+B3	STEP B
	73332		SX3	X3+B2	STEP C
15	0310000010 +		NZ	X0,LOOPIK	
	0400000000 +		EQ	AMULT	
16			END		



# APPENDIX A — Continued ASSEMBLY SUBROUTINE SUMULT

Subroutine listing:

0		2	MAX	IDENT SUMULT	
				ENTRY SUMULT	
				USE /ALLOIM/	
				BSS 2	
				USE CODE	
0	0400400000 +		SUMULT	EQ SUMULT+400000B	
1	6110000001			SB1 1	1
				SA5 MAX	
2	63250			SB2 X5	
	10711			BX7 X1	XJI
				SA1 A1+1	XJID1
3	5021000001			SA2 A1+1	SUM
				SA4 A2+1	
4	53340			SA3 X4	
	63430			SB4 X3	JKM
				SA4 A4+B1	
				SA4 X4	
5	42445			IX4 X4*X5	
	63740			SB7 X4	MZ*MAX
				SB5 B0	
				SB3 X5+B1	MAX+1
6	73075		LOOPIK	SX0 X7+B5	LOC(XJI(K,1))
	53525			SA5 X2+B5	SUM(K,I)
				BX6 X5	
				SB6 B0	J=0
7	53406		LOOPJ	SA4 X0+B6	XJI(K,J)
	53516			SA5 X1+B6	XJI(I,J)
				FX5 X4*X5	
				FX6 X5*X6	
10	66662			SB6 B6+B2	J=J+1
	24606			NX6 X6	
				LT B6,B7,LOOPJ	
11	53625			SA6 X2+B5	=SUM(I,K)
	66551			SB5 B5+B1	K=K+1
				LT B5,B4,LOOPIK	
12	66500			SB5 B0	RESTART K
	67441			SB4 B4-B1	LOWER K LIMIT I=I+1
				SX1 X1+B1	STEP LOC(XJI(I,1))
				SX2 X2+B3	STEP SUM LOC TO DIAGONAL
13	73771			SX7 X7+B1	
				LT B0,B4,LOOPIK	
14	0400000000 +			EQ SUMULT	
15				END	

## APPENDIX A — Concluded

### SEGMENTATION

Although the MMLE program does not require OVERLAY or SEGMENTATION to fit on most large computers, it is usually desirable to segment the program to decrease the load on the system. The following SEGMENTATION directives are used on the CDC OPERATING SYSTEM SCOPE 3.4 to reduce the loaded program size from 74,000<sub>8</sub> words to 52,000<sub>8</sub> words (including all buffers and system routines for input/output). The cost in execution time is negligible. The structure illustrated by these directives may be used as a guide for implementing the MMLE program on other systems.

PLTTREE	TREE	LINES- (THPLOT,APRPLT)
DATTREE	TREE	MATLD- (EDIT,DATA)
DOTREE	TREE	AEAT- (AGIRL,OUTPUT)
	TREE	MMLE- (PLTTREE,ASPIT- (DATTREE,DOTREE))
LINES	GLOBAL	LINCOM
ASPIT	GLOBAL	TOGIRL,INFO,TODATA,ROUTH,DIMENS
	GLOBAL	ALLDIM,BUF,MATRIX,COM,TOPLOT,HEADNG
	END	

## APPENDIX B

### SAMPLE CHECK CASE FOR MMLE PROGRAM

This appendix presents a sample check case for the MMLE program. This listing is intended to aid the user in checking out the MMLE program; therefore, many of the available options have not been used.

#### INPUT CARDS

```

AIRCRAFT A CHECK CASE
$INPUT CARD=T,Q=520.,V=4665., $END
0 0 0 0 0 0 5875
A      4      4
-0.038   0.111   -1.0   0.0169
-16.79   -0.241   0.4   0.0
1.55     -0.00284  -0.042  0.0
      1.
B      4      5
      .0148
12.76    20.08
.3577    -2.445

D1      7
2160.    6.5    4860.    135.    22.65    2.7    198.
ENDCASE
0 0 0 25    .7200    2.0000    .2808    .7999    .0150    -5.0024    -.2006
-1.7300    .0800    0.0000    0.0000
0 0 0 50    .6800    2.0000    .2808    .7999    .0150    -5.0023    -.3495
-.8000    .0800    0.0000    0.0000
0 0 0 75    .6500    1.9996    .2922    .9002    .0150    -4.7500    -.5503
-.8700    .1400    0.0000    0.0000
0 0 0 100   .6300    1.5015    .2808    .9002    .0150    -4.2519    -.8020
-.9200    .2200    0.0000    0.0000
0 0 0 125   .6200    1.5012    .2521    .9002    .0150    -3.7474    -1.0487
-.9750    .3500    0.0000    0.0000
0 0 0 150   .6200    1.5015    .2292    .9002    .0150    -2.4985    -1.3984
-1.0200    .6000    0.0000    0.0000
0 0 0 175   .6200    1.5012    .2005    .9999    .0200    -1.2491    -1.7017
-1.0650    .8500    0.0000    0.0000
0 0 0 200   .6300    1.7476    .1490    .9999    .0230    1.0026    -2.0513
-1.1100    1.0800    0.0000    0.0000
0 0 0 225   .6500    1.9999    .0515    .9999    .0250    3.5008    -2.4522
-1.1300    1.3300    0.0000    0.0000
0 0 0 250   .7000    2.2979    .0000    .9999    .0300    5.7451    -2.8991
-1.1650    1.5500    0.0000    0.0000
0 0 0 275   .7200    2.4984    -.0516    .9999    .0350    8.2507    -3.3007
-1.1900    1.7400    0.0000    0.0000
0 0 0 300   .7500    3.0022    -.1490    1.3001    .0420    11.9998    -3.7018
-1.2200    1.9400    0.0000    0.0000
0 0 0 325   .7800    3.5011    -.2292    1.3998    .0440    15.0034    -4.1483
-1.2450    2.1000    0.0000    0.0000
0 0 0 350   .8000    3.7989    -.3495    1.5001    .0440    16.5007    -4.5322
-1.2700    2.2400    0.0000    0.0000
0 0 0 375   .8100    4.2001    -.4527    1.5001    .0470    18.5029    -4.8476
-1.2900    2.3700    0.0000    0.0000
0 0 0 400   .8300    4.4980    -.5672    1.6004    .0540    19.4973    -5.0995
-1.3100    2.4700    0.0000    0.0000
0 0 0 425   .8800    5.5005    -.6989    1.7001    .0540    20.0497    -5.4205
-1.3400    2.5400    0.0000    0.0000
0 0 0 450   .9200    5.9966    -.8194    1.8004    .0540    20.0510    -5.3002
-1.3550    2.6000    0.0000    0.0000
0 0 0 475   .9000    6.4995    -.9514    2.0003    .0540    20.0494    -5.4492
-1.3650    2.6400    0.0000    0.0000
0 0 0 500   1.0000    7.5012    -1.0487    2.2003    .0520    20.0510    -5.3002
-1.3700    2.6500    0.0000    0.0000
0 0 0 525   1.0300    7.9976    -1.2494    2.3000    .0520    19.9953    -5.1512
-1.3800    2.6550    0.0000    0.0000
0 0 0 550   1.1200    8.4944    -1.3808    2.5000    .0490    18.9998    -5.0024
-1.3850    2.6400    0.0000    0.0000
0 0 0 575   1.1800    9.4035    -1.5014    2.7000    .0440    17.9991    -4.8015
-1.3900    2.6000    0.0000    0.0000

```

# APPENDIX B — Continued

0 0 0 600	1.2300	9.5014	-1.6500	3.0002	.0400	15.9962	-4.5497
-1.4000	2.5600	0.0000	0.0000				
0 0 0 625	1.2800	9.9975	-1.7820	3.5005	.0300	13.5011	-4.2514
-1.4050	2.4800	0.0000	0.0000				
0 0 0 650	1.3500	10.1966	-1.9193	3.7004	.0230	9.9978	-3.9022
-1.4100	2.3800	0.0000	0.0000				
0 0 0 675	1.4000	10.4995	-1.9999	4.0001	.0200	6.2493	-3.4495
-1.4150	2.2600	0.0000	0.0000				
0 0 0 700	1.4500	13.8021	-2.0971	4.3004	-.0010	1.5014	-3.0486
-1.4150	2.1200	0.0000	0.0000				
0 0 0 725	1.5500	11.2024	-2.1776	4.5003	-.0090	-3.0025	-2.5500
-1.4150	1.9700	0.0000	0.0000				
0 0 0 750	1.6300	11.0014	-2.2173	4.7003	-.0160	-7.9986	-2.0513
-1.4150	1.7600	0.0000	0.0000				
0 0 0 775	1.7200	10.8002	-2.2805	5.0006	-.0330	-13.4995	-1.5013
-1.4150	1.5500	0.0000	0.0000				
0 0 0 800	1.8000	10.4960	-2.3208	5.3002	-.0640	-18.5019	-.9510
-1.4200	1.3400	0.0000	0.0000				
0 0 0 825	1.8800	10.1975	-2.3720	5.5002	-.0710	-23.7513	-.4524
-1.4230	1.0800	0.0000	0.0000				
0 0 0 850	1.9800	9.4984	-2.3777	5.9019	-.0880	-29.0006	.0516
-1.4250	.8400	0.0000	0.0000				
0 0 0 875	2.0200	8.4954	-2.3893	5.9993	-.1140	-33.9995	.4011
-1.4250	.6400	0.0000	0.0000				
0 0 0 900	2.1000	7.4985	-2.3781	5.9993	-.1360	-38.4998	.7506
-1.4250	.4800	0.0000	0.0000				
0 0 0 925	2.2000	6.4958	-2.3662	6.1999	-.1460	-41.4997	1.0027
-1.4250	.4100	0.0000	0.0000				
0 0 0 950	2.2300	5.2031	-2.3610	6.3030	-.1620	-44.4998	1.2492
-1.4250	.3400	0.0000	0.0000				
0 0 0 975	2.3200	3.9993	-2.3492	6.4978	-.1770	-46.4981	1.3984
-1.4230	.3000	0.0000	0.0000				
0 0 1 000	2.3900	2.8022	-2.2975	6.4978	-.1890	-48.4971	1.4782
-1.4200	.2600	0.0000	0.0000				
0 0 1 025	2.4300	1.5013	-2.2520	6.4978	-.1890	-50.4962	1.5529
-1.4150	.2500	0.0000	0.0000				
0 0 1 050	2.5200	.2980	-2.2002	6.4978	-.1960	-51.5039	1.6273
-1.4100	.2400	0.0000	0.0000				
0 0 1 075	2.6000	-1.0029	-2.1490	6.3030	-.2100	-53.0045	1.7018
-1.4000	.2200	0.0000	0.0000				
0 0 1 100	2.6300	-2.4985	-2.0969	6.3030	-.2200	-53.7489	1.7476
-1.4000	.2000	0.0000	0.0000				
0 0 1 125	2.6800	-3.7014	-1.9998	6.3030	-.2250	-54.4991	1.7991
-1.3900	.1900	0.0000	0.0000				
0 0 1 150	2.7200	-5.0022	-1.9481	6.3030	-.2290	-55.0028	1.8509
-1.3650	.1800	0.0000	0.0000				
0 0 1 175	2.7800	-6.4956	-1.9123	6.3030	-.2390	-55.5006	1.9193
-1.3400	.1750	0.0000	0.0000				
0 0 1 200	2.8000	-7.6984	-1.8510	6.1999	-.2340	-55.7462	1.9884
-1.3000	.1700	0.0000	0.0000				
0 0 1 225	2.8300	-9.0027	-1.7818	5.9993	-.2440	-55.9981	2.0112
-1.2600	.1650	0.0000	0.0000				
0 0 1 250	2.8500	-10.3046	-1.7475	5.7988	-.2460	-55.9980	2.0283
-1.2150	.1600	0.0000	0.0000				
0 0 1 275	2.8900	-11.5018	-1.7020	5.7002	-.2460	-55.7456	2.0514
-1.1600	.1550	0.0000	0.0000				
0 0 1 300	2.9000	-13.0020	-1.5989	5.0006	-.2480	-55.4990	2.0683
-1.1100	.1500	0.0000	0.0000				
0 0 1 325	2.9500	-15.0014	-1.5528	4.5003	-.2480	-55.0003	2.0801
-1.0500	.1500	0.0000	0.0000				
0 0 1 350	2.9700	-16.3016	-1.5011	4.3004	-.2510	-54.4962	2.0684
-.9900	.1500	0.0000	0.0000				
0 0 1 375	2.9700	-17.6987	-1.3979	3.5005	-.2480	-53.9977	2.0625
-.9250	.1500	0.0000	0.0000				
0 0 1 400	2.9700	-19.1998	-1.3692	3.0002	-.2480	-53.7457	2.0012
-.8650	.1500	0.0000	0.0000				

# APPENDIX B — Continued

J 0 1 425	2.9500	-20.7978	-1.3006	2.5000	-.2480	-53.0010	2.0284
-.7900	.1500	0.0000	0.0000				
J 0 1 450	2.9300	-21.9947	-1.2322	2.0000	-.2480	-52.4968	2.0224
-.7300	.1500	0.0000	0.0000				
J 0 1 475	2.9200	-23.5012	-1.1805	1.5000	-.2460	-51.5000	1.9997
-.6700	.1500	0.0000	0.0000				
J 0 1 500	2.9000	-24.8013	-1.1173	.7999	-.2440	-49.9992	1.9481
-.6000	.1500	0.0000	0.0000				
J 0 1 525	2.8500	-26.0040	-1.0483	.3000	-.2440	-48.4983	1.9023
-.5400	.1500	0.0000	0.0000				
J 0 1 550	2.8000	-27.4991	-1.0025	-.5000	-.2390	-46.0004	1.8509
-.4700	.1500	0.0000	0.0000				
J 0 1 575	2.7500	-28.9999	-.9509	-.9999	-.2340	-42.4995	1.8220
-.4200	.1500	0.0000	0.0000				
J 0 1 600	2.6300	-30.5014	-.9681	-2.0000	-.2220	-39.5000	1.7819
-.3600	.1500	0.0000	0.0000				
J 0 1 625	2.5700	-31.8009	-.8482	-2.8000	-.2200	-36.2490	1.7118
-.3200	.1500	0.0000	0.0000				
J 0 1 650	2.4800	-33.1986	-.8023	-3.8000	-.2100	-33.4993	1.6271
-.2750	.1600	0.0000	0.0000				
J 0 1 675	2.3900	-34.4992	-.7792	-4.5000	-.2010	-30.0002	1.5817
-.2400	.1600	0.0000	0.0000				
J 0 1 700	2.3000	-35.4954	-.6992	-5.3000	-.1980	-26.9969	1.4785
-.2200	.1600	0.0000	0.0000				
J 0 1 725	2.2200	-36.4976	-.6478	-5.9993	-.1910	-24.0007	1.4098
-.2000	.1600	0.0000	0.0000				
J 0 1 750	2.1000	-37.7981	-.6190	-7.0021	-.1810	-21.9961	1.3178
-.1800	.1600	0.0000	0.0000				
J 0 1 775	2.0200	-39.0011	-.5786	-7.9991	-.1690	-19.0000	1.2319
-.1600	.1700	0.0000	0.0000				
J 0 1 800	1.9300	-39.5050	-.5503	-9.0018	-.1570	-16.5025	1.1519
-.1400	.1700	0.0000	0.0000				
J 0 1 825	1.8200	-40.5015	-.4984	-9.9988	-.1480	-13.7530	1.0485
-.1300	.1700	0.0000	0.0000				
J 0 1 850	1.7300	-40.9997	-.4587	-11.0016	-.1360	-11.2499	.9513
-.1200	.1700	0.0000	0.0000				
J 0 1 875	1.6300	-41.5036	-.4298	-11.9986	-.1290	-8.7470	.8311
-.1000	.1700	0.0000	0.0000				
J 0 1 900	1.5300	-41.5035	-.4183	-12.8008	-.1240	-6.2495	.7505
-.0900	.1700	0.0000	0.0000				
J 0 1 925	1.4300	-41.5032	-.3897	-13.4999	-.1050	-3.5012	.6477
-.0800	.1700	0.0000	0.0000				
J 0 1 950	1.3000	-40.9988	-.3784	-14.5026	-.0880	-1.2494	.5214
-.0600	.1700	0.0000	0.0000				
J 0 1 975	1.2200	-40.7982	-.3726	-15.8033	-.0810	1.0025	.4011
-.0500	.1700	0.0000	0.0000				
J 0 2 000	1.1200	-40.5000	-.3494	-16.5024	-.0640	3.5008	.2807
-.0400	.1700	0.0000	0.0000				
J 0 2 25	1.0100	-40.2993	-.3378	-17.2014	-.0520	6.0015	.1776
-.0250	.1700	0.0000	0.0000				
J 0 2 50	.9200	-39.8005	-.3208	-18.0036	-.0380	8.0001	.0516
-.0100	.1700	0.0000	0.0000				
J 0 2 75	.8000	-39.5023	-.2982	-19.0007	-.0300	9.9986	-.0802
0.0000	.1700	0.0000	0.0000				
J 0 2 100	.7000	-38.7975	-.2977	-20.0034	-.0180	11.9970	-.2177
.0100	.1700	0.0000	0.0000				
J 0 2 125	.6000	-38.0012	-.3211	-20.7999	-.0040	14.2533	-.3496
.0200	.1700	0.0000	0.0000				
J 0 2 150	.4700	-36.9985	-.3324	-21.4989	.0060	16.2523	-.4298
.0350	.1700	0.0000	0.0000				
J 0 2 175	.4000	-36.0016	-.3494	-22.5017	.0180	18.5027	-.5787
.0450	.1700	0.0000	0.0000				
J 0 2 200	.3000	-35.1997	-.3780	-23.5044	.0400	20.5013	-.6991
.0500	.1700	0.0000	0.0000				
J 0 2 225	.2200	-34.0022	-.3897	-24.0030	.0440	22.5001	-.8079
.0600	.1700	0.0000	0.0000				

# APPENDIX B – Continued

0 0 2 250	.1300	-33.3033	-.4127	-25.0000	.0520	24.4984	-.9509
.0650	.1700	0.0000	0.0000				
0 0 2 275	.0300	-32.0027	-.4300	-26.0027	.0640	25.5002	-1.0487
.0700	.1700	0.0000	0.0000				
0 0 2 300	-.0300	-30.7996	-.4526	-26.7992	.0730	27.4987	-1.1802
.0750	.1700	0.0000	0.0000				
0 0 2 325	-.1200	-29.4993	-.4986	-27.5040	.0860	28.9987	-1.3005
.0800	.1700	0.0000	0.0000				
0 0 2 350	-.1800	-28.5025	-.5213	-28.5010	.0980	30.9977	-1.3809
.0800	.1700	0.0000	0.0000				
0 0 2 375	-.2500	-27.5002	-.5670	-29.2001	.1070	31.9993	-1.5011
.0900	.1700	0.0000	0.0000				
0 0 2 400	-.3500	-26.3028	-.5901	-30.0023	.1190	33.4997	-1.5870
.0900	.1700	0.0000	0.0000				
0 0 2 425	-.4000	-25.5006	-.6016	-30.8045	.1290	34.2494	-1.6787
.0900	.1700	0.0000	0.0000				
0 0 2 450	-.4500	-23.9998	-.6474	-31.5035	.1360	35.4978	-1.7477
.0950	.1700	0.0000	0.0000				
0 0 2 475	-.5500	-22.9974	-.6817	-32.0020	.1410	36.2475	-1.8451
.1000	.1700	0.0000	0.0000				
0 0 2 500	-.5800	-21.6970	-.7219	-32.8042	.1480	36.9974	-1.9196
.1000	.1700	0.0000	0.0000				
0 0 2 525	-.6300	-20.5000	-.7794	-33.5033	.1560	37.4952	-1.9828
.1000	.1700	0.0000	0.0000				
0 0 2 550	-.6800	-19.6980	-.8123	-34.0018	.1600	38.4975	-2.0285
.1000	.1700	0.0000	0.0000				
0 0 2 575	-.7300	-18.4951	-.8479	-34.5003	.1650	38.7491	-2.0799
.0900	.1700	0.0000	0.0000				
0 0 2 600	-.7800	-17.0000	-.8994	-35.0045	.1700	39.0005	-2.1490
.0900	.1700	0.0000	0.0000				
0 0 2 625	-.8000	-15.9975	-.9227	-35.0045	.1700	39.5045	-2.1773
.0900	.1700	0.0000	0.0000				
0 0 2 650	-.8300	-14.5025	-.9800	-36.0016	.1730	40.0028	-2.2004
.0900	.1700	0.0000	0.0000				
0 0 2 675	-.8500	-13.5000	-1.0085	-36.3053	.1730	40.2489	-2.2289
.0900	.1700	0.0000	0.0000				
0 0 2 700	-.8800	-12.5033	-1.0484	-36.5001	.1820	40.5008	-2.2522
.0850	.1700	0.0000	0.0000				
0 0 2 725	-.9000	-11.5008	-1.0774	-36.7006	.1820	40.5009	-2.2407
.0800	.1700	0.0000	0.0000				
0 0 2 750	-.9500	-10.2008	-1.1515	-37.0043	.1850	40.7531	-2.2291
.0700	.1700	0.0000	0.0000				
0 0 2 775	-.9800	-9.5022	-1.1917	-37.2049	.1850	40.9995	-2.2289
.0600	.1700	0.0000	0.0000				
0 0 2 800	-.9000	-8.0011	-1.2203	-37.5028	.1850	40.9995	-2.2289
.0500	.1700	0.0000	0.0000				
0 0 2 825	-.9000	-6.9989	-1.2780	-37.6003	.1850	40.9997	-2.2174
.0350	.1700	0.0000	0.0000				
0 0 2 850	-.8800	-5.9966	-1.3180	-37.7034	.1850	40.9997	-2.2117
.0200	.1700	0.0000	0.0000				
0 0 2 875	-.8500	-5.0024	-1.3808	-37.8008	.1850	40.9998	-2.2002
.0100	.1700	0.0000	0.0000				
0 0 2 900	-.8200	-3.5013	-1.3980	-37.8008	.1850	41.0001	-2.1773
-.0100	.1700	0.0000	0.0000				
0 0 2 925	-.8000	-2.8021	-1.4324	-37.9039	.1800	41.0004	-2.1486
-.0300	.1700	0.0000	0.0000				
0 0 2 950	-.7800	-1.5014	-1.4498	-37.9039	.1800	40.7543	-2.1202
-.0400	.1700	0.0000	0.0000				
0 0 2 975	-.7700	-.8024	-1.5185	-37.9039	.1800	40.4969	-2.0802
-.0500	.1700	0.0000	0.0000				
0 0 3 000	-.7500	.2980	-1.5527	-37.8008	.1750	39.9986	-2.0514
-.0600	.1700	0.0000	0.0000				
0 0 3 025	-.7000	1.0025	-1.5814	-37.8008	.1750	39.5005	-2.0111
-.0700	.1700	0.0000	0.0000				
0 0 3 050	-.6500	1.9997	-1.6213	-37.8008	.1730	38.4980	-1.9826
-.0750	.1700	0.0000	0.0000				

# APPENDIX B – Continued

0 0 3 75	-.6300	3.0028	-1.6504	-37.7034	.1730	37.4959	-1.9198
-.0800	.1700	0.0000	0.0000				
0 0 3 100	-.6000	3.9996	-1.6788	-37.7034	.1700	36.4994	-1.8678
-.0850	.1700	0.0000	0.0000				
0 0 3 125	-.5500	4.6987	-1.7304	-37.5028	.1650	35.4972	-1.8107
-.0900	.1700	0.0000	0.0000				
0 0 3 150	-.5000	5.5007	-1.7476	-37.3023	.1600	33.4977	-1.7704
-.0950	.1700	0.0000	0.0000				
0 0 3 175	-.4300	6.2958	-1.7819	-37.0043	.1600	32.0029	-1.7117
-.1000	.1700	0.0000	0.0000				
0 0 3 200	-.3800	7.0004	-1.7992	-36.8038	.1480	30.5024	-1.6214
-.1000	.1700	0.0000	0.0000				
0 0 3 225	-.3300	7.7967	-1.8220	-36.7006	.1460	28.7493	-1.5815
-.1050	.1700	0.0000	0.0000				
0 0 3 250	-.2500	8.4955	-1.8507	-36.5001	.1410	27.0024	-1.5015
-.1100	.1700	0.0000	0.0000				
0 0 3 275	-.2000	9.2974	-1.8793	-36.3053	.1390	25.4962	-1.4212
-.1100	.1700	0.0000	0.0000				
0 0 3 300	-.1200	9.9963	-1.9023	-36.2021	.1270	23.9956	-1.3524
-.1150	.1700	0.0000	0.0000				
0 0 3 325	-.0500	10.5002	-1.9312	-36.0016	.1220	22.5008	-1.2780
-.1200	.1700	0.0000	0.0000				
0 0 3 350	0.0000	10.8037	-1.9482	-35.8010	.1170	21.0003	-1.1977
-.1230	.1700	0.0000	0.0000				
0 0 3 375	.0300	11.5026	-1.9711	-35.6005	.1100	19.4998	-1.1175
-.1240	.1700	0.0000	0.0000				
0 0 3 400	.1000	12.0011	-1.9770	-35.3025	.0980	17.9995	-1.0201
-.1250	.1700	0.0000	0.0000				
0 0 3 425	.1800	12.3047	-1.9826	-35.0045	.0950	16.2525	-.9509
-.1230	.1700	0.0000	0.0000				
0 0 3 450	.2500	12.7000	-1.9885	-34.5003	.0830	14.4999	-.8709
-.1200	.1700	0.0000	0.0000				
0 0 3 475	.3200	13.0038	-1.9883	-34.2998	.0760	13.4980	-.7794
-.1150	.1700	0.0000	0.0000				
0 0 3 500	.4000	13.5023	-1.9828	-34.0018	.0710	11.9977	-.6819
-.1100	.1700	0.0000	0.0000				
0 0 3 525	.4300	14.0009	-1.9824	-33.9044	.0640	10.4972	-.6016
-.1000	.1700	0.0000	0.0000				
0 0 3 550	.5300	14.3047	-1.9713	-33.8013	.0570	9.0027	-.4985
-.0900	.1700	0.0000	0.0000				
0 0 3 575	.6000	14.4021	-1.9712	-33.5033	.0490	7.5024	-.4011
-.0800	.1700	0.0000	0.0000				
0 0 3 600	.6500	14.5053	-1.9712	-33.0048	.0420	6.2541	-.3209
-.0700	.1700	0.0000	0.0000				
0 0 3 625	.7500	14.6028	-1.9596	-32.5005	.0400	5.0021	-.2806
-.0600	.1700	0.0000	0.0000				
0 0 3 650	.8300	14.6028	-1.9596	-31.9046	.0280	3.2486	-.0974
-.0400	.1700	0.0000	0.0000				
0 0 3 675	.9000	14.6946	-1.9480	-31.8015	.0200	1.7477	0.0000
-.0250	.1700	0.0000	0.0000				
0 0 3 700	.9800	14.5973	-1.9423	-31.5035	.0030	.2521	.0802
-.0100	.1700	0.0000	0.0000				
0 0 3 725	1.0300	14.5975	-1.9194	-31.0050	-.0010	-1.2490	.1777
.0100	.1700	0.0000	0.0000				
0 0 3 750	1.1200	14.5003	-1.9023	-30.5008	-.0090	-3.0027	.2693
.0250	.1700	0.0000	0.0000				
0 0 3 775	1.2000	14.3975	-1.8680	-30.3002	-.0140	-3.9997	.3782
.0500	.1700	0.0000	0.0000				
0 0 3 800	1.2700	14.3002	-1.8624	-30.0023	-.0330	-5.5008	.4526
.0700	.1700	0.0000	0.0000				
0 0 3 825	1.3500	13.9966	-1.8505	-29.8017	-.0380	-6.9960	.6016
.0900	.1700	0.0000	0.0000				
0 0 3 850	1.4000	13.6987	-1.8393	-29.5038	-.0470	-7.9980	.6821
.1200	.1700	0.0000	0.0000				
0 0 3 875	1.4700	13.5957	-1.8279	-29.3032	-.0570	-9.2459	.8020
.1400	.1700	0.0000	0.0000				

# APPENDIX B — Continued

0 0 3 900	1.5200	13.4983	-1.8223	-28.9995	-.0620	-11.0041	.8994
.1700	.1700	0.0000	0.0000				
0 0 3 925	1.6000	13.0000	-1.7992	-28.5010	-.0710	-11.9997	1.0315
.2100	.1700	0.0000	0.0000				
0 0 3 950	1.6300	12.5017	-1.7818	-28.0025	-.0810	-13.4998	1.1518
.2300	.1700	0.0000	0.0000				
0 0 3 975	1.7000	12.3015	-1.7476	-27.8019	-.0860	-14.5015	1.2491
.2700	.1700	0.0000	0.0000				
0 0 4 000	1.7800	11.9983	-1.7019	-27.7045	-.1020	-15.9961	1.3522
.3000	.1700	0.0000	0.0000				
0 0 4 025	1.8300	11.5003	-1.6502	-27.5043	-.1070	-17.0029	1.5068
.3000	.1700	0.0000	0.0000				
0 0 4 050	1.8800	11.0023	-1.5984	-26.9997	-.1140	-17.9992	1.5816
.3500	.1700	0.0000	0.0000				
0 0 4 075	1.9300	10.8021	-1.5699	-26.5012	-.1190	-19.4998	1.6504
.3800	.1700	0.0000	0.0000				
0 0 4 100	1.9800	10.4991	-1.5314	-26.3007	-.1340	-20.5013	1.7706
.4000	.1700	0.0000	0.0000				
0 0 4 125	2.0000	9.5019	-1.5068	-26.2033	-.1340	-21.4976	1.8506
.4250	.1700	0.0000	0.0000				
0 0 4 150	2.0200	9.0046	-1.3983	-26.0027	-.1360	-22.4989	1.9828
.4500	.1700	0.0000	0.0000				
0 0 4 175	2.0500	8.4951	-1.3521	-25.8996	-.1430	-23.0025	2.0512
.4720	.1700	0.0000	0.0000				
0 0 4 200	2.0800	7.9974	-1.2723	-25.5042	-.1550	-23.5000	2.1488
.4900	.1700	0.0000	0.0000				
0 0 4 225	2.1000	7.4996	-1.1977	-24.7994	-.1550	-23.6997	2.2288
.5100	.1700	0.0000	0.0000				
0 0 4 250	2.1500	6.8011	-1.1518	-24.5015	-.1570	-23.8023	2.2804
.5300	.1700	0.0000	0.0000				
0 0 4 275	2.1700	6.4982	-1.0718	-24.3009	-.1650	-23.8987	2.3777
.5500	.1700	0.0000	0.0000				
0 0 4 300	2.1800	6.0004	-1.0028	-24.2035	-.1720	-23.9956	2.4182
.5700	.1700	0.0000	0.0000				
0 0 4 325	2.2100	5.0024	-.9222	-24.0030	-.1740	-23.9951	2.4698
.5800	.1700	0.0000	0.0000				
0 0 4 350	2.2200	4.4978	-.8481	-23.8998	-.1740	-23.8971	2.5209
.6000	.1700	0.0000	0.0000				
0 0 4 375	2.2300	3.9994	-.7791	-23.8024	-.1790	-23.7480	2.5325
.6100	.1700	0.0000	0.0000				
0 0 4 400	2.2400	3.5012	-.6993	-23.8024	-.1810	-23.7018	2.5727
.6220	.1700	0.0000	0.0000				
0 0 4 425	2.2500	3.0026	-.6017	-23.8024	-.1840	-23.5014	2.5499
.6400	.1700	0.0000	0.0000				
0 0 4 450	2.2700	2.2977	-.5501	-23.8024	-.1810	-22.9975	2.5210
.6500	.1700	0.0000	0.0000				
0 0 4 475	2.2800	1.7991	-.4527	-23.8024	-.1810	-22.7456	2.4983
.6600	.1700	0.0000	0.0000				
0 0 4 500	2.2900	1.1976	-.3782	-23.8024	-.1860	-22.4996	2.4527
.6700	.1700	0.0000	0.0000				
0 0 4 525	2.3000	.8021	-.2808	-23.8024	-.1860	-21.9958	2.4180
.6750	.1700	0.0000	0.0000				
0 0 4 550	2.3200	.2980	-.2005	-24.0030	-.1860	-21.4977	2.3778
.6900	.1700	0.0000	0.0000				
0 0 4 575	2.3000	0.0000	-.1318	-24.0030	-.1840	-20.5009	2.3493
.7000	.1700	0.0000	0.0000				
0 0 4 600	2.3000	-.4985	-.0688	-24.1004	-.1840	-19.7509	2.2806
.7050	.1700	0.0000	0.0000				
0 0 4 625	2.3000	-1.0026	.0172	-24.2035	-.1810	-19.0011	2.2003
.7100	.1700	0.0000	0.0000				
0 0 4 650	2.3000	-1.5014	.0516	-24.3009	-.1810	-17.9991	2.1317
.7200	.1700	0.0000	0.0000				
0 0 4 675	2.2800	-1.9997	.1203	-24.5015	-.1790	-17.5014	2.0513
.7220	.1700	0.0000	0.0000				
0 0 4 700	2.2700	-2.4980	.2005	-24.7020	-.1720	-16.7514	1.9826
.7240	.1700	0.0000	0.0000				



# APPENDIX B – Continued

0 0 4 725	2.2500	-3.0025	.2292	-24.7994	-.1720	-15.9959	1.9023
.7300	.1700	0.0000	0.0000				
0 0 4 750	2.2000	-3.5011	.2808	-25.0000	-.1670	-14.7478	1.7990
.7350	.1750	0.0000	0.0000				
0 0 4 775	2.1500	-3.7989	.3495	-25.3037	-.1670	-14.2501	1.7192
.7400	.1750	0.0000	0.0000				
0 0 4 800	2.1200	-4.2975	.4011	-25.5042	-.1570	-13.5005	1.6217
.7450	.1750	0.0000	0.0000				
0 0 4 825	2.0700	-4.4983	.4298	-25.6016	-.1550	-12.5040	1.5698
.7500	.1750	0.0000	0.0000				
0 0 4 850	2.0300	-5.0020	.4813	-25.6990	-.1480	-12.0010	1.4498
.7500	.1750	0.0000	0.0000				
0 0 4 875	1.9800	-5.5006	.5271	-25.8022	-.1410	-11.1995	1.3811
.7500	.1750	0.0000	0.0000				
0 0 4 900	1.9500	-5.7987	.5673	-25.8996	-.1380	-9.9970	1.3006
.7500	.1750	0.0000	0.0000				
0 0 4 925	1.9000	-5.9989	.6016	-26.0027	-.1340	-9.0004	1.2492
.7500	.1750	0.0000	0.0000				
0 0 4 950	1.8500	-6.2967	.6188	-26.2033	-.1290	-7.9982	1.1978
.7550	.1750	0.0000	0.0000				
0 0 4 975	1.8300	-6.3996	.6472	-26.3007	-.1240	-7.0013	1.1803
.7600	.1750	0.0000	0.0000				
0 0 5 0	1.7500	-6.4966	.6821	-26.5012	-.1140	-6.2509	1.1516
.7630	.1750	0.0000	0.0000				
0 0 5 25	1.7000	-6.5993	.7222	-26.7992	-.1120	-5.5008	1.1001
.7650	.1750	0.0000	0.0000				
0 0 5 50	1.6500	-6.6963	.7679	-26.9023	-.1070	-4.2518	1.0770
.7680	.1750	0.0000	0.0000				
0 0 5 75	1.6000	-6.7990	.8022	-27.2003	-.1000	-3.0024	1.0487
.7700	.1750	0.0000	0.0000				
0 0 5 100	1.5500	-6.7989	.8194	-27.5040	-.0950	-1.5012	1.0315
.7700	.1750	0.0000	0.0000				
0 0 5 125	1.5200	-6.6956	.8309	-27.7045	-.0860	-.4985	1.0030
.7720	.1750	0.0000	0.0000				
0 0 5 150	1.4300	-6.6033	.8826	-27.8019	-.0810	1.0030	.9800
.7720	.1750	0.0000	0.0000				
0 0 5 175	1.4000	-6.5003	.8999	-28.0025	-.0760	2.4986	.9228
.7730	.1750	0.0000	0.0000				
0 0 5 200	1.3500	-6.2989	.9510	-28.0025	-.0670	3.9995	.8827
.7750	.1800	0.0000	0.0000				
0 0 5 225	1.3000	-6.0006	.9799	-28.2030	-.0620	5.9971	.8309
.7750	.1800	0.0000	0.0000				
0 0 5 250	1.2300	-5.7998	1.0030	-28.3004	-.0570	7.4983	.8194
.7800	.1800	0.0000	0.0000				
0 0 5 275	1.2000	-5.4949	1.0083	-28.4036	-.0570	9.3204	.8022
.7850	.1800	0.0000	0.0000				
0 0 5 300	1.1500	-5.2030	1.0315	-28.5010	-.0450	10.4950	.7908
.7880	.1800	0.0000	0.0000				
0 0 5 325	1.0800	-4.8017	1.0485	-28.7016	-.0350	11.4976	.7795
.7900	.1800	0.0000	0.0000				
0 0 5 350	1.0300	-3.9993	1.1172	-28.8047	-.0350	12.9987	.7508
.7900	.1800	0.0000	0.0000				
0 0 5 375	1.0000	-3.7989	1.1518	-28.9021	-.0280	14.5052	.6992
.7950	.1800	0.0000	0.0000				
0 0 5 400	.9800	-3.3006	1.1802	-28.9021	-.0230	15.5023	.6988
.8000	.1800	0.0000	0.0000				
0 0 5 425	.9200	-2.8019	1.1978	-28.9995	-.0210	16.5049	.6818
.8000	.1800	0.0000	0.0000				
0 0 5 450	.8800	-2.0000	1.2208	-28.9995	-.0180	18.0003	.6589
.8050	.1800	0.0000	0.0000				
0 0 5 475	.8300	-1.7019	1.2319	-29.1027	-.0140	18.7506	.6303
.8100	.1800	0.0000	0.0000				
0 0 5 500	.8000	-1.0026	1.2491	-28.9995	-.0060	20.2518	.6188
.8150	.1800	0.0000	0.0000				
0 0 5 525	.7500	-1.4985	1.2780	-28.9021	-.0010	21.0023	.6016
.8170	.1800	0.0000	0.0000				

# APPENDIX B – Continued

0 0 5 550	.7200	.2006	1.3009	-28.8047	.0010	21.9992	.5789
.8200	.1800	0.0000	0.0000				
0 0 5 575	.6800	.8024	1.3524	-28.7016	.0080	23.0017	.5498
.8200	.1800	0.0000	0.0000				
0 0 5 600	.6500	1.5011	1.3695	-28.6041	.0180	24.2503	.4986
.8230	.1800	0.0000	0.0000				
0 0 5 625	.6000	1.9998	1.3808	-28.5010	.0230	24.5020	.4524
.8250	.1800	0.0000	0.0000				
0 0 5 650	.5700	2.4985	1.3984	-28.4036	.0280	25.4985	.4110
.8260	.1800	0.0000	0.0000				
0 0 5 675	.5500	3.5010	1.4209	-28.3004	.0280	26.0022	.3498
.8200	.1800	0.0000	0.0000				
0 0 5 700	.5000	3.9996	1.4328	-28.3004	.0350	26.5002	.2981
.8300	.1800	0.0000	0.0000				
0 0 5 725	.4500	4.4980	1.4727	-28.2030	.0370	27.4968	.2522
.8350	.1800	0.0000	0.0000				
0 0 5 750	.4300	5.3003	1.4784	-28.0025	.0420	27.7478	.1490
.8370	.1800	0.0000	0.0000				
0 0 5 775	.4000	5.9985	1.5013	-27.8994	.0440	28.0051	.0974
.8400	.1800	0.0000	0.0000				
0 0 5 800	.3500	6.4976	1.5527	-27.8019	.0520	28.5028	.0172
.8400	.1800	0.0000	0.0000				
0 0 5 825	.3300	7.3000	1.5699	-27.7045	.0520	28.7023	-.0802
.8400	.1800	0.0000	0.0000				
0 0 5 850	.3000	7.9993	1.5814	-27.6014	.0520	28.7474	-.1490
.8450	.1800	0.0000	0.0000				
0 0 5 875	.2700	8.4978	1.5818	-27.5040	.0590	28.9987	-.2292
.8500	.1800	0.0000	0.0000				

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 ZMAX(3)=1000.,  
 CARD=T,  
 MMAPR= .10E+01 ,ALPHA= 7.86 ,MACH= .429 ,CG= .260 ,PARAM= 5.0000,  
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 15.66803 0.00000 -0.00000 -32.15869  
 0.00000 .99155 0.00000 0.00000  
 B 4 5  
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 D1 5  
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 .100E+01-0. -0. -0. -0. -0. -0. -0.  
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 END  
 113638 765 8.5753 -1.9595 413.5412 4.3927 .7507 0.0000 .0006  
 -2.9244 .0309 -.0501 4.3839 2.054045599.9089 .4274 38.4406  
 113638 785 8.5616 -2.0726 413.6227 4.3253 .7578 0.0000 -.0005  
 -2.3376 .0318 -.0486 4.3850 2.112545599.9089 .4274 38.4406  
 113638 805 8.5408 -2.2248 413.6921 4.3085 .7605 0.0000 -.0015  
 -1.7390 .0322 -.0468 4.3858 2.196145599.9089 .4274 38.4406

# APPENDIX B – Continued

113638 825	8.5509	-2.3516	413.7493	4. .89	.7521	0.0000	.0001
-1.5414	.0331	-.0456	4.3869	2.63545599.9089	.4274	38.4406	
113638 845	8.5877	-2.5260	413.7486	4.3038	.7402	0.0000	.0027
-1.9137	.0319	-.0437	4.3847	2.306645599.9089	.4274	38.4406	
113638 865	8.6012	-2.5961	413.7083	4.2496	.7307	0.0000	.0053
-2.6130	.0314	-.0411	4.3825	2.380245599.9089	.4274	38.4406	
113638 885	8.5797	-2.6251	413.7084	4.1654	.7241	0.0000	.0044
-3.3808	.0302	-.0386	4.3781	2.464545599.9089	.4274	38.4406	
113638 905	8.5756	-2.5501	413.7084	4.0980	.7197	0.0000	.0016
-4.1495	.0281	-.0343	4.3781	2.504545599.9089	.4274	38.4406	
113638 925	8.5627	-2.4277	413.7084	4.0813	.7094	0.0000	.0033
-4.9065	.0262	-.0314	4.3793	2.534945599.9089	.4274	38.4406	
113638 945	8.4809	-2.1846	413.7084	4.0555	.6899	0.0000	.0072
-5.6091	.0253	-.0288	4.3831	2.607945599.9089	.4274	38.4406	
113638 965	8.4024	-1.9271	413.7084	3.9824	.6769	0.0000	.0063
-6.0751	.0241	-.0256	4.3869	2.692645599.9089	.4274	38.4406	
113638 985	8.3974	-1.6396	413.7084	3.8979	.6845	0.0000	.0004
-6.0882	.0226	-.0223	4.3906	2.732745599.9089	.4274	38.4406	
113639 5	8.3924	-1.3778	413.6970	3.8580	.6937	0.0000	-.0042
-5.6172	.0212	-.0194	4.3935	2.763045599.9089	.4274	38.4406	
113639 25	8.3589	-1.1780	413.5372	3.8540	.7016	0.0000	-.0028
-4.8719	.0215	-.0178	4.3968	2.836045599.6841	.4269	38.3552	
113639 45	8.3762	-1.0928	413.1609	3.8549	.7085	0.0000	-.0006
-4.0660	.0214	-.0154	4.4030	2.920845583.6748	.4262	38.2710	
113639 65	8.4073	-1.0380	412.6949	3.8551	.7216	0.0000	.0001
-3.2368	.0213	-.0131	4.4120	2.960945583.5624	.4260	38.2283	
113639 85	8.4205	-1.0744	412.3642	3.8550	.7233	0.0000	-.0011
-2.3875	.0198	-.0101	4.4225	2.964945583.4500	.4258	38.1855	
113639 105	8.4568	-1.2403	412.2143	3.8550	.7297	0.0000	-.0023
-1.5454	.0186	-.0075	4.4328	2.969645583.4500	.4258	38.1855	
113639 125	8.4908	-1.4808	412.1725	3.8550	.7473	0.0000	-.0057
-1.8791	.0164	-.0051	4.4407	3.023945583.4500	.4258	38.1855	
113639 145	8.4271	-1.7332	412.1700	3.8289	.7544	0.0000	-.0060
-1.6036	.0154	-.0036	4.4463	3.108545583.4500	.4258	38.1855	
113639 165	8.3779	-2.0156	412.1710	3.7553	.7504	0.0000	-.0009
-1.7918	.0129	-.0024	4.4493	3.176245583.4500	.4258	38.1855	
113639 185	8.4097	-2.2631	412.1710	3.6708	.7553	0.0000	-.0064
-1.3128	.0115	-.0017	4.4527	3.193045583.4500	.4258	38.1855	
113639 205	8.4246	-2.4381	412.1710	3.6310	.7624	0.0000	.0098
-2.0049	.0094	-.0012	4.4544	3.192645583.4500	.4258	38.1855	
113639 225	8.3743	-2.5167	412.1710	3.6008	.7494	0.0000	.0089
-2.7575	.0082	-.0007	4.4577	3.192145583.4500	.4258	38.1855	
113639 245	8.3433	-2.5156	412.1710	3.5281	.7272	0.0000	.0067
-3.5236	.0058	-.0002	4.4622	3.192145583.4500	.4258	38.1855	
113639 265	8.3208	-2.4164	412.1710	3.4438	.7124	0.0000	.0062
-4.2852	.0027	.0000	4.4671	3.192145583.4500	.4258	38.1855	
113639 285	8.2572	-2.2232	412.1710	3.4039	.6955	0.0000	.0049
-5.0012	.0000	-.0000	4.4721	3.192145583.4500	.4258	38.1855	
113639 305	8.2150	-2.0162	412.1710	3.3999	.6821	0.0000	.0037
-5.4495	-.0033	-.0005	4.4786	3.192145583.4500	.4258	38.1855	
113639 325	8.2278	-1.8144	412.1443	3.4008	.6723	0.0000	.0070
-5.3935	-.0054	-.0012	4.4856	3.192145583.4500	.4258	38.1855	
113639 345	8.2101	-1.6285	412.0635	3.4010	.6730	0.0000	.0084
-4.8517	-.0081	-.0024	4.4942	3.192145583.3376	.4255	38.1428	
113639 365	8.1986	-1.4795	411.9219	3.3748	.6858	0.0000	.0045
-4.0525	-.0097	-.0039	4.5040	3.192145583.2252	.4253	38.1000	
113639 385	8.2485	-1.4631	411.7953	3.3012	.7017	0.0000	.0014
-3.1842	-.0117	-.0059	4.5147	3.192145583.2252	.4253	38.1000	
113639 405	8.2806	-1.5141	411.7223	3.2168	.7179	0.0000	.0027
-2.2934	-.0138	-.0083	4.5241	3.192145583.2252	.4253	38.1000	
113639 425	8.2579	-1.6447	411.7062	3.1770	.7294	0.0000	.0013
-1.4101	-.0156	-.0111	4.5338	3.192145583.2252	.4253	38.1000	
113639 445	8.2446	-1.9130	411.7067	3.1729	.7409	0.0000	-.0055
-1.5447	-.0172	-.0139	4.5430	3.186545583.2252	.4253	38.1000	
113639 465	8.2341	-2.2763	411.7072	3.1739	.7466	0.0000	-.0120
.2533	-.0184	-.0167	4.5499	3.132145583.2252	.4253	38.1000	

# APPENDIX B – Continued

113639 485	8.1615	-2.6704	411.7072	3.1479	.7476	0.0000	-.0132
.8164	-.0189	-.0183	4.5525	3.047545583.2252	.4253	38.1000	
113639 505	8.0815	-3.0977	411.7071	3.0743	.7420	0.0000	-.0102
.9448	-.0206	-.0210	4.5539	2.979845583.2252	.4253	38.1000	
113639 525	8.0343	-3.5350	411.7071	2.9899	.7405	0.0000	-.0052
.6279	-.0217	-.0227	4.5542	2.963045583.2252	.4253	38.1000	
113639 545	7.9862	-3.9021	411.7035	2.9239	.7331	0.0000	-.0004
.0335	-.0237	-.0253	4.5553	2.937245583.2252	.4253	38.1000	
113639 565	7.9403	-4.1584	411.6851	2.8463	.7157	0.0000	-.0022
-.6994	-.0239	-.0259	4.5546	2.863745567.4531	.4251	38.1013	
113639 585	7.9260	-4.3669	411.6648	2.7629	.6994	0.0000	.0027
-1.4893	-.0247	-.0274	4.5549	2.778845583.2252	.4253	38.1000	
113639 605	7.9117	-4.5001	411.6633	2.6971	.6879	0.0000	.0005
-2.2923	-.0258	-.0285	4.5530	2.738845583.2252	.4253	38.1000	
113639 625	7.8604	-4.5177	411.6611	2.6195	.6722	0.0000	-.0011
-3.0865	-.0277	-.0306	4.5519	2.734745583.2252	.4253	38.1000	
113639 645	7.7962	-4.4364	411.6338	2.5305	.6545	0.0000	-.0010
-3.8947	-.0292	-.0321	4.5496	2.709445567.4531	.4251	38.1013	
113639 665	7.7513	-4.2546	411.5866	2.4367	.6334	0.0000	.0011
-4.6789	-.0303	-.0349	4.5497	2.635645567.4531	.4251	38.1013	
113639 685	7.6943	-3.9591	411.5608	2.3486	.6104	0.0000	.0014
-5.4106	-.0303	-.0371	4.5495	2.550745567.4531	.4251	38.1013	
113639 705	7.6482	-3.6214	411.5579	2.2767	.5961	0.0000	.0004
-5.8926	-.0312	-.0408	4.5504	2.510645567.4531	.4251	38.1013	
113639 725	7.6520	-3.2974	411.5585	2.2060	.5999	0.0000	-.0013
-5.8928	-.0310	-.0418	4.5509	2.500945567.4531	.4251	38.1013	
113639 745	7.6546	-3.0145	411.5586	2.1224	.6074	0.0000	-.0014
-5.3849	-.0300	-.0437	4.5551	2.447545567.4531	.4251	38.1013	
113639 765	7.5991	-2.7744	411.5586	2.0557	.6126	0.0000	-.0010
-4.5873	-.0286	-.0445	4.5583	2.363145567.4531	.4251	38.1013	
113639 785	7.5399	-2.6415	411.5585	2.0389	.6193	0.0000	-.0004
-3.7049	-.0277	-.0466	4.5630	2.295445567.4531	.4251	38.1013	
113639 805	7.5089	-2.5788	411.5585	2.0337	.6309	0.0000	-.0009
-2.8041	-.0270	-.0473	4.5636	2.252445567.4531	.4251	38.1013	
113639 825	7.4980	-2.6031	411.5585	1.9802	.6419	0.0000	-.0027
-1.8930	-.0261	-.0497	4.5647	2.178945567.4531	.4251	38.1013	
113639 845	7.5116	-2.7503	411.5585	1.8962	.6489	0.0000	-.0045
-.9899	-.0252	-.0511	4.5638	2.094545567.4531	.4251	38.1013	
113639 865	7.5187	-3.0047	411.5585	1.8289	.6612	0.0000	-.0048
-.1498	-.0242	-.0522	4.5645	2.028245567.4531	.4251	38.1013	
113639 885	7.4708	-3.3096	411.5585	1.8066	.6693	0.0000	-.0048
.4637	-.0229	-.0509	4.5624	1.950245567.4531	.4251	38.1013	
113639 905	7.4125	-3.6388	411.5585	1.7529	.6730	0.0000	-.0064
.6720	-.0222	-.0510	4.5601	1.866445567.4531	.4251	38.1013	
113639 925	7.3834	-3.9659	411.5585	1.6695	.6648	0.0000	-.0086
.4108	-.0223	-.0502	4.5561	1.820945567.4531	.4251	38.1013	
113639 945	7.3499	-4.2379	411.5415	1.5761	.6581	0.0000	-.0075
-.1821	-.0223	-.0499	4.5530	1.762445567.4531	.4251	38.1013	
113639 965	7.2830	-4.4543	411.4934	1.4859	.6421	0.0000	-.0052
-.9383	-.0215	-.0471	4.5482	1.678945551.6928	.4250	38.1025	
113639 985	7.2205	-4.5647	411.4381	1.3964	.6286	0.0000	-.0052
-1.7436	-.0209	-.0451	4.5450	1.611445551.6928	.4250	38.1025	
113640 5	7.1776	-4.6089	411.4121	1.3031	.6168	0.0000	-.0075
-2.5729	-.0208	-.0423	4.5402	1.589045551.6928	.4250	38.1025	
113640 25	7.1304	-4.5240	411.4094	1.2151	.5982	0.0000	-.0077
-3.4037	-.0201	-.0400	4.5358	1.535045551.6928	.4250	38.1025	
113640 45	7.0858	-4.3477	411.4101	1.1432	.5712	0.0000	-.0042
-4.2229	-.0190	-.0366	4.5306	1.451145551.6928	.4250	38.1025	
113640 65	7.0637	-4.0891	411.4101	1.0726	.5524	0.0000	-.0006
-5.0267	-.0185	-.0340	4.5258	1.383445551.6928	.4250	38.1025	
113640 85	7.0516	-3.7457	411.4101	.9890	.5461	0.0000	-.0004
-5.7853	-.0182	-.0303	4.5204	1.366645551.6928	.4250	38.1025	
113640 105	7.0292	-3.3494	411.4101	.9167	.5448	0.0000	-.0012
-6.2541	-.0181	-.0288	4.5169	1.361445551.6928	.4250	38.1025	
113640 125	7.0075	-2.9264	411.3834	.8459	.5425	0.0000	-.0020
-6.1758	-.0168	-.0255	4.5126	1.307545551.6928	.4250	38.1025	

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113640 145	6.9644	-2.5579	411.2815	.7624	.5468	0.0000	-.0038
-5.5759	-.0156	-.0246	4.5118	1.223145551.5405	.4247	38.0598	
113640 165	6.9296	-2.2471	411.1199	.6957	.5622	0.0000	-.0062
-4.7276	-.0142	-.0222	4.5107	1.155545551.4682	.4245	38.0170	
113640 185	6.9509	-2.0761	410.9929	.6790	.5797	0.0000	-.0058
-3.8206	-.0138	-.0218	4.5109	1.138745551.4682	.4245	38.0170	
113640 205	7.0185	-1.9898	410.9480	.6793	.5917	0.0000	-.0056
-2.8999	-.0136	-.0200	4.5082	1.139145551.4682	.4245	38.0170	
113640 225	7.0708	-1.9887	410.9448	.6798	.5991	0.0000	-.0082
-1.9766	-.0134	-.0188	4.5064	1.139645551.4682	.4245	38.0170	
113640 245	7.0887	-2.0849	410.9459	.6537	.6085	0.0000	-.0110
-1.0609	-.0127	-.0161	4.5038	1.139545551.4682	.4245	38.0170	
113640 265	7.0668	-2.3011	410.9784	.5803	.6219	0.0000	-.0117
-.1970	-.0118	-.0137	4.5019	1.139545551.4682	.4245	38.0170	
113640 285	7.0271	-2.5919	411.1147	.4960	.6297	0.0000	-.0112
.5241	-.0108	-.0102	4.4976	1.139545551.6928	.4250	38.1025	
113640 305	7.0045	-2.9428	411.3422	.4506	.6306	0.0000	-.0102
.9987	-.0103	-.0074	4.4915	1.139545551.8051	.4252	38.1453	
113640 325	6.9934	-3.3233	411.5377	.3925	.6290	0.0000	-.0097
1.1520	-.0098	-.0040	4.4841	1.139545551.8051	.4252	38.1453	
113640 345	6.9488	-3.7194	411.6544	.3096	.6269	0.0000	-.0100
.9748	-.0098	-.0004	4.4768	1.139545551.8051	.4252	38.1453	
113640 365	6.8709	-4.0653	411.7452	.2425	.6239	0.0000	-.0125
.5325	-.0098	.0037	4.4696	1.139545551.9174	.4255	38.1880	
113640 385	6.8117	-4.3533	411.8037	.1997	.6112	0.0000	-.0124
-.0810	-.0099	.0076	4.4641	1.139545551.9174	.4255	38.1880	
113640 405	6.7841	-4.5533	411.7955	.1266	.5916	0.0000	-.0104
-.7934	-.0094	.0113	4.4593	1.139545551.8051	.4252	38.1453	
113640 425	6.7540	-4.6728	411.7772	.0155	.5742	0.0000	-.0081
-1.5786	-.0088	.0139	4.4541	1.139545551.9174	.4255	38.1880	
113640 445	6.7146	-4.7068	411.8288	-.1012	.5646	0.0000	-.0092
-2.3973	-.0083	.0160	4.4465	1.139545551.2811	.4255	38.2320	
113640 465	6.6734	-4.6335	411.8957	-.1936	.5614	0.0000	-.0104
-3.2418	-.0080	.0179	4.4380	1.139545551.2811	.4255	38.2320	
113640 485	6.6236	-4.4591	411.9435	-.2617	.5500	0.0000	-.0093
-4.0836	-.0079	.0201	4.4288	1.165845536.2811	.4255	38.2320	
113640 505	6.5801	-4.1750	411.9628	-.3427	.5320	0.0000	-.0067
-4.9155	-.0083	.0221	4.4227	1.239645536.2811	.4255	38.2320	
113640 525	6.5553	-3.7833	412.0180	-.4300	.5152	0.0000	-.0054
-5.7217	-.0086	.0235	4.4186	1.324445536.3933	.4258	38.2748	
113640 545	6.5146	-3.2856	412.1033	-.4774	.5031	0.0000	-.0056
-6.5017	-.0088	.0248	4.4140	1.390745536.3933	.4258	38.2748	
113640 565	6.4414	-2.7304	412.1719	-.5383	.4961	0.0000	-.0059
-7.1179	-.0091	.0256	4.4084	1.468645536.3933	.4258	38.2748	
113640 585	6.3930	-2.1577	412.1889	-.6253	.4950	0.0000	-.0074
-7.3263	-.0093	.0259	4.4027	1.552545536.3933	.4258	38.2748	
113640 605	6.3828	-1.6004	412.1885	-.6955	.5001	0.0000	-.0100
-7.0376	-.0093	.0251	4.3983	1.618645536.3933	.4258	38.2748	
113640 625	6.4021	-1.0910	412.1880	-.7131	.5031	0.0000	-.0102
-6.4054	-.0089	.0236	4.3945	1.696645536.3933	.4258	38.2748	
113640 645	6.4546	-.6705	412.1881	-.7127	.5092	0.0000	-.0079
-5.6369	-.0088	.0221	4.3945	1.806745536.3933	.4258	38.2748	
113640 665	6.5216	-.3391	412.1881	-.7121	.5204	0.0000	-.0071
-4.8121	-.0081	.0192	4.3961	1.920545536.3933	.4258	38.2748	
113640 685	6.5717	-.1023	412.1881	-.7122	.5336	0.0000	-.0092
-3.9468	-.0074	.0163	4.3967	2.035745536.3933	.4258	38.2748	
113640 705	6.5891	.0179	412.1881	-.7122	.5467	0.0000	-.0118
-3.0331	-.0061	.0124	4.3928	2.148745536.3933	.4258	38.2748	
113640 725	6.5806	.0233	412.1881	-.7122	.5626	0.0000	-.0130
-2.1098	-.0051	.0094	4.3865	2.263745536.3933	.4258	38.2748	
113640 745	6.5726	-.0782	412.1881	-.7122	.5816	0.0000	-.0131
-1.2149	-.0035	.0050	4.3805	2.376745536.3933	.4258	38.2748	
113640 765	6.6124	-.2655	412.1881	-.7122	.5984	0.0000	-.0128
-.3748	-.0022	.0018	4.3784	2.491845536.3933	.4258	38.2748	
113640 785	6.6960	-.5350	412.1881	-.7122	.6084	0.0000	-.0125
.3738	-.0009	-.0014	4.3784	2.604845536.3933	.4258	38.2748	

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113640 805	6.7303	-.8618	412.1938	-.7122	.6146	0.0000	-.0113
.9201	-.0015	-.0003	4.3775	2.719945536.3933	.4258	.4258	38.2748
113640 825	6.7194	-1.2500	412.2452	-.7122	.6208	0.0000	-.0115
1.1400	-.0018	.0002	4.3717	2.833045536.5054	.4260	.4260	38.3175
113640 845	6.7228	-1.6553	412.2991	-.7395	.6255	0.0000	-.0129
.9901	-.0013	-.0012	4.3629	2.948145520.7686	.4259	.4259	38.3188
113640 865	6.7623	-2.0258	412.3576	-.8165	.6212	0.0000	-.0123
.5463	-.0001	-.0040	4.3514	3.066845536.5054	.4261	.4261	38.3175
113640 885	6.7905	-2.3265	412.3894	-.9048	.6029	0.0000	-.0095
-.0906	-.0001	-.0045	4.3397	3.210145520.8807	.4261	.4261	38.3615
113640 905	6.7796	-2.5559	412.4171	-.9464	.5861	0.0000	-.0089
-.8228	-.0007	-.0036	4.3312	3.339445536.5054	.4260	.4260	38.3175
113640 925	6.7385	-2.6859	412.3830	-.9565	.5791	0.0000	-.0110
-1.5956	-.0021	-.0009	4.3293	3.465545520.7686	.4259	.4259	38.3188
113640 945	6.6842	-2.6935	412.3332	-1.0122	.5739	0.0000	-.0119
-2.3868	-.0046	.0039	4.3282	3.592345520.7686	.4259	.4259	38.3188
113640 965	6.6612	-2.6015	412.2853	-1.0999	.5627	0.0000	-.0101
-3.2144	-.0064	.0071	4.3226	3.739145520.7686	.4259	.4259	38.3188
113640 985	6.6636	-2.4222	412.2704	-1.1704	.5470	0.0000	-.0065
-4.0647	-.0066	.0070	4.3139	3.894945520.7686	.4259	.4259	38.3188
113641 5	6.6765	-2.1588	412.2703	-1.1879	.5308	0.0000	-.0030
-4.9040	-.0056	.0047	4.3071	4.045545520.7686	.4259	.4259	38.3188
113641 25	6.6976	-1.8048	412.2708	-1.1875	.5210	0.0000	-.0020
-5.7156	-.0062	.0054	4.3022	4.196645520.7686	.4259	.4259	38.3188
113641 45	6.7189	-1.3521	412.2708	-1.1870	.5178	0.0000	-.0046
-6.5041	-.0077	.0076	4.2992	4.352045520.7686	.4259	.4259	38.3188
113641 65	6.7092	-.8386	412.2707	-1.2085	.5177	0.0000	-.0066
-7.1130	-.0097	.0106	4.2989	4.502645520.7686	.4259	.4259	38.3188
113641 85	6.7159	-.2981	412.2708	-1.2288	.5183	0.0000	-.0063
-7.3151	-.0084	.0079	4.2979	4.653745520.7686	.4259	.4259	38.3188
113641 105	6.7416	.2068	412.2708	-1.2292	.5234	0.0000	-.0064
-7.0355	-.0080	.0069	4.2964	4.809245520.7686	.4259	.4259	38.3188
113641 125	6.7871	.6758	412.2708	-1.2005	.5335	0.0000	-.0070
-6.4287	-.0086	.0074	4.2949	4.959945520.7686	.4259	.4259	38.3188
113641 145	6.8215	1.0615	412.2708	-1.1872	.5420	0.0000	-.0060
-5.6734	-.0107	.0098	4.2963	5.111245520.7686	.4259	.4259	38.3188
113641 165	6.8603	1.3800	412.2671	-1.1866	.5560	0.0000	-.0058
-4.8624	-.0104	.0089	4.2992	5.266845520.7686	.4259	.4259	38.3188
113641 185	6.9233	1.5838	412.2317	-1.1870	.5770	0.0000	-.0072
-4.0182	-.0093	.0069	4.3023	5.417545505.0436	.4257	.4257	38.3200
113641 205	7.0201	1.6708	412.1768	-1.1870	.5961	0.0000	-.0083
-3.1255	-.0077	.0047	4.3042	5.563345505.0436	.4257	.4257	38.3200
113641 225	7.1075	1.6673	412.1328	-1.1870	.6124	0.0000	-.0076
-2.2067	-.0084	.0053	4.3078	5.690745505.0436	.4257	.4257	38.3200
113641 245	7.1524	1.5621	412.1484	-1.1870	.6310	0.0000	-.0060
-1.3078	-.0102	.0069	4.3133	5.810345505.0436	.4257	.4257	38.3200
113641 265	7.1738	1.3415	412.2235	-1.1597	.6544	0.0000	-.0059
-.4664	-.0123	.0083	4.3191	5.953845505.1556	.4260	.4260	38.3628
113641 285	7.1852	1.0207	412.3097	-1.0827	.6728	0.0000	-.0071
.2674	-.0129	.0084	4.3227	6.077945505.1556	.4260	.4260	38.3628
113641 305	7.2175	.6295	412.3559	-.9944	.6821	0.0000	-.0090
-.8024	-.0155	.0101	4.3242	6.176345505.1556	.4260	.4260	38.3628
113641 325	7.2808	.2203	412.4151	-.9527	.6844	0.0000	-.0091
1.0262	-.0184	.0120	4.3243	6.266645505.2676	.4262	.4262	38.4055
113641 345	7.3503	-.1925	412.4995	-.9485	.6818	0.0000	-.0079
.9075	-.0217	.0139	4.3235	6.377745505.2676	.4262	.4262	38.4355
113641 365	7.3944	-.5932	412.5679	-.9554	.6746	0.0000	-.0068
.5577	-.0266	.0167	4.3227	6.491845505.2676	.4262	.4262	38.4055
113641 385	7.4130	-.9764	412.6114	-1.0121	.6672	0.0000	-.0057
.1364	-.0323	.0199	4.3221	6.586945505.2676	.4262	.4262	38.4355
113641 405	7.3926	-1.3062	412.6858	-1.1000	.6630	0.0000	-.0062
-2.622	-.0375	.0222	4.3225	6.681045505.3796	.4264	.4264	38.4482
113641 425	7.3631	-1.5702	412.7710	-1.1704	.6590	0.0000	-.0082
-.6366	-.0413	.0233	4.3256	6.769945505.3796	.4264	.4264	38.4482
113641 445	7.3630	-1.8010	412.8115	-1.1879	.6499	0.0000	-.0082
-1.0074	-.0459	.0245	4.3288	6.863545505.3796	.4264	.4264	38.4482

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113641 465	7.3764	-1.9779	412.8156	-1.1875	.6404	0.0000	-.0052
-1.4229	-.0514	.0263	4.3314	6.954745505	.3796	.4264	38.4482
113641 485	7.3535	-2.0998	412.8147	-1.1870	.6335	0.0000	-.0028
-1.8586	-.0557	.0264	4.3350	7.039745505	.3796	.4264	38.4482
113641 505	7.3049	-2.1635	412.8109	-1.2143	.6256	0.0000	-.0018
-2.3828	-.0602	.0271	4.3395	7.106045505	.3796	.4264	38.4482
113641 525	7.2846	-2.1609	412.7890	-1.2913	.6174	0.0000	-.0009
-2.9436	-.0658	.0280	4.3437	7.184545489	.6662	.4263	38.4495
113641 545	7.2856	-2.0969	412.7732	-1.3796	.6179	0.0000	-.0031
-3.5098	-.0731	.0296	4.3453	7.269045489	.6662	.4263	38.4495
113641 565	7.2840	-1.9688	412.8041	-1.4213	.6196	0.0000	-.0047
-4.0621	-.0796	.0301	4.3469	7.314945489	.7781	.4265	38.4922
113641 585	7.2826	-1.7841	412.8609	-1.4256	.6085	0.0000	-.0023
-4.5779	-.0852	.0300	4.3485	7.373845489	.7781	.4265	38.4922
113641 605	7.2731	-1.5453	412.9141	-1.4246	.5961	0.0000	.0004
-5.0387	-.0915	.0295	4.3526	7.458045489	.7781	.4265	38.4922
113641 625	7.2743	-1.2593	412.9644	-1.4303	.5931	0.0000	-.0014
-5.4322	-.0975	.0289	4.3583	7.526045489	.7781	.4265	38.4922
113641 645	7.2945	-.9367	413.0386	-1.4869	.5899	0.0000	-.0033
-5.7521	-.1026	.0277	4.3648	7.543045489	.8899	.4268	38.5350
113641 665	7.3238	-.5860	413.1019	-1.5749	.5906	0.0000	-.0024
-5.9762	-.1052	.0258	4.3695	7.548345489	.8899	.4268	38.5350
113641 685	7.3381	-.2209	413.1844	-1.6453	.5898	0.0000	.0006
-6.0950	-.1091	.0235	4.3734	7.602645490	.0018	.4270	38.5777
113641 705	7.3679	.1440	413.2731	-1.6628	.5929	0.0000	.0013
-6.1214	-.1138	.0210	4.3770	7.687845490	.0018	.4270	38.5777
113641 725	7.4081	.4916	413.3408	-1.6566	.6024	0.0000	-.0011
-6.0699	-.1214	.0184	4.3821	7.756045490	.0018	.4270	38.5777
113641 745	7.4376	.8247	413.3576	-1.5994	.6140	0.0000	-.0019
-5.9239	-.1275	.0156	4.3879	7.772945490	.0018	.4270	38.5777
113641 765	7.4626	1.1440	413.3438	-1.5115	.6155	0.0000	.0009
-5.6691	-.1317	.0125	4.3941	7.772645490	.0018	.4270	38.5777
113641 785	7.5164	1.4166	413.3135	-1.4411	.6206	0.0000	.0018
-5.3267	-.1329	.0092	4.4000	7.772045490	.0018	.4270	38.5777
113641 805	7.5690	1.6319	413.2652	-1.4236	.6372	0.0000	-.0007
-4.9299	-.1348	.0061	4.4059	7.772145474	.3000	.4268	38.5790
113641 825	7.6108	1.8050	413.2279	-1.4240	.6554	0.0000	-.0021
-4.4981	-.1385	.0033	4.4109	7.772145474	.3000	.4268	38.5790
113641 845	7.6597	1.9494	413.2102	-1.4245	.6673	0.0000	-.0015
-4.0433	-.1407	.0001	4.4161	7.772145474	.3000	.4268	38.5790
113641 865	7.7488	2.0252	413.2079	-1.3971	.6761	0.0000	-.0016
-3.5741	-.1433	-.0028	4.4202	7.772145474	.3000	.4268	38.5790
113641 885	7.8768	2.0335	413.2139	-1.3292	.6893	0.0000	-.0018
-3.0749	-.1471	-.0056	4.4239	7.772145474	.3000	.4268	38.5790
113641 905	8.0000	1.9937	413.2688	-1.2319	.7006	0.0000	-.0012
-2.5602	-.1511	-.0079	4.4260	7.772145474	.4118	.4271	38.6217
113641 925	8.0795	1.8834	413.3539	-1.1902	.7173	0.0000	-.0018
-2.0684	-.1544	-.0095	4.4265	7.772145474	.4118	.4271	38.6217
113641 945	8.1186	1.6903	413.4277	-1.1859	.7306	0.0000	-.0024
-1.6253	-.1581	-.0100	4.4257	7.772145474	.4118	.4271	38.6217
113641 965	8.1385	1.4291	413.4994	-1.1869	.7383	0.0000	-.0014
-1.2239	-.1619	-.0101	4.4246	7.772145474	.5235	.4273	38.6644
113641 985	8.1499	1.1514	413.5841	-1.1870	.7452	0.0000	-.0029
-.8823	-.1642	-.0091	4.4223	7.772145474	.5235	.4273	38.6644
113642 5	8.1768	.8657	413.6781	-1.1870	.7527	0.0000	-.0061
-6.6458	-.1670	-.0075	4.4191	7.772145474	.5235	.4273	38.6644
113642 25	8.2498	.5536	413.7695	-1.1870	.7614	0.0000	-.0075
-.5259	-.1727	-.0067	4.4169	7.772145474	.6352	.4275	38.7071
113642 45	8.3543	.2099	413.8545	-1.1870	.7663	0.0000	-.0053
-.4995	-.1773	-.0066	4.4154	7.772145474	.6352	.4275	38.7071
113642 65	8.4298	-.1315	413.8999	-1.1870	.7662	0.0000	-.0017
-.5424	-.1806	-.0056	4.4137	7.772145474	.6352	.4275	38.7071
113642 85	8.4301	-.4597	413.9587	-1.1870	.7606	0.0000	.0021
-.6642	-.1833	-.0030	4.4104	7.772145474	.7469	.4278	38.7498
113642 105	8.4094	-.7566	414.0427	-1.1870	.7552	0.0000	.0045
-.9032	-.1859	.0003	4.4065	7.772145474	.7469	.4278	38.7498

# APPENDIX B – Continued

113642 125	8.4327	-1.0202	414.1106	-1.1873	.7543	0.0000	.0062
-1.2670	-.1889	.0046	4.4021	7.772145474.7469	.4279	38.7498	
113642 145	8.4780	-1.2382	414.1276	-1.1870	.7536	0.0000	.0071
-1.7173	-.1928	.0091	4.3981	7.777845474.7469	.4278	38.7498	
113642 165	8.5037	-1.4136	414.1401	-1.1870	.7510	0.0000	.0062
-2.2184	-.1962	.0137	4.3938	7.811845474.7469	.4278	38.7498	
113642 185	8.4932	-1.5163	414.1841	-1.1870	.7417	0.0000	.0021
-2.7542	-.1977	.0173	4.3896	7.877345474.8586	.4280	38.7925	
113642 205	8.4739	-1.5403	414.2209	-1.2143	.7258	0.0000	-.0020
-3.3067	-.1994	.0208	4.3856	7.945245459.1683	.4279	38.7938	
113642 225	8.4635	-1.4998	414.2239	-1.2913	.7102	0.0000	-.0026
-3.8601	-.2025	.0245	4.3822	7.990045459.1683	.4279	38.7938	
113642 245	8.4669	-1.4259	414.2102	-1.3796	.7017	0.0000	.0005
-4.3958	-.2057	.0287	4.3792	8.002445459.1683	.4279	38.7938	
113642 265	8.4733	-1.3015	414.2069	-1.4213	.7020	0.0000	.0030
-4.8840	-.2089	.0331	4.3767	8.002545459.1683	.4279	38.7938	
113642 285	8.4700	-1.1238	414.2128	-1.4256	.7041	0.0000	.0046
-5.3120	-.2123	.0375	4.3743	8.002145459.1683	.4279	38.7938	
113642 305	8.4743	-.8732	414.2675	-1.4246	.7003	0.0000	.0069
-5.6727	-.2136	.0416	4.3707	8.002145459.2799	.4281	38.8365	
113642 325	8.4689	-.5903	414.3523	-1.4244	.7018	0.0000	.0078
-5.9532	-.2153	.0442	4.3671	8.002845459.2799	.4281	38.8365	
113642 345	8.4717	-.2981	414.4202	-1.4245	.7082	0.0000	.0043
-6.1229	-.2195	.0466	4.3641	8.103245459.2799	.4281	38.8365	
113642 365	8.5024	-.0091	414.4428	-1.4245	.7184	0.0000	-.0025
-6.1739	-.2237	.0494	4.3619	8.188945459.2799	.4281	38.8365	
113642 385	8.5523	.2911	414.4969	-1.4245	.7200	0.0000	-.0058
-6.1194	-.2248	.0523	4.3595	8.229345459.3915	.4283	38.8792	
113642 405	8.5822	.5724	414.6075	-1.4245	.7225	0.0000	-.0050
-5.9787	-.2230	.0534	4.3570	8.233445459.3915	.4283	38.8792	
113642 425	8.5960	.8025	414.7459	-1.4245	.7167	0.0000	-.0004
-5.7561	-.2233	.0547	4.3546	8.232445459.5031	.4286	38.9219	
113642 445	8.6294	1.0105	414.8160	-1.4245	.7149	0.0000	.0047
-5.4610	-.2247	.0562	4.3526	8.258845443.8243	.4284	38.9232	
113642 465	8.6838	1.1922	414.8190	-1.4245	.7283	0.0000	.0065
-5.1137	-.2264	.0581	4.3511	8.333545459.5031	.4286	38.9219	
113642 485	8.7506	1.3412	414.7854	-1.4245	.7503	0.0000	.0003
-4.7290	-.2272	.0599	4.3500	8.419245443.8243	.4284	38.9232	
113642 505	8.8153	1.4179	414.7623	-1.4245	.7606	0.0000	-.0042
-4.2967	-.2261	.0602	4.3501	8.459645443.8243	.4284	38.9232	
113642 525	8.8595	1.4284	414.7473	-1.3971	.7632	0.0000	-.0012
-3.8114	-.2244	.0607	4.3497	8.469445443.8243	.4284	38.9232	
113642 545	8.8736	1.3996	414.7447	-1.3202	.7749	0.0000	.0014
-3.2801	-.2242	.0605	4.3489	8.523445443.8243	.4284	38.9232	
113642 565	8.8811	1.3291	414.7450	-1.2319	.7905	0.0000	-.0020
-2.7438	-.2262	.0603	4.3480	8.608645443.8243	.4284	38.9232	
113642 585	8.9093	1.1684	414.7507	-1.1902	.8002	0.0000	-.0052
-2.2467	-.2280	.0608	4.3468	8.677045443.8243	.4284	38.9232	
113642 605	8.9563	.9046	414.8052	-1.1859	.8148	0.0000	-.0024
-1.7986	-.2285	.0639	4.3439	8.694045443.9358	.4287	38.9659	
113642 625	9.0086	.5967	414.8954	-1.1869	.8382	0.0000	-.0017
-1.4014	-.2291	.0690	4.3390	8.720245443.9358	.4287	38.9659	
113642 645	9.0580	.2816	415.0177	-1.1870	.8539	0.0000	-.0044
-1.0565	-.2297	.0731	4.3337	8.794445444.0473	.4289	39.0085	
113642 665	9.0817	-.0565	415.1453	-1.1870	.8500	0.0000	-.0091
-0.7822	-.2301	.0762	4.3297	8.880245444.0473	.4289	39.0085	
113642 685	9.0864	-.4018	415.2866	-1.1870	.8453	0.0000	-.0131
-0.5940	-.2293	.0791	4.3267	8.926445444.1587	.4291	39.0512	
113642 705	9.0715	-.7777	415.3878	-1.1870	.8474	0.0000	-.0153
-0.5046	-.2320	.0841	4.3231	8.985545444.1587	.4291	39.0512	
113642 725	9.0385	-1.1860	415.4275	-1.2143	.8497	0.0000	-.0133
-0.5125	-.2363	.0889	4.3193	9.070045444.1587	.4291	39.0512	
113642 745	9.0044	-1.5860	415.4574	-1.2913	.8390	0.0000	-.0067
-0.6304	-.2399	.0928	4.3160	9.144045444.1587	.4291	39.0512	
113642 765	8.9872	-1.9502	415.5267	-1.3796	.8201	0.0000	.0010
-0.8551	-.2421	.0966	4.3119	9.216145444.2702	.4294	39.0939	



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113642 785	8.9917	-2.2720	415.5815	-1.4213	.7939	0.0000	.0092
-1.1282	-.2443	.0998	4.3087	9.301245428.6029	.4292	39.0952	
113642 805	8.9748	-2.5674	415.6207	-1.4256	.7839	0.0000	.0102
-1.3710	-.2447	.1029	4.3060	9.374945428.7142	.4294	39.1379	
113642 825	8.9304	-2.8328	415.6650	-1.4519	.8027	0.0000	.0016
-1.5447	-.2451	.1061	4.3024	9.447145428.7142	.4294	39.1379	
113642 845	8.8721	-3.0945	415.7207	-1.5287	.8219	0.0000	-.0048
-1.6749	-.2469	.1105	4.2966	9.532245428.7142	.4294	39.1379	
113642 865	8.8340	-3.3047	415.7376	-1.6171	.8072	0.0000	-.0018
-1.7944	-.2487	.1137	4.2924	9.606045428.7142	.4294	39.1379	
113642 885	8.7901	-3.4851	415.7638	-1.6646	.7868	0.0000	.0046
-1.9100	-.2507	.1174	4.2888	9.678245428.7142	.4294	39.1379	
113642 905	8.7284	-3.6448	415.8371	-1.7255	.7867	0.0000	.0017
-2.0297	-.2538	.1212	4.2862	9.763445428.8256	.4297	39.1805	
113642 925	8.6786	-3.7946	415.9217	-1.8125	.7915	0.0000	-.0060
-2.1759	-.2559	.1246	4.2840	9.858145428.8256	.4297	39.1805	
113642 945	8.6489	-3.9164	415.9617	-1.9101	.7800	0.0000	-.0040
-2.3432	-.2573	.1262	4.2829	9.950245428.8256	.4297	39.1805	
113642 965	8.6181	-4.0079	415.9658	-2.0047	.7609	0.0000	.0062
-2.5246	-.2575	.1273	4.2790	10.055745428.8256	.4297	39.1805	
113642 985	8.5761	-4.0877	415.9910	-2.0926	.7456	0.0000	.0091
-2.7130	-.2590	.1299	4.2744	10.151645428.8256	.4297	39.1805	
113643 6	8.5341	-4.1368	416.0647	-2.1611	.7368	0.0000	.0043
-2.9128	-.2586	.1329	4.2703	10.255545428.9369	.4299	39.2232	
113643 25	8.4928	-4.1579	416.1322	-2.2424	.7215	0.0000	.0016
-3.1324	-.2619	.1373	4.2658	10.309745428.9369	.4299	39.2232	
113643 45	8.4453	-4.1210	416.1295	-2.3356	.7055	0.0000	.0029
-3.3670	-.2648	.1415	4.2592	10.424445413.2812	.4298	39.2245	
113643 65	8.3790	-4.0680	416.1323	-2.4339	.6983	0.0000	.0046
-3.5917	-.2689	.1457	4.2522	10.566745413.3924	.4300	39.2672	
113643 86	8.2822	-3.9925	416.1894	-2.5261	.7053	0.0000	.0030
-3.7884	-.2691	.1474	4.2473	10.675045413.3924	.4300	39.2672	
113643 105	8.1665	-3.8884	416.2540	-2.6015	.7111	0.0000	.0006
-3.9760	-.2695	.1484	4.2439	10.770145413.3924	.4300	39.2672	
113643 126	8.0742	-3.7383	416.2715	-2.6755	.7077	0.0000	-.0011
-4.1668	-.2711	.1503	4.2414	10.885645413.3924	.4300	39.2672	
113643 145	8.0266	-3.5806	416.2711	-2.7632	.6880	0.0000	-.0025
-4.3535	-.2764	.1541	4.2388	11.027945413.3924	.4300	39.2672	
113643 166	7.9986	-3.4135	416.2706	-2.8390	.6713	0.0000	-.0030
-4.5233	-.2810	.1566	4.2354	11.157245413.3924	.4300	39.2672	
113643 186	7.9579	-3.2287	416.2706	-2.9132	.6645	0.0000	-.0024
-4.6686	-.2848	.1584	4.2302	11.277945413.3924	.4300	39.2672	
113643 206	7.9225	-3.0259	416.2968	-3.0009	.6657	0.0000	.0009
-4.7852	-.2857	.1580	4.2241	11.422645413.3924	.4300	39.2672	
113643 226	7.8973	-2.8001	416.3704	-3.0799	.6566	0.0000	.0030
-4.8852	-.2850	.1562	4.2193	11.553545413.5036	.4302	39.3098	
113643 246	7.8846	-2.5635	416.4811	-3.0884	.6507	0.0000	.0035
-4.9740	-.2856	.1539	4.2158	11.681245413.5036	.4302	39.3098	
113643 266	7.8888	-2.3219	416.5774	-3.1154	.6526	0.0000	.0028
-5.0448	-.2878	.1524	4.2123	11.788745413.6148	.4305	39.3525	
113643 286	7.8940	-2.0681	416.6176	-3.1919	.6581	0.0000	.0013
-5.0807	-.2889	.1492	4.2104	11.912145397.9706	.4303	39.3538	
113643 306	7.8705	-1.8060	416.6272	-3.2803	.6616	0.0000	-.0009
-5.0882	-.2902	.1453	4.2104	12.041045397.9706	.4303	39.3538	
113643 326	7.8488	-1.5385	416.6784	-3.3221	.6581	0.0000	-.0021
-5.0656	-.2911	.1399	4.2109	12.184545398.0817	.4305	39.3965	
113643 346	7.8491	-1.2977	416.7592	-3.3264	.6498	0.0000	-.0008
-5.0227	-.2897	.1333	4.2115	12.313945398.0817	.4305	39.3965	
113643 365	7.8505	-1.0682	416.7995	-3.3254	.6492	0.0000	.0017
-4.9533	-.2854	.1251	4.2133	12.429445398.0817	.4305	39.3965	
113643 386	7.8355	-.8561	416.8037	-3.3252	.6630	0.0000	.0006
-4.8506	-.2832	.1176	4.2163	12.525145398.0817	.4305	39.3965	
113643 406	7.8321	-.6442	416.8027	-3.3253	.6718	0.0000	-.0013
-4.7027	-.2821	.1102	4.2199	12.620245398.0817	.4305	39.3965	
113643 426	7.8598	-.4432	416.8126	-3.3253	.6663	0.0000	-.0018
-4.5438	-.2833	.1033	4.2240	12.715945398.0817	.4305	39.3965	

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113643 446	7.9140	-.2701	416.7892	-3.3468	.6644	0.0000	-.0011
-4.3822	-.2851	.0967	4.2272	12.839345398.0817	.4305	39.3965	
113643 466	7.9515	-.1424	416.7820	-3.3945	.6703	0.0000	-.0023
-4.2160	-.2843	.0896	4.2295	12.942345398.0817	.4305	39.3965	
113643 486	7.9386	-.0362	416.8322	-3.4720	.6804	0.0000	-.0041
-4.0384	-.2819	.0827	4.2307	13.016645398.1928	.4308	39.4391	
113643 506	7.9234	.0667	416.8986	-3.5316	.6909	0.0000	-.0048
-3.8601	-.2813	.0761	4.2329	13.088745382.5602	.4306	39.4404	
113643 526	7.9502	.1431	416.9190	-3.5601	.6989	0.0000	-.0015
-3.6712	-.2799	.0695	4.2363	13.174445382.5602	.4306	39.4404	
113643 546	7.9891	.1706	416.9123	-3.5638	.7040	0.0000	.0027
-3.4702	-.2773	.0631	4.2404	13.243045382.5602	.4306	39.4404	
113643 566	8.0057	.1708	416.9461	-3.5632	.7125	0.0000	.0019
-3.2599	-.2768	.0582	4.2437	13.286945382.5602	.4306	39.4404	
113643 586	8.0128	.1609	417.0141	-3.5631	.7237	0.0000	-.0023
-3.0412	-.2783	.0536	4.2460	13.362045382.6712	.4309	39.4831	
113643 606	8.0121	.1356	417.0433	-3.5631	.7328	0.0000	-.0048
-2.8244	-.2801	.0488	4.2481	13.448145382.5602	.4306	39.4404	
113643 626	8.0064	.0785	417.0599	-3.5631	.7392	0.0000	-.0030
-2.6166	-.2810	.0441	4.2515	13.489145382.6712	.4309	39.4831	
113643 646	8.0214	-.0166	417.1065	-3.5631	.7403	0.0000	-.0017
-2.4270	-.2811	.0389	4.2562	13.493245382.6712	.4309	39.4831	
113643 666	8.0563	-.1266	417.2024	-3.5631	.7385	0.0000	-.0005
-2.2538	-.2816	.0331	4.2609	13.519145382.7822	.4311	39.5257	
113643 686	8.0812	-.2565	417.2909	-3.5631	.7386	0.0000	-.0014
-2.0998	-.2831	.0281	4.2636	13.594445382.7822	.4311	39.5257	
113643 706	8.1004	-.4051	417.3302	-3.5631	.7412	0.0000	-.0040
-1.9635	-.2821	.0241	4.2650	13.681145382.7822	.4311	39.5257	
113643 726	8.1229	-.5715	417.3341	-3.5631	.7412	0.0000	-.0055
-1.8459	-.2779	.0199	4.2676	13.722145382.7822	.4311	39.5257	
113643 746	8.1375	-.7432	417.3160	-3.5631	.7361	0.0000	-.0028
-1.7540	-.2740	.0149	4.2724	13.726245382.7822	.4311	39.5257	
113643 766	8.1174	-.9137	417.2676	-3.5631	.7380	0.0000	.0005
-1.6966	-.2715	.0098	4.2782	13.725245367.1611	.4309	39.5270	
113643 786	8.0898	-1.0875	417.2382	-3.5631	.7477	0.0000	.0014
-1.6725	-.2721	.0055	4.2831	13.725145367.1611	.4309	39.5270	
113643 806	8.0847	-1.2628	417.2853	-3.5631	.7547	0.0000	-.0005
-1.6816	-.2745	.0013	4.2868	13.725145367.2720	.4312	39.5697	
113643 826	8.0918	-1.4487	417.3668	-3.5690	.7564	0.0000	-.0010
-1.7071	-.2755	-.0027	4.2898	13.725145367.2720	.4312	39.5697	
113643 846	8.0822	-1.6231	417.4331	-3.6257	.7517	0.0000	-.0004
-1.7318	-.2727	-.0060	4.2925	13.725145367.2720	.4312	39.5697	
113643 866	8.0710	-1.7938	417.5060	-3.7138	.7471	0.0000	.0006
-1.7689	-.2705	-.0093	4.2952	13.725145367.3829	.4314	39.6123	
113643 886	8.0609	-1.9511	417.5938	-3.7843	.7425	0.0000	-.0003
-1.8557	-.2677	-.0126	4.2979	13.725145351.7733	.4313	39.6137	
113643 906	8.0472	-2.0939	417.6641	-3.8019	.7361	0.0000	-.0009
-1.9897	-.2687	-.0157	4.3002	13.725145351.8841	.4315	39.6563	
113643 926	8.0446	-2.2105	417.7081	-3.8014	.7205	0.0000	-.0014
-2.1465	-.2711	-.0184	4.3022	13.725145351.8841	.4315	39.6563	
113643 946	8.0449	-2.3117	417.7178	-3.8283	.7151	0.0000	-.0027
-2.3157	-.2751	-.0220	4.3054	13.725145351.8841	.4315	39.6563	
113643 966	8.0263	-2.3863	417.7192	-3.9054	.7156	0.0000	-.0034
-2.4960	-.2759	-.0256	4.3091	13.725145351.8841	.4315	39.6563	
113643 986	8.0022	-2.4362	417.7720	-3.9940	.7201	0.0000	-.0028
-2.6817	-.2762	-.0294	4.3121	13.725145351.9949	.4317	39.6989	
113644 0	7.9861	-2.4527	417.8557	-4.0357	.7169	0.0000	-.0032
-2.8846	-.2762	-.0330	4.3144	13.725145351.9949	.4317	39.6989	
113644 26	7.9602	-2.4544	417.9226	-4.0459	.7135	0.0000	-.0050
-3.1223	-.2752	-.0365	4.3171	13.725145351.9949	.4317	39.6989	
113644 46	7.9221	-2.4344	417.9652	-4.1016	.7054	0.0000	-.0035
-3.3754	-.2727	-.0397	4.3203	13.719445351.9949	.4317	39.6989	
113644 66	7.8860	-2.3860	418.0379	-4.1896	.6981	0.0000	-.0005
-3.6219	-.2704	-.0424	4.3230	13.684945352.1057	.4320	39.7416	
113644 86	7.8754	-2.3005	418.1212	-4.2603	.6923	0.0000	.0014
-3.8434	-.2690	-.0447	4.3260	13.618545352.1057	.4320	39.7416	

# APPENDIX B – Continued

113644 106	7.8763	-2.1989	418.1608	-4.2778	.6875	0.0000	.0017
-4.0354	-.2666	-.0460	4.3286	13.549845352.1057	.4320	39.7416	
113644 126	7.8742	-2.0731	418.1908	-4.2833	.6859	0.0000	.0002
-4.2023	-.2631	-.0481	4.3313	13.504445352.1057	.4320	39.7416	
113644 146	7.8627	-1.9258	418.2198	-4.3395	.6826	0.0000	-.0010
-4.3532	-.2634	-.0512	4.3339	13.491845352.2164	.4322	39.7842	
113644 166	7.8642	-1.7417	418.1821	-4.4277	.6761	0.0000	-.0024
-4.5025	-.2622	-.0541	4.3365	13.491745336.5076	.4318	39.7429	
113644 186	7.8728	-1.5301	418.1684	-4.4984	.6691	0.0000	-.0020
-4.6512	-.2594	-.0564	4.3401	13.465345336.5076	.4318	39.7429	
113644 206	7.8726	-1.3112	418.1197	-4.5159	.6701	0.0000	-.0011
-4.7873	-.2572	-.0588	4.3441	13.389845336.6183	.4320	39.7855	
113644 226	7.8555	-1.0926	418.1959	-4.5155	.6764	0.0000	-.0015
-4.8829	-.2542	-.0612	4.3484	13.303245336.6183	.4320	39.7855	
113644 246	7.8344	-.8775	418.2424	-4.5150	.6764	0.0000	-.0028
-4.9483	-.2525	-.0628	4.3508	13.262445336.6183	.4320	39.7855	
113644 266	7.8315	-.6505	418.2800	-4.5150	.6706	0.0000	-.0023
-4.9972	-.2503	-.0643	4.3524	13.231445336.7289	.4323	39.8281	
113644 286	7.8584	-.4277	418.3431	-4.5150	.6656	0.0000	-.0012
-5.0425	-.2505	-.0660	4.3530	13.157045336.7289	.4323	39.8281	
113644 306	7.8957	-.2008	418.4193	-4.5150	.6658	0.0000	-.0003
-5.0603	-.2487	-.0675	4.3538	13.070645336.7289	.4323	39.8281	
113644 326	7.9108	.0368	418.4551	-4.5150	.6690	0.0000	-.0013
-5.0456	-.2425	-.0676	4.3553	13.029845336.7289	.4323	39.8281	
113644 346	7.9142	.2055	418.4853	-4.5150	.6734	0.0000	-.0027
-5.0028	-.2339	-.0672	4.3583	12.998845321.2529	.4323	39.8721	
113644 366	7.9280	.4036	418.5135	-4.5150	.6790	0.0000	-.0018
-4.9322	-.2287	-.0676	4.3612	12.924545321.2529	.4323	39.8721	
113644 386	7.9631	.6053	418.5615	-4.5150	.6816	0.0000	.0029
-4.8309	-.2265	-.0694	4.3634	12.838245321.2529	.4323	39.8721	
113644 406	8.0019	.7704	418.6399	-4.5150	.6859	0.0000	.0049
-4.7028	-.2241	-.0705	4.3637	12.791645321.3635	.4326	39.9147	
113644 426	8.0375	.9089	418.7234	-4.5150	.7004	0.0000	.0018
-4.5480	-.2208	-.0710	4.3639	12.732145321.3635	.4326	39.9147	
113644 446	8.0584	1.0327	418.7627	-4.5150	.7144	0.0000	-.0020
-4.3716	-.2189	-.0720	4.3658	12.647145321.3635	.4326	39.9147	
113644 466	8.0834	1.1445	418.7722	-4.5150	.7195	0.0000	-.0014
-4.1841	-.2178	-.0730	4.3683	12.578445321.3635	.4326	39.9147	
113644 486	8.1090	1.2290	418.8249	-4.5150	.7209	0.0000	.0011
-3.9991	-.2170	-.0741	4.3693	12.534545321.4741	.4328	39.9573	
113644 506	8.1298	1.2779	418.9079	-4.5150	.7319	0.0000	.0019
-3.8101	-.2152	-.0746	4.3702	12.459745321.4741	.4328	39.9573	
113644 526	8.1556	1.3015	418.9746	-4.5091	.7485	0.0000	.0003
-3.6144	-.2087	-.0730	4.3722	12.374945321.4741	.4328	39.9573	
113644 546	8.2057	1.2936	418.9966	-4.4523	.7615	0.0000	-.0006
-3.4118	-.1996	-.0704	4.3742	12.306645321.4741	.4328	39.9573	
113644 566	8.2889	1.2642	419.0185	-4.3642	.7677	0.0000	.0017
-3.2006	-.1902	-.0678	4.3757	12.227345321.5846	.4330	39.9999	
113644 586	8.4081	1.1961	419.0145	-4.2936	.7634	0.0000	.0032
-2.9813	-.1836	-.0663	4.3762	12.142145293.5606	.4328	40.0023	
113644 606	8.5460	1.0885	418.9813	-4.2760	.7607	0.0000	.0010
-2.7677	-.1803	-.0659	4.3756	12.074945293.5606	.4328	40.0023	
113644 626	8.6433	.9550	418.9563	-4.2764	.7662	0.0000	-.0027
-2.5648	-.1772	-.0659	4.3745	11.995645293.5606	.4328	40.0023	
113644 646	8.6723	.8115	419.0046	-4.2769	.7820	0.0000	-.0027
-2.3774	-.1745	-.0654	4.3738	11.910545293.6710	.4330	40.0450	
113644 666	8.6786	.6673	419.0882	-4.2769	.7939	0.0000	-.0013
-2.2070	-.1696	-.0642	4.3764	11.843345293.6710	.4330	40.0450	
113644 686	8.7030	.5009	419.1549	-4.2769	.7984	0.0000	-.0012
-2.0630	-.1655	-.0628	4.3806	11.764245293.6710	.4330	40.0450	
113644 706	8.7329	.3080	419.1670	-4.2769	.7943	0.0000	-.0004
-1.9418	-.1622	-.0618	4.3834	11.679145293.6710	.4330	40.0450	
113644 726	8.7419	.0940	419.1401	-4.2769	.7949	0.0000	.0039
-1.8357	-.1587	-.0602	4.3815	11.612045275.0091	.4328	40.0466	
113644 746	8.7539	-.1195	419.0932	-4.2769	.8018	0.0000	.0022
-1.7451	-.1535	-.0588	4.3795	11.532945275.0091	.4328	40.0466	

# APPENDIX B — Continued

113644 766	8.7739	-.3505	419.0625	-4.2769	.8156	0.0000	-.0037
-1.6864	-.1473	-.0566	4.3789	11.447945293.6710	.4330	40.0450	
113644 786	8.7786	-.5907	419.0360	-4.2769	.8190	0.0000	-.0048
-1.6607	-.1423	-.0556	4.3829	11.380945275.0091	.4328	40.0466	
113644 806	8.7502	-.8400	419.0184	-4.2769	.7945	0.0000	.0018
-1.6615	-.1348	-.0537	4.3889	11.301845275.0091	.4328	40.0466	
113644 826	8.7298	-1.0738	419.0535	-4.2769	.7743	0.0000	.0043
-1.6807	-.1291	-.0529	4.3930	11.216945275.1194	.4330	40.0892	
113644 846	8.7272	-1.2934	419.1332	-4.2828	.7873	0.0000	.0004
-1.7187	-.1266	-.0527	4.3914	11.170845275.1194	.4330	40.0892	
113644 866	8.7146	-1.5205	419.2000	-4.3396	.8152	0.0000	-.0033
-1.7743	-.1277	-.0536	4.3882	11.111645275.1194	.4330	40.0892	
113644 886	8.6893	-1.7418	419.2166	-4.4277	.8100	0.0000	-.0031
-1.8560	-.1251	-.0533	4.3884	11.027145275.1194	.4330	40.0892	
113644 906	8.6742	-1.9330	419.2162	-4.4984	.7912	0.0000	-.0020
-1.9738	-.1215	-.0524	4.3915	10.932245275.1194	.4330	40.0892	
113644 926	8.6656	-2.1052	419.2213	-4.5159	.7940	0.0000	.0026
-2.1355	-.1170	-.0511	4.3958	10.840445275.1194	.4330	40.0892	
113644 946	8.6498	-2.2618	419.3004	-4.5155	.8016	0.0000	-.0069
-2.3129	-.1125	-.0492	4.3980	10.755145275.2297	.4333	40.1318	
113644 966	8.6378	-2.4013	419.4558	-4.5424	.7913	0.0000	-.0081
-2.4590	-.1082	-.0473	4.3973	10.688645275.3400	.4335	40.1744	
113644 986	8.6115	-2.5271	419.6267	-4.6196	.7717	0.0000	-.0051
-2.5464	-.1035	-.0458	4.3960	10.609745275.3400	.4335	40.1744	
113645 6	8.5581	-2.6443	419.7122	-4.7082	.7707	0.0000	-.0020
-2.5843	-.0977	-.0441	4.3963	10.525045256.8047	.4335	40.2186	
113645 26	8.5013	-2.7288	419.7328	-4.7500	.7729	0.0000	-.0035
-2.5970	-.0916	-.0425	4.3983	10.458145256.8047	.4335	40.2186	
113645 46	8.4688	-2.7983	419.7175	-4.7817	.7633	0.0000	-.0047
-2.6131	-.0874	-.0414	4.4000	10.379345256.8047	.4335	40.2186	
113645 66	8.4600	-2.8753	419.7082	-4.8579	.7527	0.0000	-.0048
-2.6390	-.0854	-.0413	4.4010	10.294745256.8047	.4335	40.2186	
113645 86	8.4477	-2.9584	419.7077	-4.9464	.7490	0.0000	-.0074
-2.6769	-.0821	-.0401	4.4019	10.234645256.8047	.4335	40.2186	
113645 106	8.4071	-3.0469	419.7079	-4.9882	.7458	0.0000	-.0074
-2.7171	-.0784	-.0385	4.4029	10.174645256.8047	.4335	40.2186	
113645 126	8.3293	-3.1199	419.7079	-5.0199	.7457	0.0000	-.0035
-2.7486	-.0745	-.0367	4.4017	10.105845256.8047	.4335	40.2186	
113645 146	8.2445	-3.1695	419.7079	-5.0962	.7499	0.0000	-.0025
-2.7736	-.0726	-.0359	4.4001	10.020545256.8047	.4335	40.2186	
113645 166	8.1760	-3.2038	419.7336	-5.1847	.7442	0.0000	-.0035
-2.8039	-.0699	-.0351	4.3995	9.931745256.8047	.4335	40.2186	
113645 186	8.1184	-3.2466	419.8111	-5.2266	.7282	0.0000	-.0017
-2.8266	-.0665	-.0340	4.3992	9.858145256.9148	.4338	40.2612	
113645 206	8.0649	-3.2727	419.9086	-5.2583	.7167	0.0000	.0020
-2.8439	-.0625	-.0323	4.3997	9.786045238.3959	.4338	40.3054	
113645 226	8.0137	-3.2773	419.9643	-5.3345	.7133	0.0000	.0023
-2.8850	-.0588	-.0308	4.4023	9.700745238.3959	.4338	40.3054	
113645 246	7.9761	-3.2797	420.0017	-5.4231	.7125	0.0000	-.0008
-2.9498	-.0526	-.0281	4.4052	9.627045238.3959	.4338	40.3054	
113645 266	7.9426	-3.2937	420.0738	-5.4650	.7159	0.0000	-.0052
-3.0133	-.0461	-.0252	4.4063	9.554845238.5059	.4341	40.3480	
113645 286	7.9113	-3.3031	420.1619	-5.4967	.7129	0.0000	-.0057
-3.0689	-.0404	-.0225	4.4067	9.469645238.5059	.4341	40.3480	
113645 306	7.8866	-3.2849	420.2542	-5.5730	.7030	0.0000	-.0023
-3.1227	-.0377	-.0212	4.4065	9.375045238.6159	.4343	40.3906	
113645 326	7.8637	-3.2346	420.3407	-5.6616	.6975	0.0000	-.0011
-3.1774	-.0358	-.0204	4.4072	9.283145238.6159	.4343	40.3906	
113645 346	7.8343	-3.1853	420.4059	-5.7094	.6987	0.0000	-.0024
-3.2424	-.0336	-.0195	4.4096	9.197645238.6159	.4343	40.3906	
113645 366	7.7938	-3.1207	420.4222	-5.7706	.6958	0.0000	-.0021
-3.3163	-.0304	-.0182	4.4147	9.131045238.6159	.4343	40.3906	
113645 386	7.7609	-3.0526	420.4067	-5.8579	.6948	0.0000	-.0011
-3.3890	-.0248	-.0156	4.4204	9.052145238.6159	.4343	40.3906	
113645 406	7.7386	-2.9684	420.4014	-5.9286	.6909	0.0000	-.0010
-3.4530	-.0218	-.0144	4.4238	8.967245220.1132	.4343	40.4348	

# APPENDIX B – Continued

113645 426	7.7170	-2.8894	420.4174	-5.9521	.6837	0.0000	-.0003
-3.5058	-.0193	-.0132	4.4247	8.900345220.1132	.4343	40.4348	
113645 446	7.6816	-2.8094	420.4575	-6.0086	.6786	0.0000	.0005
-3.5504	-.0159	-.0116	4.4247	8.821445220.1132	.4343	40.4348	
113645 465	7.6338	-2.7182	420.5238	-6.0965	.6781	0.0000	-.0011
-3.5956	-.0119	-.0096	4.4256	8.710045220.2231	.4346	40.4774	
113645 486	7.5847	-2.6226	420.6065	-6.1673	.6744	0.0000	-.0020
-3.6555	-.0082	-.0078	4.4294	8.595045220.2231	.4346	40.4774	
113645 506	7.5552	-2.5170	420.6721	-6.1849	.6695	0.0000	.0001
-3.7323	-.0035	-.0051	4.4342	8.505145220.2231	.4346	40.4774	
113645 526	7.5313	-2.3999	420.6885	-6.2120	.6708	0.0000	.0017
-3.8180	.0036	-.0006	4.4390	8.439145220.2231	.4346	40.4774	
113645 546	7.5184	-2.2611	420.7137	-6.2889	.6743	0.0000	-.0021
-3.8959	.0089	.0028	4.4432	8.360545220.2231	.4346	40.4774	
113645 566	7.5063	-2.1321	420.7853	-6.3777	.6745	0.0000	-.0054
-3.9672	.0105	.0044	4.4473	8.249245220.3330	.4348	40.5200	
113645 586	7.4939	-2.0011	420.8474	-6.4197	.6675	0.0000	-.0043
-4.0226	.0120	.0052	4.4513	8.134345220.3330	.4348	40.5200	
113645 606	7.4746	-1.8571	420.8540	-6.4240	.6639	0.0000	-.0018
-4.0628	.0132	.0063	4.4554	8.038945201.7367	.4346	40.5216	
113645 626	7.4676	-1.6864	420.8891	-6.4229	.6641	0.0000	-.0019
-4.1005	.0133	.0065	4.4590	7.944645201.8465	.4348	40.5642	
113645 646	7.4631	-1.5314	421.0368	-6.4228	.6689	0.0000	-.0020
-4.1422	.0137	.0071	4.4609	7.849745201.9562	.4351	40.6067	
113645 666	7.4456	-1.3804	421.2269	-6.4229	.6671	0.0000	-.0016
-4.1955	.0166	.0097	4.4624	7.727545202.0660	.4353	40.6493	
113645 686	7.4413	-1.2226	421.3786	-6.4504	.6648	0.0000	-.0016
-4.2564	.0203	.0131	4.4638	7.619945202.0660	.4353	40.6493	
113645 706	7.4620	-1.0470	421.4925	-6.5278	.6626	0.0000	-.0019
-4.3117	.0210	.0142	4.4656	7.497245202.1757	.4355	40.6919	
113645 726	7.4745	-.8675	421.5833	-6.6167	.6620	0.0000	-.0017
-4.3499	.0210	.0146	4.4671	7.369245202.1757	.4355	40.6919	
113645 746	7.4770	-.6992	421.6535	-6.6586	.6590	0.0000	-.0015
-4.3872	.0222	.0164	4.4683	7.227045202.2854	.4358	40.7344	
113645 766	7.4991	-.5241	421.6976	-6.6629	.6563	0.0000	-.0029
-4.4188	.0225	.0171	4.4700	7.119545183.7053	.4356	40.7361	
113645 786	7.5413	-.3301	421.7111	-6.6619	.6609	0.0000	-.0043
-4.4426	.0224	.0174	4.4732	7.024845183.7053	.4356	40.7361	
113645 806	7.5611	-.1350	421.6962	-6.6618	.6728	0.0000	-.0035
-4.4621	.0233	.0188	4.4747	6.909745183.7053	.4356	40.7361	
113645 826	7.5715	.0371	421.6965	-6.6618	.6780	0.0000	.0000
-4.4860	.0267	.0230	4.4734	6.768245183.7053	.4356	40.7361	
113645 846	7.5877	.1976	421.7585	-6.6618	.6770	0.0000	.0016
-4.5114	.0293	.0266	4.4698	6.639645183.8149	.4358	40.7786	

## OUTPUT LISTING

09/17/74

INPUT DATA (T INDICATES TRUE OR YES, F INDICATES FALSE OR NO)

## PROGRAM OPTIONS

APRIORI WEIGHTING = 0. 0 TIME HALVING IN EAT.  
ITERATIONS = 6 (ITERATION WILL STOP IF ERROR SUM CHANGES BY LESS THAN A FACTOR OF .40E-02)  
CASE WILL BE STOPPED IF ERROR SUM IS GREATER THAN .40E+21

**OUTPUT**

PLOTS? T (NO PLOTS UNLESS FINAL ERROR SUM IS LESS THAN .100E+06)  
 NUMBER OF CONTROLS AND EXTRA SIGNALS TO BE PLOTTED = 8  
 SECONDS PER CENTIMETER = 1.00  
 PRINTED FLIGHT AND FINAL COMPUTED TIME HISTORIES? F  
 EXTRA OUTPUT OF INTERMEDIATE STEPS FOR A DIAGNOSTIC AID? F  
 PUNCHED FINAL NON-DIMENSIONAL DERIVATIVES AND CONFIDENCE LEVELS? F  
 PUNCHED FINAL DIMENSIONAL MATRICES? F

FLIGHT CONDITION AND VEHICLE CHARACTERISTICS (0. INDICATES VALUE OBTAINED FROM TIME HISTORY ON QBAR,V OR PACH)  
(MACP, ALPHA, CG AND PARAM ARE FOR REFERENCE ONLY, NOT USED IN PROGRAM)

```

METRIC UNITS? F
DYNAMIC PRESSURE = 520.0
VELOCITY = 4665.0
MACH = 6.000
ALPHA = 999.00 (IF 999, OBTAINED FROM TIME HISTORY)
OTHER IDENTIFYING PARAMETER = 0.
SPAN = .00
CHORD = .00
WING AREA = .0
IX = ***** IXZ = 0.0
IY = *****

```

WEIGHT = \*\*\*\*\*  
INSTRUMENT OFFSETS FROM CG

INSTRUMENT IS FORWARD OF CG	
ALPHA	0.000 AN 0.000
BETA	0.000 AY 0.000

INSTRUMENT IS BELOW CG	
BETA	0.000 AY 0.000

## SIGNAL SCALING AND BIASES

[illegible]

MANEUVER	1	START TIME	0	0	0	STOP TIME	0	0	5	075
MANEUVER	1	START TIME	0	0	0	STOP TIME	0	0	5	075

# APPENDIX B – Continued

## AIRCRAFT A CHECK CASE

### INPUT MATRICES :

A		INPUT MATRICES							
		4	BY	4					

TOTAL NUMBER OF POINTS FOR MANEUVER 1 = 235

```

AIRCRAFT A CHECK CASE                                09/17/74

STARTING VALUES   MACH = 0.000   ALPHA = 0.00   PARAM = 0.0000   CG = .250

DIMENSIONAL DERIVATIVES / SEC / SEC**2
  BETA
  Y   -.038000
  L   -16.790000
  N    1.550000
  P   -1.11000
  R   -1.000000*
  DA  -0.000000*
  DR   .014800
  DC1 -0.000000*
  DC2 -0.000000*
  DELTA-0 -0.000000
          -0.000000*
          -0.000000*
          -0.000000*

NON-DIMENSIONAL DERIVATIVES / DEG (ROTARY /RAD)
  BETA
  CY*****
  CL*****
  CN*****
  P   0.000000
  R   0.000000
  DA  0.000000
  DR *****
  DC1 0.000000*
  DC2 0.000000*
  DELTA-0 0.000000
          0.000000*
          0.000000*
          0.000000*

( * ) INDICATES DERIVATIVE HELD FIXED DURING MATCH

NUMBER OF UNKNOWNNS = 21

ENTERING ITERATION LOOP

DIMENSIONAL DERIVATIVE MATRICES PER RADIAN. BIASES IN RADIAN.

A      4 BY 4
--.3800E-01 .1110E+00 -.1000E+01 .6900E-02
-.1679E+02 -.2410E+00 .4000E+00 0.
.1550E+01 -.2840E-02 -.4200E-01 0.
0. .1000E+01 0. 0.
B      4 BY 5
0. .1480E-01 0. 0. 0.
.1276E+02 .2000E+02 0. 0. 0.
.3577E+00 -.2445E+01 0. 0. 0.
0. 0. 0. 0. 0.
VARIABLE BIAS 0. 0. 0. 0. 0.

ERRORS
.1951E-03 .1905E-01 .1562E-03 .4192E-01 .9587E-03 .1459E-01 .1887E-03
WEIGHTED ERRORS
.2271E+00 .1238E+00 .7593E+00 .5660E+01 .2172E-01 .3940E-01 .2153E-01

ITERATION NUMBER 1 COMPLETED

A      4 BY 4
-.4692E-01 .1023E+00 -.1000E+01 .6900E-02
-.2424E+02 -.1403E+00 .2220E+01 0.
.1289E+01 -.3239E-03 -.1284E+00 0.
0. .1000E+01 0. 0.
B      4 BY 5
.2250E-02 .1535E-01 0. 0. 0.
.1430E+02 .1740E+02 0. 0. 0.
.4389E+00 -.2173E+01 0. 0. 0.
0. 0. 0. 0. 0.
VARIABLE BIAS .5277E+00 -.2469E-01 -.4478E-02

ERRORS
.4787E-05 .1302E-02 .7344E-05 .1885E-02 .3279E-03 .3593E-02 .3082E-04
WEIGHTED ERRORS
.1034E-01 .8462E-02 .3569E-01 .2545E+00 .7428E-02 .9701E-02 .6103E-02

ITERATION NUMBER 2 COMPLETED

WEIGHTED ERROR SUM = .6853E+01

WEIGHTED ERROR SUM = .3322E+00

```



# APPENDIX B – Continued

A									WEIGHTED ERROR SUM = .5911E-01				
		4	BY	4									
			</										

```

ITERATION TERMINATING, ERROR WITHIN .001000 BOUND.
CONFIDENCE LEVELS FOR NEXT TO LAST ITERATION
(DIMENSIONAL)

AC      3 BY 3
      .5401E-03 .7999E-03 0.
      .1508E+00 .9145E-02 .2088E+00
      .1056E-01 .7281E-03 .1637E-01

BC      3 BY 5
      .9128E-03 .1019E-02 0.
      .3688E+00 .3906E+00 0.
      .3197E-01 .3726E-01 0.
      .2101E-03
      .7108E-02
      .5759E-03

(NON-DIMENSIONAL)

AC      3 BY 3
      .2629E+07 .7999E-03 0.
      .5063E+10 .1641E+18 .3746E+19
      .3543E+09 .1306E+17 .2938E+18

BC      3 BY 5
      .4442E+07 .4959E+07 0.
      .1236E+11 .1311E+11 0.
      .1073E+10 .1251E+10 0.
      .5859E+08
      .1367E+11
      .1107E+10

```

## APPENDIX B – Continued

AIRCRAFT A CHECK CASE																09/17/77
FINAL VALUES		MACH = 0.000	ALPHA = 0.00	PARAM = 0.0000	CG = .250											
DIMENSIONAL DERIVATIVES / SEC / SEC**2																
BETA	P	R	DA	DR	DC1	DC2	DELTA-C-									
Y	-.046703	.102595	.002753	.015943	-0.000000*	-0.000000*	-.603035									
L	-24.320923	-.101510	14.469795	17.868306	-0.000000*	-0.000000*	.409219									
N	1.269852	.000448	-.151448	-.506167	-0.000000*	-0.000000*	-.007553									
NON-DIMENSIONAL DERIVATIVES / DEG (ROTARY /RAD)																
BETA	P	R	DA	DR	DC1	DC2	DELTA-D-									
CY*****	0.000000	0.000000*	*****	*****	0.000000*	0.000000*	*****									
CL*****	*****	*****	*****	*****	*****	*****	*****									
CN*****	*****	*****	*****	*****	*****	*****	*****									
( * ) INDICATES DERIVATIVE HELD FIXED DURING MATCH																
VARIABLE BIAS	.5179E+00	-.2582E-01	-.4472E-02													
FINAL DIMENSIONAL MATRICES																
A					BY 4											
	-.4673E-01	.1026E+00	-.1000E+01	.6900E-02												
	-.2432E+02	-.1015E+00	.2464E+01	0.												
	.1290E+01	.4483E-03	-.1514E+00	0.												
	0.	.1000E+01	0.	0.												
B					BY 5											
	.2753E-02	.1594E-01	0.	-.3035E-02												
	.1447E+02	.1787E+02	0.	.4092E+00												
	.5062E+03	-.2125E+01	0.	-.7553E-02												
	0.	0.	0.	-.8423E-02												
DEGREES AY POOT ROOT WEIGHTED ERROR SUM = .5890E-01																
ERRORS																
WEIGHTED ERRORS																
.9707E-02	.5287E-02	.1014E-01	.8474E-02	.8017E-02	.1167E-01	.5613E-02										
ERRORS																
6.85	.33	.06	.06	.06	.06	.06										

# APPENDIX B - Continued

09/17/74

AIRCRAFT B CHECK CASE  
 NEWTON-RAPHSON DIGITAL DERIVATIVE MATCHING  
 1 APR 1974

INPUT DATA (T INDICATES TRUE OR YES, F INDICATES FALSE OR NO)  
 LONGITUDINAL CASE  
 DATA SOURCE CARD? T TAPE? F  
 DATA RATE IS 50. SAMPLES/SECOND ON SOURCE FILE (IF 0, DETERMINED FROM TIMES ON THE SOURCE FILE)  
 ON INPUT TAPE: 25 DATA WORDS PER RECORD. SPECIAL SIGNAL ORDER DEFAULT? T

## PROGRAM OPTIONS

APRIORI WEIGHTING = .10E+01 0 TIME HALVINGS IN EAT.  
 ITERATIONS = 6 (ITERATION WILL STOP IF ERROR SUM CHANGES BY LESS THAN A FACTOR OF .10E-02)  
 CASE WILL BE STOPPED IF ERROR SUM IS GREATER THAN .10E+21

## OUTPUT

PLOTS? T (NO PLOTS UNLESS FINAL ERROR SUM IS LESS THAN .100E+06)  
 NUMBER OF CONTROLS AND EXTRA SIGNALS TO BE PLOTTED = 8  
 SECONDS PER CENTIMETER = .50  
 PRINTED FLIGHT AND FINAL COMPUTED TIME HISTORIES? F  
 EXTRA OUTPUT OF INTERMEDIATE STEPS FOR A DIAGNOSTIC AID? F  
 PUNCHED FINAL NON-DIMENSIONAL DERIVATIVES AND CONFIDENCE LEVELS? T  
 PUNCHED FINAL DIMENSIONAL MATRICES? F

FLIGHT CONDITION AND VEHICLE CHARACTERISTICS (0. INDICATES VALUE OBTAINED FROM TIME HISTORY ON QBAR,V OR MACH)  
 (MACH,ALPHA,CG AND PARAM ARE FOR REFERENCE ONLY, NOT USED IN PROGRAM)

METRIC UNITS? F  
 DYNAMIC PRESSURE = 39.0 VELOCITY = 415.2  
 MACH = .429 ALPHA = 7.86 (IF 999., OBTAINED FROM TIME HISTORY)  
 CENTER OF GRAVITY = .260 OTHER IDENTIFYING PARAMETER = .500E+01  
 WING AREA = 85.0 SPAN = 16.05 CHORD = 5.98  
 IX = 275.0 IY = 1912.0 IZ = 2228.0 IXX = 11.6  
 WEIGHT = 2470.0  
 INSTRUMENT OFFSETS FROM CG

X-DIRECTION OFFSETS (+ = INSTRUMENT IS FORWARD OF CG)  
 ALPHA 0.000 AN -.010  
 BETA 0.000 AY 0.000

Z-DIRECTION OFFSETS (+ = INSTRUMENT IS BELOW CG)  
 BETA 0.000 AY 0.000

SIGNAL SCALING AND BIASES  
 SIGNALS  
 VAR BIAS  
 VAR I-C.  
 FIXED BIAS  
 SCALE FACT  
 PLOT LIMITS  
 MINIMUM  
 MAXIMUM

	Q	V	THET	AN	QDOT	AX	DE	DC	DC1	DC2	PHI	ALT	MACH	QBAR
ALFA	0													
F	F	F	F	T	T	T								
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1.00	1.00	1.00	1.00	1.00	1.00	1.00								
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MANEUVER 1 START TIME 11 36 38 750 STOP TIME 11 36 45 840

## 119

### INPUT MATRICES :

[illegible]

09/17/74

## AIRCRAFT B CHECK CASE

STARTING VALUES HACH = .429 ALPHA = 7.86 PARAM = 5.0000 CG = .263

DIMENSIONAL DERIVATIVES / SEC / SEC\*\*2

	ALFA	Q	V	DE	DC	DC1	DC2	DELTA-0
N	.420350	-1.000000*	0.000000*	.064890	0.000000*	0.000000*	0.000000*	-.073460
M	-3.794300	-.363210	0.000000*	-6.280730	0.000000*	0.000000*	0.000000*	.161650
A	-15.668030*	-0.000000*	0.000000*	-8.353920*	0.000000*	0.000000*	0.000000*	2.393650*

NON-DIMENSIONAL DERIVATIVES / DEG (ROTARY /RAD)

	ALFA	Q	V	DE	DC	DC1	DC2	DELTA-0
CN	.070547	0.000000*	0.000000*	.010890	0.000000*	0.000000*	0.000000*	-.706389
CM	-.006354	-4.839157	0.000000*	-.010518	0.000000*	0.000000*	0.000000*	.017429
CA	-.606333*	-0.000000*	0.000000*	-.003377*	0.000000*	0.000000*	0.000000*	.055437*

( \* ) INDICATES DERIVATIVE HELD FIXED DURING MATCH

NUMBER OF UNKNOWNMS = 9

## ENTERING ITERATION LOOP

DIMENSIONAL DERIVATIVE MATRICES PER RADIAN. BIASES IN RADIAN.

	4	BY 4	5
A	.4204E+00	.1300E+01 -0.	.2210E-02
	-.3794E+01	-.3632E+00 0.	0.
	.1567E+02 0.	-.9916E+00 0.	-.3216E+02
B	0.	.9916E+00 0.	0.
	-.6489E-01 -0.	-0.	.7346E-01
	-.6281E+01 0.	0.	.1817E+00
	.8354E+01 -0.	-0.	-.2394E+01
	-0.	.1000E+01 -0.	-0.

VARIABLE BIAS .1000E+01

WEIGHTED ERROR SUM = .2193E+03

ERRORS .1810E-04 .7834E-04 .4079E+02 .4008E-03 .5171E-02

WEIGHTED ERRORS .1810E+01 .5484E+01 0. .1603E+03 .5171E+02

## ITERATION NUMBER 1 COMPLETED

	4	BY 4	5
A	-.4555E+00	.1000E+01 -0.	.2210E-02
	-.3229E+01	-.3851E+00 0.	0.
	.1567E+02 0.	-.9916E+00 0.	-.3216E+02
B	0.	.9916E+00 0.	0.
	-.5102E-01 -0.	-0.	.8519E-01
	-.6259E+01 0.	0.	.1012E+00
	.8354E+01 -0.	-0.	-.2394E+01
	-0.	.1000E+01 -0.	.1491E-02

VARIABLE BIAS .1012E+01

WEIGHTED ERROR SUM = .6688E+01

ERRORS .6808E-05 .1238E-04 .2221E+02 .6785E-05 .2427E-03

WEIGHTED ERRORS .6808E+00 .8665E+00 0. .2714E+01 .2427E+01

## ITERATION NUMBER 2 COMPLETED

# APPENDIX B — Continued

A									WEIGHTED ERROR SUM = .5923E+01				
	4	BY	4										
	-.4511E+00	.1000E+01	-0.			.2210E-02							
	-.3222E+01	-.4853E+00	0.			0.							
	.1567E+02	0.	-0.			-.3216E+02							
B	0.	.9916E+00	0.		3.								
	4	BY	5										
	-.5149E-01	-0.	-0.			0.							
	-.6271E+01	0.	0.			0.							
	.8354E+01	-0.	-0.			0.							
	-0.	.1000E+01	-0.			-0.							
	AN												
	VARIABLE BIAS	.1013E+01											
ERRORS													
	.5865E-05	.1364E-04	.2252E+02	.6054E-05	.1961E-03								
WEIGHTED ERRORS													
	.5865E+00	.9547E+00	0.	.2421E+01	.1961E+01								
ITERATION NUMBER 3 COMPLETED													
A													
	4	BY	4										
	-.4502E+00	.1000E+01	-0.			.2210E-02							
	-.3196E+01	-.4956E+00	0.			0.							
	.1567E+02	0.	-0.			-.3216E+02							
B	0.	.9916E+00	0.		0.								
	4	BY	5										
	-.5192E-01	-0.	-0.			0.							
	-.6260E+01	0.	0.			0.							
	.8354E+01	-0.	-0.			0.							
	-0.	.1000E+01	-0.			-0.							
	AN												
	VARIABLE BIAS	.1012E+01											
ERRORS													
	.5931E-05	.1376E-04	.2251E+02	.6012E-05	.1941E-03								
WEIGHTED ERRORS													
	.5931E+00	.9632E+00	0.	.2405E+01	.1941E+01								
ITERATION NUMBER 4 COMPLETED													
A													
	4	BY	4										
	-.4503E+00	.1000E+01	-0.			.2210E-02							
	-.3193E+01	-.4999E+00	0.			0.							
	.1567E+02	0.	-0.			-.3216E+02							
B	0.	.9916E+00	0.		0.								
	4	BY	5										
	-.5195E-01	-0.	-0.			0.							
	-.6264E+01	0.	0.			0.							
	.8354E+01	-0.	-0.			0.							
	-0.	.1000E+01	-0.			-0.							
	AN												
	VARIABLE BIAS	.1012E+01											
ERRORS													
	.5940E-05	.1389E-04	.2251E+02	.5987E-05	.1937E-03								
WEIGHTED ERRORS													
	.5940E+00	.9722E+00	0.	.2395E+01	.1937E+01								
ITERATION NUMBER 5 COMPLETED													
ITERATION TERMINATING, ERROR WITHIN .001000 ROUND.													

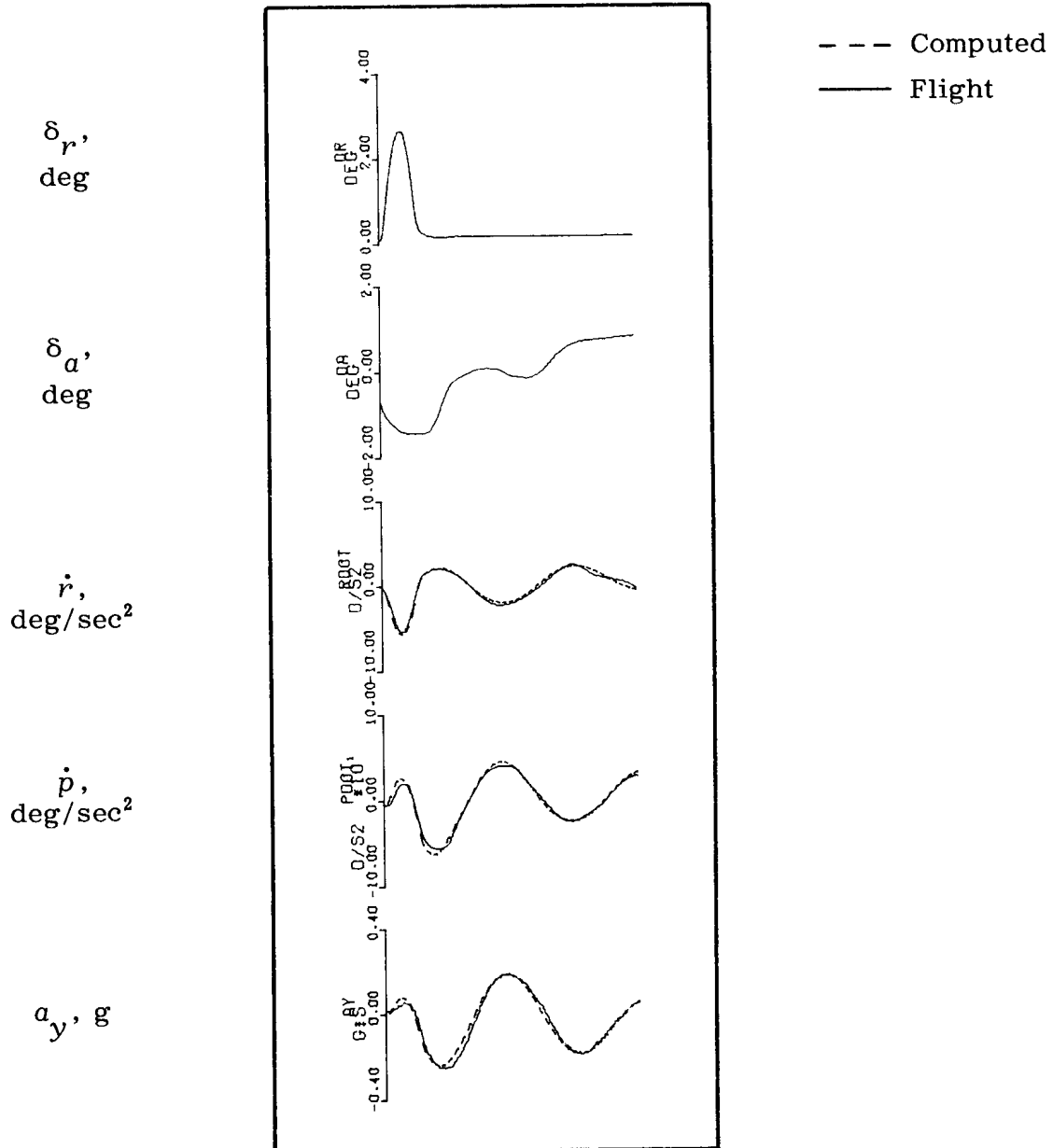






# APPENDIX B — Continued

Two sample plots from the MMLE program are shown. The plots as produced by the automatic plotter are shown within the heavy lines. Explanatory material is included to aid the user in implementing the program. Each plot is presented in two parts to avoid loss of detail from a large reduction. The title on each plot corresponds to the title on the output listing.



# APPENDIX B — Continued

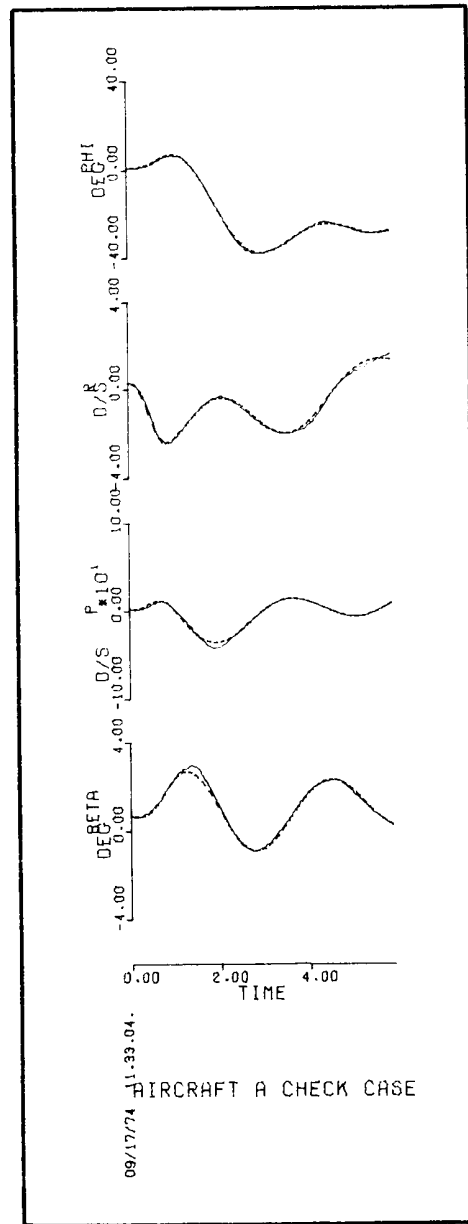
$\phi$ , deg

$r$ ,  
deg/sec

$p$ ,  
deg/sec

$\beta$ , deg

Date and time  
of run



# APPENDIX B – Continued

$\bar{q}$ ,  
lb/sq ft

$M$

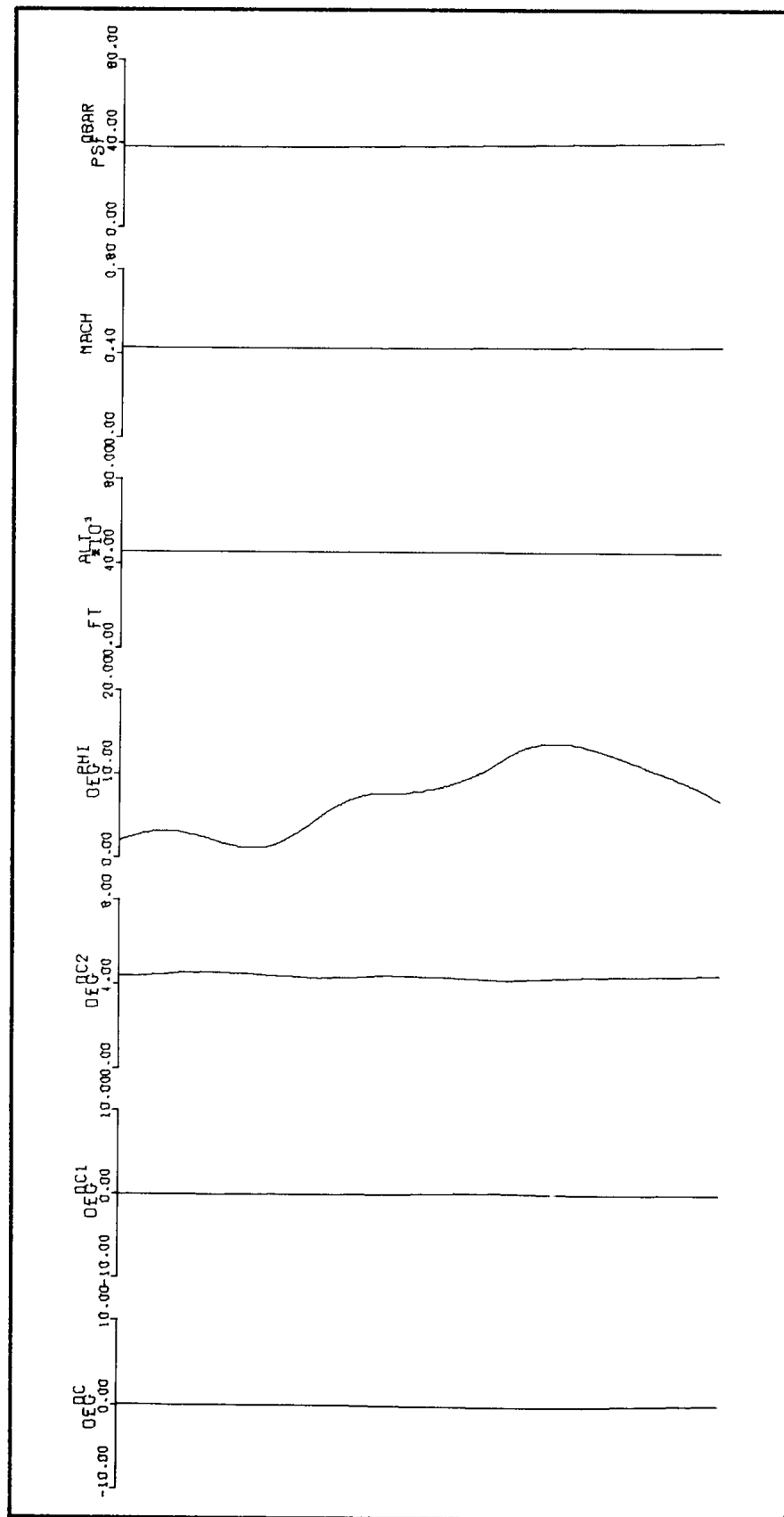
Altitude,  
ft

$\phi$ , deg

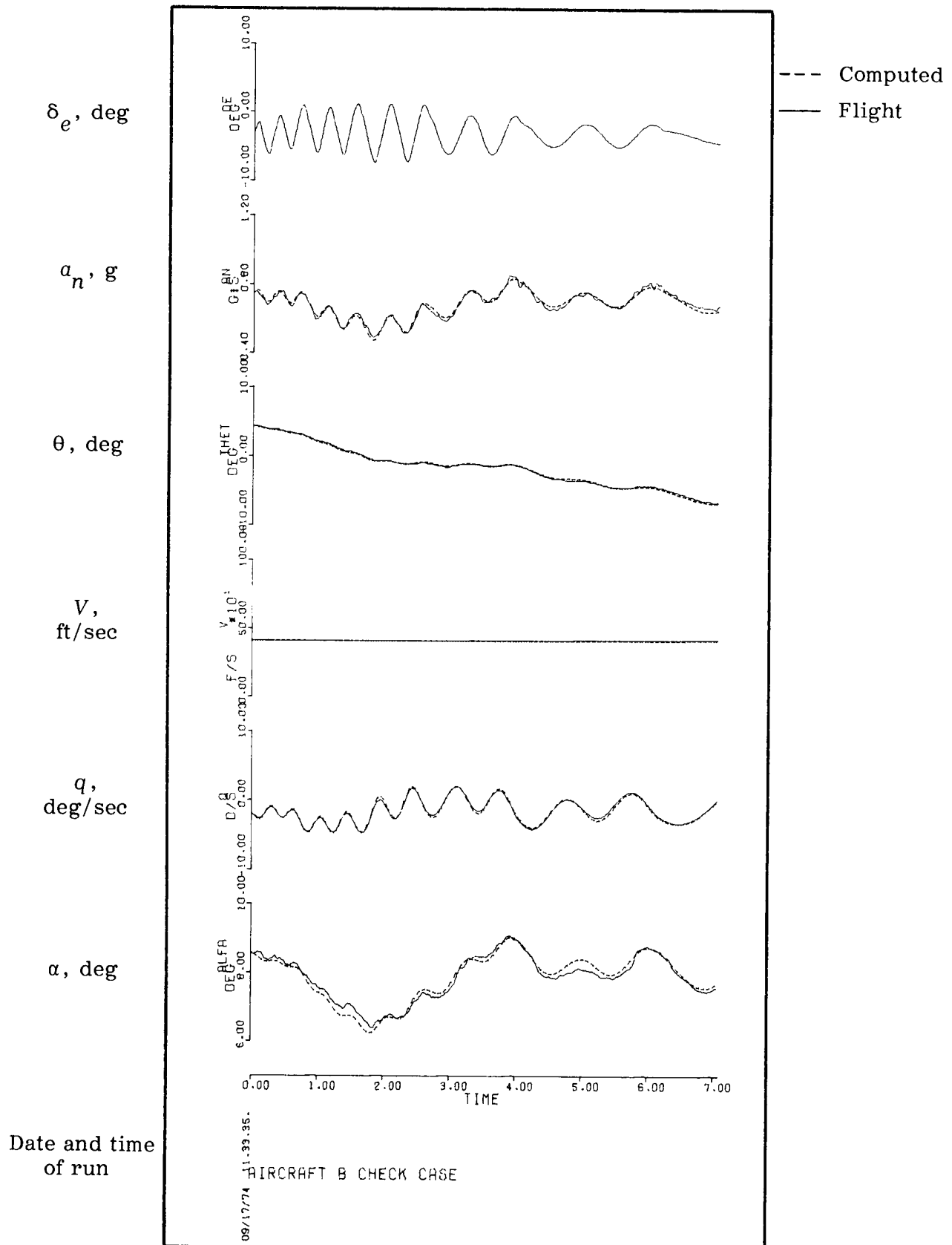
$\delta_{c_2}$ , deg

$\delta_{c_1}$ , deg

$\delta_c$ , deg



# APPENDIX B — Concluded



## APPENDIX C

### SETUP PROGRAM AND SUBROUTINES

Listings of the main program and the subroutines used in the SETUP program are presented together with supplementary information.

#### MAIN PROGRAM SETUP

Description: The main SETUP program sets several defaults and then reads the option cards to determine whether it is to read an input tape, punch a card deck, write an output tape, or perform any combination of these operations. It then directs the execution of the assigned tasks for each case.

Programing notes: As in the MMLE program, the program statement is needed on CDC 6000/7000 systems. On an IBM 360/370 system, DD cards perform this function. Cards 590 to 730 are concerned solely with setting the default values for DELTA as defined in the input description (p. 30).

## APPENDIX C – Continued

Program listing:

PROGRAM SETUP(INPUT,PUNCH,OUTPUT,TAPE4,TAPE15,TAPE1=INPUT,	MAIN 0
- TAPE2=PUNCH,TAPE3=OUTPUT)	MAIN 10
COMMON /ALLOIM/ MAX,MIX	MAIN 20
COMMON /OPTION/ TAPE,DECK,READ	MAIN 30
COMMON /FLCOND/ ALPHA,THETA,Q,V,MACH,IX,IY,IZ,IXZ,W,PHI,CG,KIAS,	MAIN 40
- ALT, LONG,PARAM,FLT,CASE,AVG,DELTA,ST,ET,DETRIM	MAIN 50
REAL MACH,IX,IY,IZ,IXZ,KIAS,AVG(40)	MAIN 60
INTEGER ST(4),ET(4),FLT,CASE	MAIN 70
LOGICAL TAPE,DECK,READ, LONG,LATR,DELTA(4),LATDEL(4),LONDEL(4),DEL	MAIN 80
NAMELIST /COND/ LONG,LATR,FLT,CASE,ALPHA,THETA,Q,V,MACH,W,IX,IY,	MAIN 90
- IZ,IXZ,KIAS,ALT,CG,PARAM,DELTA,PHI,DETRIM	MAIN 100
DATA WRT/4HWRT/,PNC/4HPNC/,RD/4HREAD/,START/4HSTAR/	MAIN 110
MAX=5	MAIN 120
REWIND 15	MAIN 130
DO 10 I=1,4	MAIN 140
LONDEL(I)=.FALSE.	MAIN 150
10 LATDEL(I)=.FALSE.	MAIN 160
TAPE=.FALSE.	MAIN 170
DECK=.FALSE.	MAIN 180
READ=.FALSE.	MAIN 190
DETRIM=0.	MAIN 200
PARAM=0.	MAIN 210
CG=999.	MAIN 220
IXZ=0.	MAIN 230
ALT=0.	MAIN 240
KIAS=0.	MAIN 250
THETA=0.	MAIN 260
PHI=0.	MAIN 270
FLT=0.	MAIN 280
CASE=0.	MAIN 290
LONG=.FALSE.	MAIN 300
C	MAIN 310
C READ OPTIONS	MAIN 320
C	MAIN 330
20 READ (1,1000) OPTN	MAIN 340
IF(OPTN.EQ.START) GO TO 50	MAIN 350
IF(OPTN.NE.WRT) GO TO 40	MAIN 360
TAPE=.TRUE.	MAIN 370
WRITE(3,2001)	MAIN 380
30 READ=.TRUE.	MAIN 390
WRITE(3,2000)	MAIN 400
GO TO 20	MAIN 410
40 IF(OPTN.EQ.RD) GO TO 30	MAIN 420
IF(OPTN.NE.PNC) GO TO 20	MAIN 430
DECK=.TRUE.	MAIN 440
WRITE(3,2002)	MAIN 450
GO TO 20	MAIN 460
50 IF(DECK) CALL SETIN	MAIN 470
IF(READ) CALL RDSET	MAIN 480
C	MAIN 490
C CASE LOOP	MAIN 500
C	MAIN 510
100 READ (1,1001) ST,ET	MAIN 520
IF(ST(1).LT.0) GO TO 200	MAIN 530
LATR=.FALSE.	MAIN 540
DO 110 I=1,4	MAIN 550
110 DELTA(I)=.FALSE.	MAIN 560

# APPENDIX C – Continued

READ (1,COND)	MAIN 570
IF(LATR) LONG=.FALSE.	MAIN 580
DEL=DELTA(1).OR.DELTA(2).OR.DELTA(3).OR.DELTA(4)	MAIN 590
IF(LONG) GO TO 150	MAIN 600
IF(.NOT.DEL) GO TO 130	MAIN 610
DO 120 I=1,4	MAIN 620
120 LATDEL(I)=DELTA(I)	MAIN 630
GO TO 190	MAIN 640
130 DO 140 I=1,4	MAIN 650
140 DELTA(I)=LATDEL(I)	MAIN 660
GO TO 190	MAIN 670
150 IF(.NOT.DEL) GO TO 170	MAIN 680
DO 160 I=1,4	MAIN 690
160 LONDEL(I)=DELTA(I)	MAIN 700
GO TO 190	MAIN 710
170 DO 180 I=1,4	MAIN 720
180 DELTA(I)=LONDEL(I)	MAIN 730
190 WRITE(3,2003)FLT,CASE,ST,ET,LONG	MAIN 740
IF(READ) CALL TAPER0	MAIN 750
IF(DECK) CALL PNCH	MAIN 760
GO TO 100	MAIN 770
1000 FORMAT(A4)	MAIN 780
1001 FORMAT(2(I2,I3,1X))	MAIN 790
2000 FORMAT(18H0TAPE WILL BE READ)	MAIN 800
2001 FORMAT(25H0MLE TAPE WILL BE WRITTEN)	MAIN 810
2002 FORMAT(25H0MLE DECK WILL BE PUNCHED)	MAIN 820
2003 FORMAT(1H1,2GX,6HFLIGHT,I3,5X,4MCASE,I4,5X,4HTIME,4I4,4H TO,	MAIN 830
- 4I4,5X,14HLONGITUDINAL? ,L1)	MAIN 840
200 STOP	MAIN 850
END	MAIN 860



## APPENDIX C – Continued

### SUBROUTINE SETIN

Description: Subroutine SETIN initializes all information needed to punch the MMLE program deck. It sets several defaults and reads in the values desired. It also calls WINDIN to input predicted derivatives and COND1 to make any other input required by the user.

Subroutine listing:

C	SUBROUTINE SETIN	SETI 0
	COMMON /COM/ MZLA,MZLO,S,SPAN,CBAR,CGLA,CGLC,METRIC,D1LO,	SETI 10
	- D1LA,VEH,APRALA,APRBLA,APRALO,APRBLO,WMLA,WMLO,PUNCH,CORRECT,	SETI 20
	- XALF,XB,ZB,XAN,ZAX,XAY,ZAY,SPS,DLA,DLO	SETI 30
	COMMON /DATAWT/ NBP,NMBP,NABP,CATA	SETI 40
	COMMON /WTDATA/ NCLA,NCLO,ABP,MBP,BP,NCHAX,LONG	SETI 50
	REAL DATA(3000),D1LO(7),D1LA(7),ABP(16),MBP(16),BP(8),VEH(2),	SETI 60
	- APRALA(5,4),APRALO(5,4),APRBLA(5,8),APRBLO(5,8)	SETI 70
	- LOGICAL METRIC,LONG(8),LATR(8),RAD,DEG,PUNCH,CORRECT,BODY,STAB,	SETI 80
	- LAT,LON,DLA,DLO	SETI 90
	NAMLIST /WIND/ NABP,NMBP,NBP,S,SPAN,CBAR,CGLA,CGLC,DEG,RAD,	SETI 100
	- METRIC,LONG,LATR,MZLO,MZLA,NCLO,NCLA,WMLA,WMLO,PUNCH,XALF,	SETI 110
	- XAN,ZAX,XAY,ZAY,SPS,XB,ZB,BODY,STAB	SETI 120
C	SETI 130	
C	DEFAULTS	SETI 140
	SPS=0.	SETI 150
	XB=0.	SETI 160
	ZB=0.	SETI 170
	XAY=0.	SETI 180
	ZAY=0.	SETI 190
	XAN=0.	SETI 200
	ZAX=0.	SETI 210
	XALF=0.	SETI 220
	CORRECT=.FALSE.	SETI 230
	CGLA=.25	SETI 240
	CGLC=.25	SETI 250
	MZLA=5	SETI 260
	MZLO=5	SETI 270
	PUNCH=.FALSE.	SETI 280
	METRIC=.FALSE.	SETI 290
	BODY=.FALSE.	SETI 300
	DLA=.FALSE.	SETI 310
	DLO=.FALSE.	SETI 320
	WMLA=-99999.	SETI 330
	WMLC=-99999.	SETI 340
	RAD=.FALSE.	SETI 350
	DO 5 I=1,3000	SETI 360
	5 DATA(I)=0.	SETI 370
	DO 10 I=1,8	SETI 380
	8P(I)=0.	SETI 390
	LONG(I)=.TRUE.	SETI 400
	10 LATR(I)=.FALSE.	SETI 410
	NBP=1	SETI 420
	NABP=1	SETI 430
	NMBP=1	SETI 440
	LON=.FALSE.	SETI 450
	LAT=.FALSE.	SETI 460
	READ (1,WIND)	SETI 470
	IF (ABS(XB)+ABS(ZB)+ABS(XALF)+ABS(XAN)+ABS(ZAX)+ABS(XAY)+ABS(ZAY)	SETI 480
	- .NE. 0.) CORRECT=.TRUE.	SETI 490
	DO 40 I=1,NBP	SETI 500
	IF (.NOT. LATR(I)) GO TO 30	SETI 510
	LONG(I)=.FALSE.	SETI 520
	30 IF (LONG(I)) GO TO 35	SETI 530
	LAT=.TRUE.	SETI 540
	GO TO 40	SETI 550
	35 LON=.TRUE.	SETI 560

# APPENDIX C — Continued

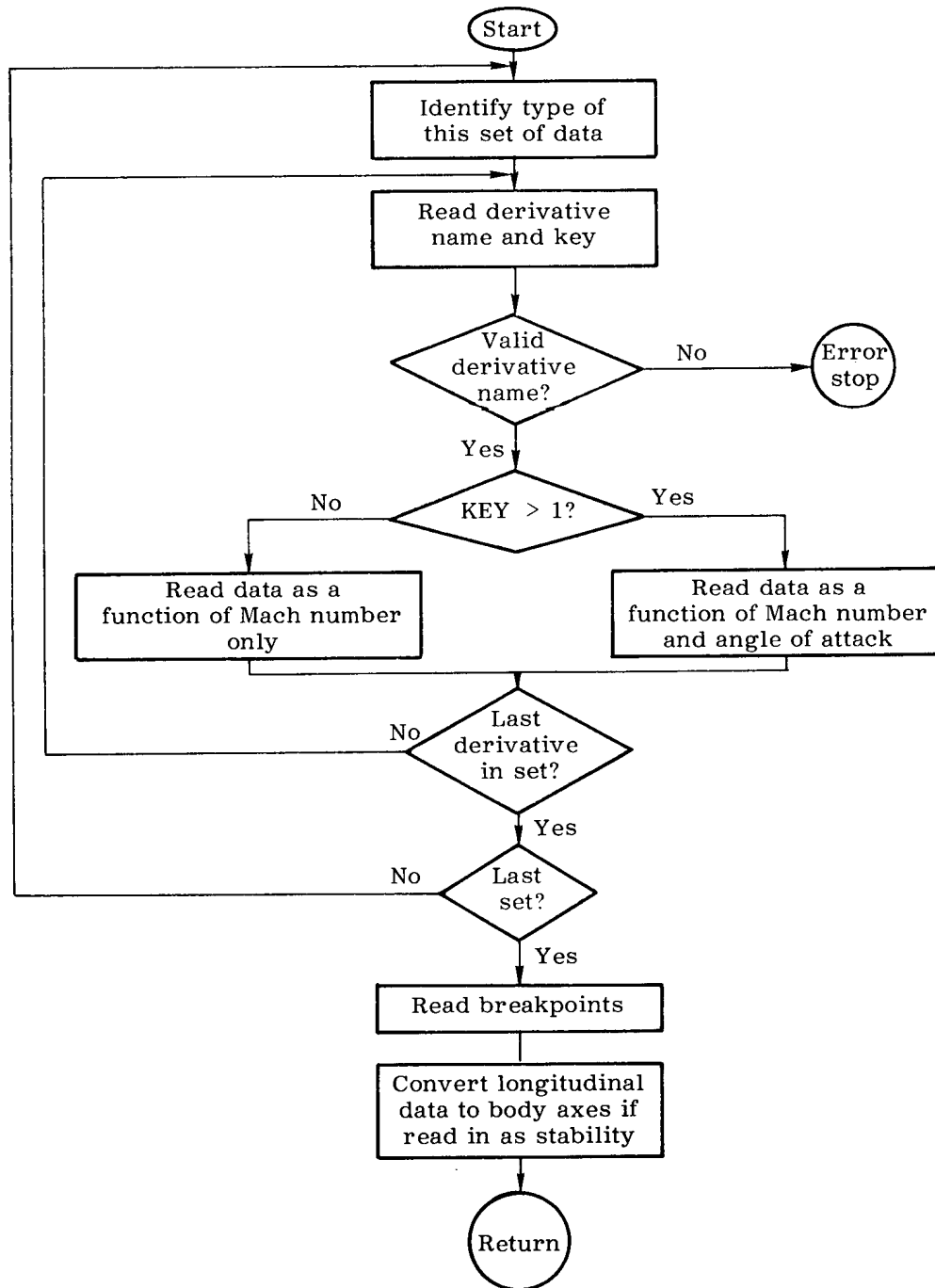
40 CONTINUE	SETI 570
READ (1,1000) VEH	SETI 580
IF(LAT) READ (1,1001) D1LA	SETI 590
IF(LON) READ (1,1001) D1LO	SETI 600
IF(D1LA(1)+D1LA(2)+D1LA(3)+D1LA(4)+D1LA(5).GT.0.) DLA=.TRUE.	SETI 610
IF(D1LO(1)+D1LO(2)+D1LO(3)+D1LO(4)+D1LO(5).GT.0.) DLO=.TRUE.	SETI 620
IF(WMLA.LT.0.) GO TO 50	SETI 630
CALL LOAD1(APRALA)	SETI 640
CALL LOAD1(APRBLA)	SETI 650
50 IF(WMLO.LT.0.) GO TO 60	SETI 660
CALL LOAD1(APRALO)	SETI 670
CALL LOAD1(APRBL0)	SETI 680
60 WRITE(3,2000)VEH,CGLA,CGLO,RAD	SETI 690
CALL WINDIN(DATA,NBP,NMBP,NABP,BODY,.TRUE.,RAD)	SETI 700
CALL COND1	SETI 710
1000 FORMAT(2A4)	SETI 720
1001 FORMAT(7F10.4)	SETI 730
2000 FORMAT(1H1,2A4,5X,27HWIND TUNNEL DATA. REF CG =,F5.3,7H (LAT),,	SETI 740
- F5.3,23H (LONG) PER RACIAN? ,L1)	SETI 750
RETURN	SETI 760
END	SETI 770

# APPENDIX C – Continued

## SUBROUTINE WINDIN

Description: Subroutine WINDIN reads in predicted derivatives, converting longitudinal data from the stability axes to the body axes if required.

Flow chart:



## APPENDIX C — Continued

Programing notes: The loop from cards 770 to 1000 is written in a more expanded form than necessary to improve its efficiency.

### Subroutine listing:

C	SUBROUTINE WINDIN(DATA,NBP,NMBP,NABP,BODY,PRINT,RAD)	WIND 0
C	READS IN WIND TUNNEL DATA	WIND 10
C		WIND 20
C	DATA IS DIMENSIONED (NBP,NMBP,NABP,NCMAX) WITH THE LAST 2	WIND 30
C	DIMENSIONS HANDLED IN FORTRAN FOR COMPILERS LIMITED TO 3-D	WIND 40
	COMMON /WTDATA/ NCLA,NCLO,ABP,MBP,8P,NCMAX,LONG	WIND 50
	REAL DATA(NBP,NMBP,1),ABP(16),MBP(16),8P(8),DER(21,3)	WIND 60
	LOGICAL LONG(8),BODY,PRINT,RAD	WIND 70
	INTEGER NNA8P(21)	WIND 80
	DATA DER/3HCYB,3HCLB,3HCNB,3HCLP,3HCNP,3HCLR,3HCNR,4HCYDA,4HCLDA,	WIND 90
	- 4HCNDA,4HCYDR,4HCLDR,4HCNDR,4HCYD1,4HCLD1,4HCND1,4HCYD2,	WIND 100
	- 4HCLD2,4HCND2,1H ,1H ,	WIND 110
	- 3HCLA,3HCMA,3MCDA,3HCMQ,3HCLV,3HCMV,3HCDV,4HCLDE,4HCMDE,	WIND 120
	- 4HCDE,4HCLDC,4HCMDC,4HCDDC,4HCLD1,4HCMO1,4HCDD1,4HCLD2,	WIND 130
	- 4HCMO2,4HCDD2,2HCL,2HCD,	WIND 140
	- 3HCNA,3HCMA,3HCAA,3HCMQ,3HCNV,3HCMV,3HCAV,4HCNDE,4HCMDE,	WIND 150
	- 4HCADE,4HCNDC,4HCMDC,4HCADC,4HCND1,4HCMO1,4HCAD1,4HCND2,	WIND 160
	- 4HCMO2,4HCAD2,2HCN,2HCA/	WIND 170
	NCMAX=21	WIND 180
C	READ NBP SETS OF WIND TUNNEL DATA	WIND 190
	DO 200 L=1,NBP	WIND 200
	NC=NCLA	WIND 210
	LL=1	WIND 220
	IF(.NOT.LONG(L)) GO TO 5	WIND 230
	NC=NCLO	WIND 240
	LL=2	WIND 250
	IF(BODY) LL=3	WIND 260
	5 IF(NC.EQ.0) GO TO 200	WIND 270
	DO 100 II=1,NC	WIND 280
C	READ AND IDENTIFY DERIVATIVE NAME	WIND 290
	READ (1,1002) DERIV,N	WIND 300
	IF(PRINT) WRITE(3,2000)DERIV	WIND 310
	DO 10 I=1,NCMAX	WIND 320
	IF(DERIV.EQ.DER(I,LL)) GO TO 20	WIND 330
10	CONTINUE	WIND 340
	WRITE(3,2001)DERIV	WIND 350
	STOP	WIND 360
C	INPUT DATA AS FUNCTION OF MACH AND ALPHA OR MACH ONLY	WIND 370
20	K2=I*NABP	WIND 380
	K1=K2-NABP+1	WIND 390
	IF(N.LE.1) GO TO 40	WIND 400
	DO 30 J=1,NMBP	WIND 410
	READ (1,1001) (DATA(L,J,K),K=K1,K2)	WIND 420
30	IF(PRINT) WRITE(3,2002)(DATA(L,J,K),K=K1,K2)	WIND 430
	GO TO 60	WIND 440
40	READ (1,1001) (DATA(L,J,K1),J=1,NMBP)	WIND 450
	IF(PRINT) WRITE(3,2002)(DATA(L,J,K1),J=1,NMBP)	WIND 460
	DO 50 J=1,NMBP	WIND 470
	DO 50 K=K1,K2	WIND 480
50	DATA(L,J,K)=DATA(L,J,K1)	WIND 490
60	IF(.NOT.RAD.OR.(I.GT.3.AND.I.LT.8).OR.I.GT.19) GO TO 100	WIND 500
	DO 70 J=1,NMBP	WIND 510
	DO 70 K=K1,K2	WIND 520
70	DATA(L,J,K)=DATA(L,J,K)/57.2958	WIND 530
100	CONTINUE	WIND 540
200	CONTINUE	WIND 550

# APPENDIX C — Continued

C		WIND 570
C	READ BREAKPOINTS	WIND 580
C		WIND 590
	READ (1,1001) (ABP(J),J=1,NABP)	WIND 600
	IF(PRINT) WRITE(3,2003) (ABP(J),J=1,NABP)	WIND 610
	READ (1,1001) (MBP(J),J=1,NMBP)	WIND 620
	IF(PRINT) WRITE(3,2004) (MBP(J),J=1,NMBP)	WIND 630
	READ (1,1001) (BP(J),J=1,8)	WIND 640
	IF(PRINT) WRITE(3,2005) (BP(J),J=1,NBP)	WIND 650
	IF(BODY) RETURN	WIND 660
C	CONVERT STABILITY TO BODY AXES	WIND 670
	DO 210 I=1,21	WIND 680
210	NNABP(I)=I*NABP	WIND 690
	DO 300 K=1,NABP	WIND 700
	DO 220 I=1,21	WIND 710
220	NNABP(I)=NNABP(I)+1	WIND 720
	SA=SIN(ABP(K)/57.2958)	WIND 730
	CA=COS(ABP(K)/57.2958)	WIND 740
	DO 300 L=1,NBP	WIND 750
	IF(.NOT.LONG(L)) GO TO 300	WIND 760
	DO 290 J=1,NMBP	WIND 770
	TEMP=DATA(L,J,NNABP(19))*CA+DATA(L,J,NNABP(20))*SA	WIND 780
	DATA(L,J,NNABP(20))=DATA(L,J,NNABP(20))*CA-TEMP	WIND 790
	DATA(L,J,NNABP(19))=TEMP	WIND 800
	TEMP=DATA(L,J,K)*CA+DATA(L,J,NNABP(21))*SA+DATA(L,J,NNABP(22))	WIND 810
	- /57.2958	WIND 820
	DATA(L,J,NNABP(21))=DATA(L,J,NNABP(21))*CA-TEMP	WIND 830
	- DATA(L,J,NNABP(19))/57.2958	WIND 840
	DATA(L,J,K)=TEMP	WIND 850
	TEMP=DATA(L,J,NNABP(4))*CA+DATA(L,J,NNABP(6))*SA	WIND 860
	DATA(L,J,NNABP(6))=DATA(L,J,NNABP(6))*CA-TEMP	WIND 870
	DATA(L,J,NNABP(4))=TEMP	WIND 880
	TEMP=DATA(L,J,NNABP(7))*CA+DATA(L,J,NNABP(9))*SA	WIND 890
	DATA(L,J,NNABP(9))=DATA(L,J,NNABP(9))*CA-TEMP	WIND 900
	DATA(L,J,NNABP(7))=TEMP	WIND 910
	TEMP=DATA(L,J,NNABP(10))*CA+DATA(L,J,NNABP(12))*SA	WIND 920
	DATA(L,J,NNABP(12))=DATA(L,J,NNABP(12))*CA-TEMP	WIND 930
	DATA(L,J,NNABP(10))=TEMP	WIND 940
	TEMP=DATA(L,J,NNABP(13))*CA+DATA(L,J,NNABP(15))*SA	WIND 950
	DATA(L,J,NNABP(15))=DATA(L,J,NNABP(15))*CA-TEMP	WIND 960
	DATA(L,J,NNABP(13))=TEMP	WIND 970
	TEMP=DATA(L,J,NNABP(16))*CA+DATA(L,J,NNABP(18))*SA	WIND 980
	DATA(L,J,NNABP(18))=DATA(L,J,NNABP(18))*CA-TEMP	WIND 990
280	DATA(L,J,NNABP(16))=TEMP	WIND1000
300	CONTINUE	WIND1010
1001	FORMAT(8F10.4)	WIND1020
1002	FORMAT(A4,4X,I2)	WIND1030
2000	FORMAT(1X,A8)	WIND1040
2001	FORMAT(1X,A8,49HIS NOT A VALID DERIVATIVE NAME FOR THIS TYPE CASE)	WIND1050
2002	FORMAT(5X,10E13.5)	WIND1060
2003	FORMAT(18H ALPHA BREAKPOINTS/5X,10F13.5)	WIND1070
2004	FORMAT(17H MACH BREAKPOINTS/5X,10F13.5)	WIND1080
2005	FORMAT(18H PARAM BREAKPOINTS/5X,10F13.5)	WIND1090
	RETURN	WIND1100
	END	WIND1110

## APPENDIX C — Continued

### SUBROUTINE TAPERD

Description: Subroutine TAPERD supervises the reading of the input tape and obtains averages of the channels read in. It also writes the output file if desired. It calls TAPEIN, the user-supplied input routine, to do the actual reading of the input tape.

Subroutine listing:

SUBROUTINE TAPERD	TAPE 0
COMMON /OPTION/ TAPE,DECK,READ	TAPE 10
COMMON /FLCOND/ ALPHA,THETA,Q,V,MACH,IX,IY,IZ,IXZ,W,PHI,CG,KIAS,	TAPE 20
- ALT, LONG, PARAM, FLT, CASE, AVG, DELTA, ST, ET, DETRIM	TAPE 30
REAL MACH, IX, IY, IZ, IXZ, KIAS, AVG(40), DATA(40,100)	TAPE 40
LOGICAL TAPE, DECK, READ, DELTA(4)	TAPE 50
INTEGER ST(4), ET(4), TIME(4,100), JST(4)	TAPE 60
NFRAME=100	TAPE 70
DO 10 I=1,40	TAPE 80
10 AVG(I)=0.	TAPE 90
NPT=0	TAPE 100
20 CALL TAPEIN(DATA,TIME,NFRAME,ST,ET)	TAPE 110
NFR=IABS(NFRAME)	TAPE 120
DO 100 I=1,NFR	TAPE 130
IF(TAPE) WRITE (4) (TIME(J,I),J=1,4), (DATA(J,I),J=1,25)	TAPE 140
DO 30 J=1,40	TAPE 150
30 AVG(J)=AVG(J)+DATA(J,I)	TAPE 160
NPT=NPT+1	TAPE 170
IF(NPT,NE.1) GO TO 100	TAPE 180
DO 40 J=1,4	TAPE 190
40 JST(J)=TIME(J,I)	TAPE 200
100 CONTINUE	TAPE 210
IF(NFRAME.GT.0) GO TO 20	TAPE 220
110 ANPT=NPT	TAPE 230
DO 120 I=1,40	TAPE 240
120 AVG(I)=AVG(I)/ANPT	TAPE 250
WRITE (3,2000)NPT,JST,(TIME(J,NFR),J=1,4),AVG	TAPE 260
2000 FORMAT(1H0,I5,22H POINTS IN CASE. TIMES,4I4,4H TO,4I4/	TAPE 270
- 17H0CHANNEL AVERAGES/(10X,10F12.4))	TAPE 280
RETURN	TAPE 290
END	TAPE 300

## APPENDIX C – Continued

### SUBROUTINE PNCH

Description: Subroutine PNCH dimensionalizes coefficients and punches the MMLE card deck.

Programing notes: Through card 540, this subroutine contains some computations and initializations used in all cases. Then cards 590 to 980 contain the lateral-directional dimensionalization and computations; cards 1030 to 1390 contain this information for the longitudinal cases. The remaining cards control the punching of the output deck.

Subroutine listing:

```

SUBROUTINE PNCH
COMMON /FLCON0/ ALPHA,THETA,Q,V,MACH,IX,IY,IZ,IXZ,W,PHI,CG,KIAS,
- ALT, LONG, PARAM, FLT, CASE, AVG, DELTA, ST, ET, DETRIM
COMMON /COM/ MZLA,MZLO,S,SPAN,CBAR,CGLA,CGL0,METRIC,D1LO,
- D1LA,VEH,APRALA,APRBLA,APRALO,APRBLO,WMLA,WMLO,PUNCH,CORRECT,
- XALF,XB,ZB,XAN,ZAX,XAY,ZAY,SPS,DLA,DLO
COMMON /DATAW/ NBP,NMBP,NABP,DATA
REAL MACH,IX,IY,IZ,IXZ,KIAS,AVG(40),DATA(3000),D1LO(7),D1LA(7),
- VEH(2),APRALA(5,4),APRALO(5,4),APRBLA(5,8),APRBLO(5,8),
- A(5,4),B(5,5),BB(5,5),X(21),MASS
INTEGER ST(4),ET(4),FLT,CASE
LOGICAL LONG,DELTA(4),METRIC,PUNCH,CORRECT,DLA,DLO
DATA ALAB,BLAB,BBLAB,ALAT,ALON/1HA,1HB,2HBB,4HLATR,4HLONG/
A(5,1)=4.
A(5,2)=4.
A(5,3)=ALAB
B(5,1)=4.
B(5,2)=5.
B(5,3)=BLAB
CALL AZOT(A)
CALL AZOT(B)
CALL AMAKE(BB,B)
BB(5,3)=BBLAB
BB(1,5)=1.
BB(2,5)=1.
BB(4,5)=1.
CALL COND
TIMESC=.5
IT=((ET(1)-ST(1))*3600+(ET(2)-ST(2))*60+ET(3)-ST(3))*1000+
- ET(4)-ST(4)
IF(IT.GT.12500) TIMESC=1.
IF(IT.GT.25000) TIMESC=2.
CALL INTERP(DATA,NBP,NMBP,NABP,X)
RAD=57.2958
CGFLT=CG
IF(CG.NE.999.) GO TO 7
3007 FORMAT(44H0CG NOT SPECIFIED. DEFAULTED TO WIND TUNNEL.)
WRITE(3,3007)
CGFLT=CGLA
IF(LONG) CGFLT=CGL0
7 DCG=0.
ALPR=ALPHA/RAD
THETR=THETA/RAD
PHIR=PHI/RAD
STH=SIN(THETR)
CT=COS(THETR)
CP=COS(PHIR)
G=32.172
IF(METRIC) G=9.80665
MASS=W/G
QS=Q*S
QSOMV=QS/(MASS*V)
WRITE(2,3000) VEH,FLT,CASE,MACH,ALPHA,PARAM,W,IX,IY,IZ,IXZ,Q,V,
- PUNCH,TIMESC
WRITE(3,2000) ALPHA,MACH,Q,V,CGFLT,PARAM
IF(LONG) GO TO 100

```

PNCH 0  
 PNCH 10  
 PNCH 20  
 PNCH 30  
 PNCH 40  
 PNCH 50  
 PNCH 60  
 PNCH 70  
 PNCH 80  
 PNCH 90  
 PNCH 100  
 PNCH 110  
 PNCH 120  
 PNCH 130  
 PNCH 140  
 PNCH 150  
 PNCH 160  
 PNCH 170  
 PNCH 180  
 PNCH 190  
 PNCH 200  
 PNCH 210  
 PNCH 220  
 PNCH 230  
 PNCH 240  
 PNCH 250  
 PNCH 260  
 PNCH 270  
 PNCH 280  
 PNCH 290  
 PNCH 300  
 PNCH 310  
 PNCH 320  
 PNCH 330  
 PNCH 340  
 PNCH 350  
 PNCH 360  
 PNCH 370  
 PNCH 380  
 PNCH 390  
 PNCH 400  
 PNCH 410  
 PNCH 420  
 PNCH 430  
 PNCH 440  
 PNCH 450  
 PNCH 460  
 PNCH 470  
 PNCH 480  
 PNCH 490  
 PNCH 500  
 PNCH 510  
 PNCH 520  
 PNCH 530  
 PNCH 540  
 PNCH 550  
 PNCH 560

C

# APPENDIX C — Continued

C	LATERAL	PNCH 570
C		PNCH 580
	WMAPR=ABS(WMLA)	PNCH 590
	IF(.NOT.CORECT) GO TO 10	PNCH 600
	DCG=CGFLT-CGLA	PNCH 610
	XBC=XB	PNCH 620
	XAYC=XAY	PNCH 630
	IF(XB.NE.0.) XBC=XBC+DCG*CBAR	PNCH 640
	IF(XAY.NE.0.) XAYC=XAYC+DCG*CBAR	PNCH 650
	WRITE(2,3001)XBC,ZR,XAYC,ZAY	PNCH 660
10	TYPE=ALAT	PNCH 670
	BB(3,5)=1.	PNCH 680
	QSOMV=QSOMV*RAD	PNCH 690
	QSB=QS*SPAN/RAD	PNCH 700
	QSBIX=QSB/IX	PNCH 710
	QSBIZ=QSB/IZ	PNCH 720
	B2V=SPAN/(2.*V*RAD)	PNCH 730
	QSBVIX=QSBIX*B2V	PNCH 740
	QSBVIZ=QSBIZ*B2V	PNCH 750
	DCG=DCG*CBAR/SPAN	PNCH 760
	A(1,1)=QSOMV*X(1)	PNCH 770
	A(2,1)=QSBIX*X(2)	PNCH 780
	A(3,1)=QSBIZ*(X(3)+DCG*X(1))	PNCH 790
	A(1,2)=SIN(ALPR)	PNCH 800
	A(2,2)=QSBVIX*X(4)	PNCH 810
	A(3,2)=QSBVIZ*X(5)	PNCH 820
	A(4,2)=1.	PNCH 830
	A(1,3)=-COS(ALPR)	PNCH 840
	A(2,3)=QSBVIX*X(6)	PNCH 850
	A(3,3)=QSBVIZ*X(7)	PNCH 860
	A(4,3)=CP*STH/CT	PNCH 870
	A(1,4)=CP*CT*G/V	PNCH 880
	DO 20 I=1,4	PNCH 890
	J=3*I+5	PNCH 900
	B(1,I)=QSOMV*X(J)	PNCH 910
	B(2,I)=QSBIX*X(J+1)	PNCH 920
	B(3,I)=QSBIZ*(X(J+2)+DCG*X(J))	PNCH 930
	IF(.NOT.DELTA(I)) GO TO 20	PNCH 940
	BB(1,I)=1.	PNCH 950
	BB(2,I)=1.	PNCH 960
	BB(3,I)=1.	PNCH 970
20	CONTINUE	PNCH 980
	GO TO 200	PNCH 990
C		PNCH1000
C	LONGITUDINAL	PNCH1010
C		PNCH1020
100	WMAPR=ABS(WML0)	PNCH1030
	IF(.NOT.CORECT) GO TO 110	PNCH1040
	DCG=CGFLT-CGL0	PNCH1050
	XALFC=XALF	PNCH1060
	XANC=XAN	PNCH1070
	IF(XALFC.NE.0.) XALFC=XALFC+DCG*CBAR	PNCH1080
	IF(XANC.NE.0.) XANC=XANC+DCG*CBAR	PNCH1090
	WRITE(2,3003)XALFC,XANC,7AX	PNCH1100
110	TYPE=ALON	PNCH1110
	WRITE(2,3002)	PNCH1120
	QSOM=QSOMV*V	PNCH1130



# APPENDIX C — Continued

```

QSCIY=QS*CBAR/IY
V2=2./V
QSCVIY=QSCIY*CBAR/(2.*V)
A(1,1)=-QSOMV*X(1)*RAD
A(2,1)=QSCIY*(X(2)*RAD-DCG*A(1,1)/QSOMV)
A(3,1)=-QSOM*X(3)*RAD
A(1,2)=1.
A(2,2)=QSCVIY*X(4)
A(4,2)=CP
A(1,3)=-QSOMV*V2*X(5)
A(2,3)=QSCIY*V2*X(6)
A(3,3)=-QSOM*V2*X(7)
A(1,4)=-STH*CP*G/V
A(3,4)=-CT*G
DO 130 I=1,4
J=3*I+5
B(1,I)=-QSOMV*X(J)*RAD
B(2,I)=QSCIY*(X(J+1)*RAD-DCG*B(1,I)/QSOMV)
B(3,I)=-QSOM*X(J+2)*RAD
IF(.NOT.DELTA(I)) GO TO 130
BB(1,I)=1.
BB(2,I)=1.
130 CONTINUE
B(1,5)=-QSOMV*X(20)-(A(1,1)*ALPHA+B(1,1)*DETRIM)/RAD+CP*CT*G/V
B(2,5)=- (A(2,1)*ALPHA+B(2,1)*DETRIM)/RAD
B(3,5)=-QSOM*X(21)-(A(3,1)*ALPHA+B(3,1)*DETRIM)/RAD
210 IF(WMAPR.EQ.99999.) WMAPR=0.
WRITE(2,3004) WMAPR,ALPHA,MACH,CGFLT,PARAM,TYPE,S,SPAN,CBAR,SPS.
1 ST,ET
CALL PMAT(A)
CALL PMAT(B)
IF(DELTA(1).OR.DELTA(2).OR.DELTA(3).OR.DELTA(4)) CALL PMAT(BB)
IF(LONG) GO TO 210
IF(DLA) WRITE(2,3005) MZLA,D1LA
IF(WMLA.LT.0.) GO TO 250
CALL PMAT1(APRALA)
CALL PMAT1(APRELA)
GO TO 250
210 IF(DLO) WRITE(2,3005) MZLO,D1LO
IF(WMLO.LT.0.) GO TO 250
CALL PMAT1(APRALO)
CALL PMAT1(APRLO)
250 WRITE(2,3006)
RETURN
2300 FORMAT(8H0ALPHA =,F6.2,9H MACH =,F5.3,6H Q =,F7.1,6H V =,
- F7.1,7H CG =,F5.3,10H PARAM =,F10.4)
3000 FORMAT(2A4,6X,6HFLIGHT,I4,6H CASE,I4,6X,5HMACH=,F5.3,
- 8H ALPHA=,F6.2,8H PARAM=,F7.2/15H $INPUT GROSSWT=,F7.0,
- 6H ,IX=,F7.0,6H ,IY=,F7.0,6H ,IZ=,F7.0,7H ,IXZ=,F7.1,1H,/PNCH1620
- 3H Q=,F6.1,5H ,V=,F6.1,9H ,PUNCH=,L1,1CH ,TIMESC=,F3.1,
- 10H ,00TH=T,)
3001 FORMAT(4H XB=,F6.2,6H ,ZB=,F6.2,7H ,XAY=,F6.2,7H ,ZAY=,F6.2,
- 1H,)
3002 FORMAT(15H ZMAX(3)=1000..)
3003 FORMAT(6H XALF=,F6.2,7H ,XAN=,F6.2,7H ,ZAX=,F6.2,1H,)
3004 FORMAT(7H WMAPR=,E8.2,9H ,ALPHA=,F6.2,8H ,MACH=,F5.3,6H ,CG=,
- F5.3,9H ,PARAM=,F10.4,1H,/1X,A4,7H=T, S=,F5.0,

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PNCH1140  
 PNCH1150  
 PNCH1160  
 PNCH1170  
 PNCH1180  
 PNCH1190  
 PNCH1200  
 PNCH1210  
 PNCH1220  
 PNCH1230  
 PNCH1240  
 PNCH1250  
 PNCH1260  
 PNCH1270  
 PNCH1280  
 PNCH1290  
 PNCH1300  
 PNCH1310  
 PNCH1320  
 PNCH1330  
 PNCH1340  
 PNCH1350  
 PNCH1360  
 PNCH1370  
 PNCH1380  
 PNCH1390  
 PNCH1400  
 PNCH1410  
 PNCH1420  
 PNCH1430  
 PNCH1440  
 PNCH1450  
 PNCH1460  
 PNCH1470  
 PNCH1480  
 PNCH1490  
 PNCH1500  
 PNCH1510  
 PNCH1520  
 PNCH1530  
 PNCH1540  
 PNCH1550  
 PNCH1560  
 PNCH1570  
 PNCH1580  
 PNCH1590  
 PNCH1600  
 PNCH1610  
 PNCH1620  
 PNCH1630  
 PNCH1640  
 PNCH1650  
 PNCH1660  
 PNCH1670  
 PNCH1680  
 PNCH1690  
 PNCH1700

## APPENDIX C — Continued

-	8H ,SPAN=,F6.2,8H ,CHAR=,F6.2,7H ,SPS=,F4.0,7H, \$END/	PNCH1710
-	2(3I2,I3,1X))	PNCH1720
3005	FORMAT(2H01,7X,I1/7F10.1)	PNCH1730
3006	FORMAT(7HENDCASE)	PNCH1740
	END	PNCH1750

## APPENDIX C — Continued

### SUBROUTINE INTERP

Description: Subroutine INTERP interpolates predicted derivative data tables to obtain the nondimensional derivatives for a particular flight condition.

Programing notes: The subroutine first brackets the Mach number and angle of attack of the flight condition between breakpoints of the predicted data; it also selects the correct set of predicted data depending on the value of PARAM. The interpolation is divided into four sections. The interpolation occurs in one of the four sections on the basis of how many Mach and angle-of-attack breakpoints are specified. If only one breakpoint is specified, the required code changes slightly, because there are not two points to interpolate between.

#### Subroutine listing:

C	SUBROUTINE INTERP(DATA,NBP,NMBP,NABP,X)	INTE 0
C	INTERPOLATES WIND TUNNEL DATA	INTE 10
C	COMMON /FLCOND/ ALPHA,THETA,Q,V,MACH,IX,IY,IZ,IXZ,W,PHI,CG,KIAS,	INTE 20
C	- ALT, LONG, PARAM, FLT, CASE, AVG, DELTA, ST, ET, DETRIM	INTE 30
C	COMMON /WTDATA/ NCLA, NCLO, ABP, MBP, BP, NCMA, LONGWT	INTE 40
C	REAL MACH, IX, IY, IZ, IXZ, KIAS, AVG(40), DATA(NBP, NMBP, 1), ABP(16),	INTE 50
C	- MBP(16), BP(8), X(21)	INTE 60
C	INTEGER ST(4), ET(4), FLT, CASE	INTE 70
C	LOGICAL DELTA(4), LONG, LONGWT(8), XORF	INTE 80
C	FIND CORRECT SET OF DATA	INTE 90
C	L=1	INTE 100
C	DO 60 II=1, NBP	INTE 110
C	XORF=(LONG.AND.LONGWT(II)).OR.(.NOT.LONG.AND..NOT.LONGWT(II))	INTE 120
C	60 IF((PARAM.EQ.BP(II)).OR.PARAM*BP(II).EQ.0.) .AND. XORF) L=II	INTE 130
C	BRACKET ALPHA	INTE 140
C	IF(NABP.EQ.1) GO TO 50	INTE 150
C	DO 40 J=2, NABP	INTE 160
C	IF(ALPHA.GT. ABP(J)) GO TO 41	INTE 170
C	EAP=(ALPHA-ABP(J-1))/(ABP(J)-ABP(J-1))	INTE 180
C	IF(EAP.LT.0.) EAP=0.	INTE 190
C	GO TO 50	INTE 200
C	40 CONTINUE	INTE 210
C	J=NABP	INTE 220
C	EAP=1.	INTE 230
C	BRACKET MACH NUMBER	INTE 240
C	50 IF(NMBP.EQ.1) GO TO 100	INTE 250
C	DO 20 I=2, NMBP	INTE 260
C	IF(MACH.GT. MBP(I)) GO TO 20	INTE 270
C	EMN=(MACH-MBP(I-1))/(MBP(I)-MBP(I-1))	INTE 280
C	IF(EMN.LT.0.) EMN=0.	INTE 290
C	GO TO 30	INTE 300
C	20 CONTINUE	INTE 310
C	I=NMBP	INTE 320
C	EMN=1.	INTE 330
C	30 IM1=I-1	INTE 340
C	IF(NABP.EQ.1) GO TO 120	INTE 350
C	INTERPOLATE DATA	INTE 360
C	DO 90 K=1, NCMA	INTE 370
C	JK=(K-1)*NABP+J	INTE 380
C	JM1K=JK-1	INTE 390
C	PA=(DATA(L,I,JK)-DATA(L,IM1,JK))*EMN+DATA(L,IM1,JK)	INTE 400
C	PB=(DATA(L,I,JM1K)-DATA(L,IM1,JM1K))*EMN+DATA(L,IM1,JM1K)	INTE 410
C	90 X(K)=(PA-PB)*EAP+PB	INTE 420
C	GO TO 200	INTE 430
C	100 IF(NABP.EQ.1) GO TO 140	INTE 440
C	INTERPOLATE IF ONLY 1 MACH BREAKPOINT	INTE 450
C	DO 110 K=1, NCMA	INTE 460
C	JK=(K-1)*NABP+J	INTE 470
C	JM1K=JK-1	INTE 480
C	110 X(K)=DATA(L,I,JM1K)+EAP*(DATA(L,I,JK)-DATA(L,I,JM1K))	INTE 490
C	GO TO 200	INTE 500
C	IF ONLY 1 ALPHA BREAKPOINT	INTE 510
C	120 DO 130 K=1, NCMA	INTE 520
C	130 X(K)=(DATA(L,I,K)-DATA(L,IM1,K))*EMN+DATA(L,IM1,K)	INTE 530
C	GO TO 200	INTE 540
C		INTE 550
C		INTE 560

## APPENDIX C — Continued

C	IF ONLY 1 ALPHA AND 1 MACH BREAKPOINT	INTE 570
140	DO 150 K=1,NCMAX	INTE 580
150	X(K)=DATA(L,1,K)	INTE 590
200	RETURN	INTE 600
	END	INTE 610

### SUBROUTINE PMAT

Description: Subroutine PMAT punches a matrix on cards in an 8F10.5 format.

Subroutine listing:

C	SUBROUTINE PMAT(A)	PMAT 0
	PUNCHES A MATRIX	PMAT 10
	COMMON /ALLOIM/ MAX,MIX	PMAT 20
	REAL A(1)	PMAT 30
	II=A(MAX)	PMAT 40
	JJ=A(2*MAX)	PMAT 50
	WRITE(2,1000) A(3*MAX),II,JJ	PMAT 60
	KE=(JJ-1)*MAX	PMAT 70
	DO 20 I=1,II	PMAT 80
	KEND=I+KE	PMAT 90
20	WRITE(2,1001) (A(K),K=I,KEND,MAX)	PMAT 100
	CALL ASPIT(A)	PMAT 110
1000	FORMAT(A4,4X,I2,I10)	PMAT 120
1001	FORMAT(8F10.5)	PMAT 130
	RETURN	PMAT 140
	END	PMAT 150

### SUBROUTINE PMAT1

Description: Subroutine PMAT1 punches a matrix on cards in an 8E10.3 format.

Programing notes: This subroutine is needed in addition to PMAT because the APRA and APRB matrices may contain large values but do not need as many significant figures as other matrices.

Subroutine listing:

C	SUBROUTINE PMAT1(A)	PMAT 0
	PUNCHES A MATRIX IN E FORMAT	PMAT 10
	COMMON /ALLOIM/ MAX,MIX	PMAT 20
	REAL A(1)	PMAT 30
	II=A(MAX)	PMAT 40
	JJ=A(2*MAX)	PMAT 50
	WRITE(2,1000) A(3*MAX),II,JJ	PMAT 60
	KE=(JJ-1)*MAX	PMAT 70
	DO 20 I=1,II	PMAT 80
	KEND=I+KE	PMAT 90
20	WRITE(2,1001) (A(K),K=I,KEND,MAX)	PMAT 100
1000	FORMAT(A4,4X,I2,I10)	PMAT 110
1001	FORMAT(8E10.3)	PMAT 120
	RETURN	PMAT 130
	END	PMAT 140

## APPENDIX C — Continued

### SUBROUTINE RDSET

Description: Subroutine RDSET is user supplied; the subroutine listed here is a sample. This subroutine should do any initialization or input required before calling subroutine TAPEIN.

#### Subroutine listing:

	SUBROUTINE RDSET	RDSE 9
		RDSE 10
C	THIS SUBROUTINE SHOULD INCLUDE ANY INITIALIZATION DESIRED FOR	RDSE 20
C	READING THE INPUT TAPE, FOR INSTANCE SPECIFYING CHANNEL NUMBERS.	RDSE 30
C	DATA SHOULD BE PASSED TO SUBROUTINE TAPEIN WITH LABELLED COMMON	RDSE 40
C	BLOCK /TAPDAT/	RDSE 50
C	THIS SAMPLE VERSION READS THE NUMBER OF WORDS ON THE INPUT TAPE	RDSE 60
C	AND THE CHANNEL NUMBERS OF THE SIGNALS NEEDED	RDSE 70
C		RDSE 80
	COMMON /TAPDAT/ NWORD, ICHAN	RDSE 90
	INTEGER ICHAN(40)	RDSE 100
	READ (1,1000) NWORD	RDSE 110
	READ (1,1000) ICHAN	RDSE 120
	WRITE(3,2000) NWORD, ICHAN	RDSE 130
1000	FORMAT(16I5)	RDSE 140
2000	FORMAT(20H0INPUT FILE CONTAINS,15,22H DATA WORDS PER RECORD/ 9H CHANNELS/(10X,20I5))	RDSE 150
	RETURN	RDSE 160
	END	RDSE 170
		RDSE 180

## APPENDIX C – Continued

### SUBROUTINE TAPEIN

Description: Subroutine TAPEIN is user supplied; the subroutine listed here is a sample. This subroutine should be written to read data in the form available for a particular flight program. The comment cards and sample program illustrate the conventions required for interface with the rest of the program.

Subroutine listing:

	<pre> SUBROUTINE TAPEIN(DATA,TIME,NFRAME,ST,ET) C C THIS SUBROUTINE SHOULD READ THE INPUT TAPE AND PLACE UP TO C NFRAME FRAMES IN THE TIME INTERVAL BETWEEN ST AND ET (START TIME C AND END TIME) INTO THE ARRAYS TIME AND DATA C THE TIME ARRAY SHOULD CONTAIN HOURS,MINUTES,SECONDS,MILLISECONDS C THE DATA ARRAY SHOULD CONTAIN THE DATA CHANNELS IN THE ORDER TO C WRITTEN ON THE OUTPUT TAPE C WHEN THE LAST TIME IN THE REQUESTED INTERVAL IS FOUND, C NFRAME SHOULD BE SET TO MINUS THE NUMBER OF FRAMES OF DATA C BEING RETURNED C C THIS SAMPLE VERSION READS AN UNFORMATTED TAPE AND PICKS THE C SIGNALS DESIRED FROM THE CHANNELS SPECIFIED IN SUBROUTINE RDSET C COMMON /TAPDAT/ NWORD,ICHAN INTEGER ST(4),ET(4),TIME(4,100),ICHAN(40),IT(4) REAL DATA(40,100),RECORD(150) IST=ST(4)+1000*(ST(3)+60*ST(2)+3600*ST(1)) IET=ET(4)+1000*(ET(3)+60*ET(2)+3600*ET(1)) I=0 10 READ (15) IT,(RECORD(J),J=1,NWORD) ITM=IT(4)+1000*(IT(3)+60*IT(2)+3600*IT(1)) IF(ITM.LT.IST) GO TO 10 I=I+1 20 DO 30 J=1,4 TIME(J,I)=IT(J) DO 40 J=1,40 DATA(J,I)=0. IF(ICHAN(J).EQ.0) GO TO 40 DATA(J,I)=RECORD(ICHAN(J)) 40 CONTINUE IF(I.GE.NFRAME) RETURN IF(ITM.GE.IET) GO TO 100 READ (15) IT,(RECORD(J),J=1,NWORD) ITM=IT(4)+1000*(IT(3)+60*IT(2)+3600*IT(1)) GO TO 20 100 NFRAME=-I RETURN 40 END </pre>	<pre> TAPE 0 TAPE 10 TAPE 20 TAPE 30 TAPE 40 TAPE 50 TAPE 60 TAPE 70 TAPE 80 TAPE 90 TAPE 100 TAPE 110 TAPE 120 TAPE 130 TAPE 140 TAPE 150 TAPE 160 TAPE 170 TAPE 180 TAPE 190 TAPE 200 TAPE 210 TAPE 220 TAPE 230 TAPE 240 TAPE 250 TAPE 260 TAPE 270 TAPE 280 TAPE 290 TAPE 300 TAPE 310 TAPE 320 TAPE 330 TAPE 340 TAPE 350 TAPE 360 TAPE 370 TAPE 380 TAPE 390 </pre>
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## APPENDIX C — Continued

### SUBROUTINE COND1

Description: Subroutine COND1 is user supplied, and is described by the comment cards.

Subroutine listing:

	SUBROUTINE COND1	COND 0
C		COND 10
C	THIS SUBROUTINE SHOULD INCLUDE ANY INITIALIZATION NEEDED	COND 20
C	FOR SUBROUTINE COND TO DETERMINE THE FLIGHT CONDITION	COND 30
C	TYPICAL ITEMS INCLUDED HERE MIGHT BE TABLES OF INERTIAS AS A	COND 40
C	FUNCTION OF GROSS WEIGHT	COND 50
C	ANY DATA MAY BE PASSED TO SUBROUTINE COND THROUGH A LABELLED	COND 60
C	COMMON BLOCK /TABLE/	COND 70
C	SUBROUTINE SUPPLIED IS A NULL SUBROUTINE	COND 80
C		COND 90
	RETURN	COND 100
	END	COND 110

### SUBROUTINE COND

Description: Subroutine COND is user supplied. It automatically obtains the flight condition from the channel averages computed by TAPERD. The subroutine listed illustrates the method of doing this.

Subroutine listing:

	SUBROUTINE COND	COND 0
C		COND 10
C	THIS SUBROUTINE SHOULD SPECIFY THE FLIGHT CONDITION AND OTHER	COND 20
C	PARAMETERS NOT READ IN THROUGH NAMELIST /COND/	COND 30
C	AVG CONTAINS THE AVERAGE VALUES OF EACH CHANNEL READ OFF THE INPUT	COND 40
C	TAPE IF THERE WAS ONE READ	COND 50
C	THE USER MAY CHOOSE TO USE THESE AVERAGE VALUES FOR THE FLIGHT	COND 60
C	CONDITION INSTEAD OF READING IT IN	COND 70
C	FOR INSTANCE, IF ALPHA IS TO BE OBTAINED FROM THE CHANNEL AVERAGE	COND 80
C	THE STATEMENT	COND 90
C	ALPHA=AVG(1)	COND 100
C	WOULD BE INCLUDED HERE	COND 110
C	THE SEVERAL EXTRA CHANNELS AVAILABLE MAY BE USED TO OBTAIN	COND 120
C	FUEL WEIGHTS OR OTHER QUANTITIES NEEDED TO COMPUTE THE INERTIAS	COND 130
C		COND 140
C	THE SUBROUTINE SUPPLIED OBTAINS ALPHA,THETA,PHI,DETRIM,Q,V,AND	COND 150
C	MACH FROM SIGNAL AVERAGES AND COMPUTES Q AND V FROM ALTITUDE	COND 160
C	AND KIAS(KNOTS INDICATED AIRSPEED) IF THESE ARE MORE READILY	COND 170
C	AVAILABLE (INDICATED BY A NON-ZERO VALUE OF KIAS)	COND 180
C		COND 190
	COMMON /OPTION/ TAPE,DECK,READ	COND 200
	COMMON /FLCOND/ ALPHA,THETA,Q,V,MACH,IX,IY,IZ,IXZ,W,PHI,CG,KIAS,	COND 210
-	ALT, LONG, PARAM, FLT, CASE, AVG, DELTA, ST, ET, DETRIM	COND 220
	REAL MACH, IX, IY, IZ, IXZ, KIAS, AVG(40)	COND 230
	INTEGER ST(4), ET(4), FLT, CASE	COND 240
	LOGICAL DELTA(4), LONG, TAPE, DECK, READ	COND 250
	IF(.NOT.READ) GO TO 10	COND 260
	ALPHA=AVG(1)	COND 270
	THETA=AVG(4)	COND 280
	PHI=AVG(12)	COND 290
	DETRIM=AVG(8)	COND 300
	Q=AVG(15)	COND 310
	V=AVG(13)	COND 320
	MACH=AVG(14)	COND 330
10	IF(KIAS.EQ.0.) RETURN	COND 340
	Q=(KIAS*.0502)**2	COND 350
	DALT=ALT*.001	COND 360
	V=1.688*KIAS*EXP(DALT*(.01375+.0000975*DALT))	COND 370
	RETURN	COND 380
	END	COND 390

## APPENDIX C — Concluded

### SUBROUTINE LOAD1

Description: Subroutine LOAD1 reads a matrix from cards.

Subroutine listing:

SUBROUTINE LOAD1(A)	LOAD 0
COMMON /ALLDIM/ MAX,MIX	LOAD 10
REAL A(1)	LOAD 20
MAX3=3*MAX	LOAD 30
READ (1,1000) A(MAX3),II,JJ	LOAD 40
A(MAX)=II	LOAD 50
A(2*MAX)=JJ	LOAD 60
KE=(JJ-1)*MAX	LOAD 70
DO 10 I=1,II	LOAD 80
KEND=I+KE	LOAD 90
10 READ (1,1001) (A(K),K=I,KEND,MAX)	LOAD 100
1000 FORMAT(A4,4X,I2,I10)	LOAD 110
1001 FORMAT(AF10,4)	LOAD 120
RETURN	LOAD 130
END	LOAD 140

### SUBROUTINES ASPIT, AMAKE, AND AZOT

Subroutines ASPIT, AMAKE, and AZOT are identical to those used in the MMLE program.



## APPENDIX D

### SAMPLE CASE FOR THE SETUP PROGRAM

This appendix presents a sample check case for the SETUP program.

#### INPUT CARDS

```
PUNCH DECK
START
$WIND NMBP=2,NARP=2,NCL0=8,LONG(1)=T,SPAN=15.,CBAR=6.,S=100.,$END
SAMPLE
0.
CL      2
.1      .5
0.      .4
CD      2
.05     .1
.07     .12
CLA     1
.07     .065
COA     1
.01     .015
CMA     1
-.005   -.006
CLOE    1
.01     .01
CMDE    1
-.009   -.011
CMQ     1
-5.     -5.
.3      .7
.0      5.
0.
102051000 102100000 SAMPLE CASE 1
$COND IX=300.,IY=2000.,IZ=2000.,IXZ=10.,W=2500.,LONG=T,
FLT=1,CASE=1,Q=50.,V=450.,ALPHA=4.,MACH=.5,$END
102512000 102522000 SAMPLE CASE 2
$COND CASE=2,O=60.,V=500.,ALPHA=3.,MACH=.55,$END
-1
```

# APPENDIX D — Continued

## OUTPUT LISTING

SAMPLE	WIND TUNNEL DATA.		REF CG = .250 (LAT), .250 (LONG)	PER RADIAN? F
CL	.10000E+00	.50000E+00		
	0.	.40000E+00		
CD	.50000E-01	.10000E+00		
	.70000E-01	.12000E+00		
CLA	.70000E-01	.65000E-01		
CDA	.10000E-01	.15000E-01		
CMA	-.50000E-02	-.50000E-02		
CLDE	.10000E-01	.10000E-01		
CMDE	-.90000E-02	-.11000E-01		
CMQ	-.50000E+01	-.50000E+01		
ALPHA BREAKPOINTS	.30000	.70000		
MACH BREAKPOINTS	0.00000	5.00000		
PARAM BREAKPOINTS	0.00000			

# APPENDIX D — Continued

```

      FLIGHT 1      CASE 1      TIME 10 20 51 0 TO 10 21 0 0      LONGITUDINAL? T
CG NOT SPECIFIED. DEFAULTED TO WIND TUNNEL.
ALPHA = 4.00  MACH = .500  Q = 50.0  V = 450.0  CG = .250  PARAM = 0.0000
A
      -.5841E+00  .1000E+01  -0.  -0.
      -.4383E+01  -.5000E+00  0.  0.
      -.3970E+01  0.  -0.  -.3217E+02
      0.  .1000E+01  0.  0.
      4 BY 5
B
      -.8192E-01  -0.  -0.  -0.  .4204E-01
      -.7907E+01  0.  0.  0.  .3060E+00
      .4504E+00  -0.  -0.  -0.  -.5900E+01
      0.  0.  0.  0.  0.

```

# APPENDIX D — Continued

```

      FLIGHT 1      CASE 2      TIME 10 25 12 0 TO 10 25 22 0      LONGITUDINAL? T
CG NOT SPECIFIED. DEFAULTED TO WIND TUNNEL.
ALPHA = 3.00  MACH = .550  Q = 60.0  V = 500.0  CG = .250  PARAM = 0.0000
A
      -.6304E+00  .1000E+01  -0.  -0.
      -.5270E+01  -.5400E+00  0.  0.
      -.5065E+01  0.  -0.  -.3217E+02
      0.  .1000E+01  0.  0.
B
      4 BY 5
      -.8847E-01  -0.  -0.  -0.  .2165E-01
      -.9509E+01  0.  0.  0.  .2759E+00
      .5405E+00  -0.  -0.  -0.  -.7164E+01
      0.  0.  0.  0.  0.

```

# APPENDIX D — Concluded PUNCHED CARD OUTPUT LISTING

```

SAMPLE      FLIGHT  1 CASE  1      MACH= .500 ALPHA= 4.00 PARAM= 0.00
$INPUT GROS WT= 2500. ,IX= 300. ,IY= 2000. ,IZ= 2000. ,IXZ= 10.0,
Q= 50.0 ,V= 450.0 ,PUNCH=F ,TIMESC= .5 ,BOTH=T,
ZMAX(3)=1000.,
WMAPR=0. ,ALPHA= 4.00 ,MACH= .500 ,CG= .250 ,PARAM= 0.0000,
LONG=T, S= 100. ,SPAN= 15.00 ,CBAR= 6.00 ,SPS= 0., $END
102051 0 1021 0 0
A      4      4
-1.58412 1.00000 -0.00000 -0.00000
-4.38313 -.50000 0.00000 0.00000
-3.97020 0.00000 -0.00000 -32.17200
0.00000 1.00000 0.00000 0.00000
B      4      5
-1.08192 -0.00000 -0.00000 -0.00000 .04204
-7.90682 0.00000 0.00000 0.00000 .30600
.45040 -0.00000 -0.00000 -0.00000 -5.90024
0.00000 0.00000 0.00000 0.00000 0.00000
ENDCASE
SAMPLE      FLIGHT  1 CASE  2      MACH= .550 ALPHA= 3.00 PARAM= 0.00
$INPUT GROS WT= 2500. ,IX= 300. ,IY= 2000. ,IZ= 2000. ,IXZ= 10.0,
Q= 60.0 ,V= 500.0 ,PUNCH=F ,TIMESC= .5 ,BOTH=T,
ZMAX(3)=1000.,
WMAPR=0. ,ALPHA= 3.00 ,MACH= .550 ,CG= .250 ,PARAM= 0.0000,
LONG=T, S= 100. ,SPAN= 15.00 ,CBAR= 6.00 ,SPS= 0., $END
102512 0 102522 0
A      4      4
-1.63044 1.00000 -0.00000 -0.00000
-5.27007 -.54000 0.00000 0.00000
-5.06514 0.00000 -0.00000 -32.17200
0.00000 1.00000 0.00000 0.00000
B      4      5
-1.08847 -0.00000 -0.00000 -0.00000 .02165
-9.50881 0.00000 0.00000 0.00000 .27594
.54048 -0.00000 -0.00000 -0.00000 -7.16407
0.00000 0.00000 0.00000 0.00000 0.00000
ENDCASE

```

## APPENDIX E

### SUMARY PROGRAM AND SUBROUTINES

Listings of the main program and the subroutines used in the SUMARY program are presented together with supplemental information.

#### MAIN PROGRAM SUMMARY

Description: The main program SUMARY sets defaults, reads the NAMELIST, and initializes variables.

#### Program listing:

```
PROGRAM SUMARY(INPUT,OUTPUT,TAPE69,TAPE1=INPUT,TAPE3=OUTPUT)      MAIN  0
C                                                                    MAIN 10
C SUMMARY PLCT PROGRAM FOR MMLE DATA                             MAIN 20
C                                                                    MAIN 30
COMMON /ALLOIM/ MAX,MIX                                           MAIN 40
COMMON /LINCOM/ HGT                                               MAIN 50
COMMON /WTDATA/ NCLA,NCLO,ABP,MBP,BP,NCMAX,LONG                  MAIN 60
COMMON /CGCOR/ SHIFT,CGLA,CGLO,COB                               MAIN 70
COMMON /NBPS/ NMBP,NABP,NBP,NPARAM                               MAIN 80
COMMON /INS/ NPLOT,WTPLLOT                                         MAIN 90
COMMON /SUMDAT/ YLOC,XSKIP,ALEN,ASCAL2,YSTEP,AMIN,TARLAB,FDATA.  MAIN 100
- FDATA, TITLE                                                    MAIN 110
COMMON /PSCL/ CFACT,IWT1,IWT2,YLEN2,II,NPARAM                   MAIN 120
REAL TITLE(20),ARP(16),BP(8),MPP(16),DATA(3000),FDATA(5000),    MAIN 130
- FDATA(5000),BUF(1024),FDAT(200),FDATC(200),ALFS(200),          MAIN 140
- TARLAB(2),MLAB(2),PLAB(2)                                       MAIN 150
LOGICAL PRINT, LONG(8),LATR(8),DEG,RAD,RODY,STAB,SHIFT,WTPLLOT  MAIN 160
DATA MLAB/4HMACH,1H /,PLAB/4HPARA,1HM/                          MAIN 170
NAMELIST /WIND/ NBP,NABP,NMBP,NCLA,NCLO,RAD,DEG,RODY,STAB,      MAIN 180
- LONG,LATR,PRINT,CGLA,CGLO,NPARAM,SHIFT,WTPLLOT,CFACT,        MAIN 190
- AMIN,AMAX,ASCALE,YLEN,XDIST,CBAR,SPAN                          MAIN 200
NBUF=1024                                                         MAIN 210
MAX=4                                                             MAIN 220
READ (1,1000) TITLE                                              MAIN 230
WRITE(3,2000) TITLE                                              MAIN 240
HGT=.07                                                           MAIN 250
SHIFT=.FALSE.                                                    MAIN 260
CBAR=0.                                                           MAIN 270
SPAN=1.E+50                                                       MAIN 280
NPARAM=0                                                           MAIN 290
NCLA=0                                                            MAIN 300
NCLO=0                                                            MAIN 310
NBP=1                                                             MAIN 320
CGLA=.25                                                          MAIN 330
CGLO=.25                                                          MAIN 340
NABP=1                                                            MAIN 350
NMBP=1                                                            MAIN 360
PRINT=.FALSE.                                                     MAIN 370
DO 5 I=1,3000                                                     MAIN 380
5 DATA(I)=0.                                                     MAIN 390
DO 10 I=1,8                                                       MAIN 400
LATR(I)=.FALSE.                                                  MAIN 410
LONG(I)=.TRUE.                                                    MAIN 420
10 BP(I)=0.                                                       MAIN 430
RAD=.FALSE.                                                       MAIN 440
STAB=.TRUE.                                                       MAIN 450
RODY=.FALSE.                                                      MAIN 460
WTPLLOT=.TRUE.                                                    MAIN 470
CFACT=1.                                                          MAIN 480
AMIN=0.                                                           MAIN 490
AMAX=12.                                                          MAIN 500
ASCALE=1.                                                         MAIN 510
YLEN=10.                                                         MAIN 520
XDIST=10.                                                         MAIN 530
READ (1,WIND)                                                     MAIN 540
NPARAM=NPARAM                                                     MAIN 550
COB=CBAR/SPAN                                                    MAIN 560
```

# APPENDIX E – Continued

	YLEN2=YLEN/2.	MAIN 570
	YLOC=0.	MAIN 580
	ASCAL2=ASCALE*2.	MAIN 590
	ALEN=(AMAX-AMIN)/ASCAL2	MAIN 600
	XSKIP=ALEN*XDIST/2.	MAIN 610
	YSTEP=YLEN2+1.	MAIN 620
	DO 20 I=1,8	MAIN 630
	20 IF(LATR(I)) LONG(I)=.FALSE.	MAIN 640
C	READ WIND TUNNEL DATA	MAIN 650
	CALL WINDIN(DATA,NBP,NMBP,NABP,BODY,PRINT,RAD)	MAIN 660
	IF(SHIFT) WRITE(3,2001)CGLA,CGLO	MAIN 670
	IF(CRFACT.NE.0.) WRITE(3,2002)CRFACT	MAIN 680
	IWT1=1	MAIN 690
	IWT2=1	MAIN 700
	DO 15 I=1,NABP	MAIN 710
	IF(ABP(I).LT.AMIN) IWT1=I+1	MAIN 720
15	IF(ABP(I).LE.AMAX) IWT2=I	MAIN 730
	NCMX=NCMAX+2	MAIN 740
	ND=NMBP*2	MAIN 750
	TABLAB(1)=MLAB(1)	MAIN 760
	TABLAB(2)=MLAB(2)	MAIN 770
	IF(NPARAM.LE.0) GO TO 25	MAIN 780
	ND=NPARAM*2	MAIN 790
	TABLAB(1)=PLAB(1)	MAIN 800
	TABLAB(2)=PLAB(2)	MAIN 810
25	ND2=ND/2	MAIN 820
C	READ FLIGHT DATA	MAIN 830
	CALL FLIGHT(NCMX,ND,FDATA,FDATAC)	MAIN 840
	CALL PLOTS(BUF,NBUF,69)	MAIN 850
	CALL FACTOR(.787402)	MAIN 860
	CALL PLOT(0.,.5,-3)	MAIN 870
C	READ PLOTTING INSTRUCTIONS	MAIN 880
30	CALL INSTR	MAIN 890
	IF(NPLOT.LE.0) GO TO 50	MAIN 900
C	MAKE PLOTS	MAIN 910
	DO 40 II=1,NPLOT	MAIN 920
40	CALL SUMPLY(FDAT,FDATC,ALFS,ND2,DATA,NBP,NMBP,NABP)	MAIN 930
	GO TO 30	MAIN 940
50	CALL PLOT(0.,0.,999)	MAIN 950
1000	FORMAT(20A4)	MAIN 960
2000	FORMAT(51H1MMLE SUMMARY PLOTTING PROGRAM **** 1 MAY 1974/	MAIN 970
	- 1H0,20X,20A4)	MAIN 980
2001	FORMAT(55H0CNE AND CMA WILL BE CORRECTED TO THE WIND TUNNEL REFER,	MAIN 990
	- 8HENCE CGS,F10.3,7H (LATR),F10.3,7H (LONG))	MAIN1000
2002	FORMAT(48H0CONFIDENCE LEVELS WILL BE PLOTTED MULTIPLIED BY,F5.1)	MAIN1010
	STOP	MAIN1020
	END	MAIN1030

# APPENDIX E – Continued

## SUBROUTINE FLIGHT

Description: Subroutine FLIGHT reads and sorts flight data.

Programing notes: Data are stored in the arrays FDATA and FDATA C. The FDATA array contains derivative values, and the FDATA C array contains confidence levels. Note that the sign of the X and Z coefficients is changed for longitudinal data to agree with the more common N and A (axial) coefficients. The flight  $C_{m\alpha}$

and  $C_{n\beta}$  are shifted to the wind-tunnel reference center of gravity if SHIFT = T.

LONLOC and LATLOC give the positions of data in the A and B matrices considered as vectors.

Subroutine listing:

```

C      SUBROUTINE FLIGHT(NCMX,ND,FDATA,FDATAC)
C      READS FLIGHT DATA AND SORTS BY MACH OR PARAM
COMMON /WTDATA/ NCLA,NCLO,ABP,MBP,BP,NCMAX,LONG
COMMON /CGCOR/ SHIFT,CGLA,CGL0,C0B
COMMON /CASES/ NCASE
COMMON /NBPS/ NMPP,NMBP,NBP,NPARAM
REAL FDATA(NCMX,ND,1),FDATAC(NCMX,ND,1),ABP(16),MBP(16),BP(8),
-   A(16),B(32),AC(16),BC(32),MACH,TITL(9)
LOGICAL LONG(8),SHIFT
INTEGER NCASE(32),LONLOC(21),LATLOC(19)
DATA PLT/4HPLOT/,ALAT/4HLATR/,LONLOC/1,2,3,6,9,10,11,1,2,3,5,6,7,
-   9,10,11,13,14,15,17,18/,LATLOC/1,2,3,6,7,10,11,1,2,3,5,6,7,
-   9,10,11,13,14,15/
ND2=ND/2
DO 10 I=1,32
10 NCASE(I)=0
20 READ (1,1000) TYPE,TITL,MACH,ALPHA,PARAM,CG
IF(TYPE.EQ.PLT) RETURN
WRITE(3,2000)TYPE,TITL,MACH,ALPHA,PARAM,CG
C      FLIGHT DATA IS STORED AS FDATA(COEFFICIENT,GROUP,CASE)
C      WHERE GROUP=INDEX IF LONG, OR INDEX+ND/2 IF LATR
C      AND INDEX IDENTIFIES EITHER THE MACH OR (IF NPARAM.GT.3)
C      THE EXTRA PARAMETER
CALL LOAD1(A)
CALL LOAD1(B)
CALL LOAD1(AC)
CALL LOAD1(BC)
INDEX=2
IF(ND2.LT.2) GO TO 60
IF(NPARAM.GT.0) GO TO 40
DO 30 INDEX=2,NMPP
IF(MACH.LT.(MBP(INDEX)+MBP(INDEX-1))*0.5) GO TO 60
30 CONTINUE
INDEX=NMBP+1
GO TO 60
40 DO 50 INDEX=2,NPARAM
IF(PARAM.LT.(BP(INDEX)+BP(INDEX-1))*0.5) GO TO 60
50 CONTINUE
INDEX=NPARAM+1
60 INDEX=INDEX-1
IF(TYPE.EQ.ALAT) GO TO 110
C      LONGITUDINAL - CHANGE SIGN OF X AND Z DERIVATIVES
DO 70 I=1,11,2
70 A(I)=-A(I)
DO 80 I=1,19,2
80 B(I)=-B(I)
NCAS=NCASE(INDEX)+1
IF(SHIFT) A(2)=A(2)+(CGL0-CG)*A(1)
DO 100 I=1,21
IF(I.GE.8) GO TO 90
FDATA(I,INDEX,NCAS)=A(LONLOC(I))
FDATAC(I,INDEX,NCAS)=AC(LONLOC(I))
GO TO 100
90 FDATA(I,INDEX,NCAS)=B(LONLOC(I))
FDATAC(I,INDEX,NCAS)=BC(LONLOC(I))
100 CONTINUE
GO TO 150
FLIG 0
FLIG 10
FLIG 20
FLIG 30
FLIG 40
FLIG 50
FLIG 60
FLIG 70
FLIG 80
FLIG 90
FLIG 100
FLIG 110
FLIG 120
FLIG 130
FLIG 140
FLIG 150
FLIG 160
FLIG 170
FLIG 180
FLIG 190
FLIG 200
FLIG 210
FLIG 220
FLIG 230
FLIG 240
FLIG 250
FLIG 260
FLIG 270
FLIG 280
FLIG 290
FLIG 300
FLIG 310
FLIG 320
FLIG 330
FLIG 340
FLIG 350
FLIG 360
FLIG 370
FLIG 380
FLIG 390
FLIG 400
FLIG 410
FLIG 420
FLIG 430
FLIG 440
FLIG 450
FLIG 460
FLIG 470
FLIG 480
FLIG 490
FLIG 500
FLIG 510
FLIG 520
FLIG 530
FLIG 540
FLIG 550
FLIG 560

```



## APPENDIX E — Continued

110 INDEX=INDEX+ND2	FLIG 570
NCAS=NCASE(INDEX)+1	FLIG 580
IF(SHIFT) A(3)=A(3)+(CGLA-CG)*COB*A(1)	FLIG 590
DO 130 I=1,19	FLIG 600
IF(I,GE,8) GO TO 123	FLIG 610
FDATA(I,INDEX,NCAS)=A(LATLOC(I))	FLIG 620
FDATA(I,INDEX,NCAS)=AC(LATLOC(I))	FLIG 630
GO TO 130	FLIG 640
120 FDATA(I,INDEX,NCAS)=B(LATLOC(I))	FLIG 650
FDATA(I,INDEX,NCAS)=BC(LATLOC(I))	FLIG 660
130 CONTINUE	FLIG 670
150 NCASE(INDEX)=NCAS	FLIG 680
FDATA(22,INDEX,NCAS)=ALPHA	FLIG 690
FDATA(23,INDEX,NCAS)=MACH	FLIG 700
FDATA(22,INDEX,NCAS)=PARAM	FLIG 710
FDATA(23,INDEX,NCAS)=CG	FLIG 720
GO TO 20	FLIG 730
1000 FORMAT(10A4,4F10.4)	FLIG 740
2000 FORMAT(1H0,A4,5X,9A4,4F10.4)	FLIG 750
END	FLIG 760

## APPENDIX E – Continued

### SUBROUTINE INSTR

Description: Subroutine INSTR reads plotting instructions.

Programing notes: The instructions are passed to the rest of the program in the following form:

NPLOT – number of coefficients to be plotted.

LATLON – 1 if lateral data, 2 if longitudinal data.

PARM, TOL – parameter value and tolerance.

LL – number of the predicted derivative data set corresponding to LATLON and PARM.

IDER – parameter numbers that correspond to the coefficients to be plotted.

YMIN, YMAX – minimum and maximum values for the ordinates.

# APPENDIX E — Continued

## Subroutine listing:

	SUBROUTINE INSTR	INST 0
C	READS INSTRUCTIONS ON COEFFICIENTS TO PLOT, SCALES TO USE,	INST 10
C	AND THE PARAMETER AND TOLERANCE FOR FLIGHT POINTS	INST 20
C	DO NOT OVERLAY THIS SUBROUTINE AS START, DERIV, SMIN AND SMAX MUST	INST 30
C	BE PRESERVED	INST 40
	COMMON /NBPS/ NBPP, NABP, NBP, NPARAM	INST 50
	COMMON /WTDATA/ NCLA, NCLO, ABP, MBP, BP, NCMAX, LONG	INST 60
	COMMON /INS/ NPLOT, WTPLOT	INST 70
	COMMON /SELECT/ PARAM, TOL, IDER, YMIN, YMAX, LATLON, DERIVS, LL, WTPLOT	INST 80
	REAL DERIV(4), SMIN(4), SMAX(4), CER(21,2), YMIN(21), YMAX(21),	INST 90
	- DERIVS(21), ABP(16), MBP(16), BP(8)	INST 100
	INTEGER IDER(21)	INST 110
	LOGICAL WTPLOT, WTPL, LONG(8)	INST 120
	DATA END, ALON, ALAT, BLANK, STAR/3HEND, 4HLONG, 4HLATR, 1H , 4HSTAR/	INST 130
	DATA DER/3HCYB, 3HCLB, 3HCNB, 3HCLP, 3HCNP, 3HCLR, 3HCNR, 4HCYDA, 4HCLDA,	INST 140
	- 4HCNDA, 4HCYDR, 4HCLDR, 4HCNDR, 4HCYD1, 4HCLD1, 4HCND1, 4HCYD2,	INST 150
	- 4HCLD2, 4HCND2, 2*1H ,	INST 160
	- 3HCNA, 3HCMA, 3HCAA, 3HCMQ, 3HCNV, 3HCMV, 3HCAV, 4HCNDE, 4HCME,	INST 170
	- 4HCAD, 4HCNDC, 4HCMDC, 4HCADC, 4HCND1, 4HCMO1, 4HCAD1, 4HCND2,	INST 180
	- 4HCMO2, 4HCAD2, 2HCN, 2HDE/	INST 190
	IF (STAR.NE.STAR) READ (1,1001) DERIV(1), SMIN(1), SMAX(1)	INST 200
	STAR=STAR	INST 210
	NPLOT=0	INST 220
	IF (DERIV(1).EQ.END) GO TO 120	INST 230
	LATLON=1	INST 240
	IF (DERIV(1).EQ.ALON) LATLON=2	INST 250
	NC=19	INST 260
	IF (LATLON.EQ.2) NC=21	INST 270
	PARAM=SMIN(1)	INST 280
	TOL=SMAX(1)	INST 290
	WRITE(3,2004) DERIV(1), PARAM, TOL	INST 300
20	READ (1,1001) (DERIV(I), SMIN(I), SMAX(I), I=1,4)	INST 310
	IF (DERIV(1).EQ.ALAT.OR.DERIV(1).EQ.ALON.OR.DERIV(1).EQ.END) GOTO 90	INST 320
	DO 70 I=1,4	INST 330
	IF (DERIV(I).EQ.BLANK) GO TO 80	INST 340
	NPLOT=NPLOT+1	INST 350
	YMIN(NPLOT)=SMIN(I)	INST 360
	YMAX(NPLOT)=SMAX(I)	INST 370
	DO 30 J=1,NC	INST 380
	IF (DERIV(I).EQ.DFR(J,LATLON)) GO TO 60	INST 390
30	CONTINUE	INST 400
	WRITE(3,2002) DERIV(I)	INST 410
	STOP	INST 420
60	IDER(NPLOT)=J	INST 430
70	DERIVS(NPLOT)=DERIV(I)	INST 440
	GO TO 20	INST 450
80	READ (1,1001) DERIV(1), SMIN(1), SMAX(1)	INST 460
90	WRITE(3,2001) (DER(IDER(I), LATLON), I=1, NPLOT)	INST 470
100	PARAM=PARAM	INST 480
	WTPL=WTPLOT	INST 490
	IF (NPARAM.GT.0) PARAM=0.	INST 500
	DO 110 II=1,NBP	INST 510
	IF ((LONG(II).AND.(LATLON.EQ.1)) .OR.	INST 520
	- (.NOT.LONG(II).AND.(LATLON.EQ.2))) GO TO 110	INST 530
	LL=II	INST 540
	IF (PARAM*BP(II)*(PARAM-BP(II)).EQ.(.)) GO TO 120	INST 550
110	CONTINUE	INST 560

# APPENDIX E — Continued

WRITE(3,2003)	INST 570
WTPL=,FALSE.	INST 580
1001 FORMAT(4(A4,F6.0,F10.0))	INST 590
2001 FORMAT(27H COEFFICIENTS TO BE PLOTTED/1X,2(A6)	INST 600
2002 FORMAT(1H0,A4,45H IS NOT A VALID DERIVATIVE NAME FOR THIS PLOT)	INST 610
2003 FORMAT(30HCNO WIND TUNNEL DATA AVAILABLE)	INST 620
2004 FORMAT(1H0,A4,6H PLOTS,5X,6HPARAM=,F10.4,5X,10HTOLERANCE=,F10.4)	INST 630
120 RETURN	INST 640
END	INST 650

## APPENDIX E — Continued

### SUBROUTINE SUMPLT

Description: Subroutine SUMPLT plots data for one derivative.

Programing notes: Most of the data manipulation has been done, and the data are ready to plot. Thus this subroutine does little except the actual plotting.

Subroutine listing:

C	SUBROUTINE SUMPLT(FDAT,FOATC,ALFS,ND2,DATA,NRP,NMRP,NABP) PLOTS SUMMARY INFORMATION FOR ONE DERIVATIVE COMMON /SUMDAT/ YLOC,XSKIP,ALFN,ASCAL2,YSTEP,AMIN,TABLAB,FDATA, - FDATA,TITLE COMMON /PSCL/ CRFACT,IWT1,IWT2,YLEN2,II,NPARAM COMMON /PDAT/ NOPLOT,VMN,YSCALE,NCAS,CRF,WTP,DERIV,WTO,KWT COMMON /WTDATA/ NCLA,NCLQ,ABP,MBP,BP,NCMAX,LONG REAL FDAT(ND2,1),FOATC(ND2,1),ALFS(ND2,1),DATA(NRP,NMRP,1), - FDATA(5000),FDATAC(5000),TABLAB(2),ABP(16),MBP(16),BP(8), - TITLE(20),WTO(18,16),APPS(18) INTEGER NCAS(16),ISYMB(16) LOGICAL NOPLOT,LONG(8),WTP DATA ISYMB/1,0,5,2,12,10,6,9,4,11,7,8,8,8,8,8/ NCMX=NCMAX+2 ND=ND2*2 CALL PSCL(NCMX,ND,ND2,FDATA,FDATAC,FCAT,FOATC,ALFS,DATA,NRP, - NMRP,NABP) IF(II.NE.1) GO TO 10 CALL PLOT(0.,-YLOC,-3) YLOC=0. CALL PLTDAT(XSKIP,12,25) 10 IF(NOPLOT) RETURN KWT1=KWT-1 J=0 DO 15 I=IWT1,IWT2 J=J+1 15 ABPS(J)=ABP(I) ABPS(KWT+1)=AMIN ABPS(KWT+2)=ASCAL2 IF(YLOC.NE.0.) GO TO 30 CALL PLOT(XSKIP,YSTEP,-3) CALL SYMBOL(.,YSTEP,.14,TITLE(1),0.,4) DO 20 I=2,20 20 CALL SYMBOL(999.,YSTEP,.14,TITLE(I),0.,4) YLOC=YSTEP GO TO 40 30 CALL PLOT(0.,-YSTEP,-3) YLOC=0. 40 CALL AXIS(0.,0.,5HALPHA,-5,ALFN,0.,AMIN,ASCAL2) CALL AXIS(0.,0.,DERIV,4,YLEN2,90.,VMN,YSCALE) CALL SYMBOL(ALFN,YLEN2,.10,4HSYMB,0.,4) CALL SYMBOL(ALFN+.5,YLEN2,.10,TABLAB,0.,8) YORG=YLEN2 DO 50 I=1,ND2 IF(NCAS(I).LE.0) GO TO 51 YORG=YORG+.25 CALL SYMBOL(ALFN+.1,YORG+.07,.14,ISYMB(I),0.,-1) BPVAL=MBP(I) IF(NPARAM.GT.0) BPVAL=BP(I) CALL NUMBER(ALFN+.5,YORG,.14,BPVAL,0.,2) 50 CONTINUE C PLOT FLIGHT POINTS DO 60 I=1,ND2 NCI=NCAS(I) IF(NCI.LE.0) GO TO 70 ISI=ISYMB(I) DO 60 J=1,NCI	SUMP 0 SUMP 10 SUMP 20 SUMP 30 SUMP 40 SUMP 50 SUMP 60 SUMP 70 SUMP 80 SUMP 90 SUMP 100 SUMP 110 SUMP 120 SUMP 130 SUMP 140 SUMP 150 SUMP 160 SUMP 170 SUMP 180 SUMP 190 SUMP 200 SUMP 210 SUMP 220 SUMP 230 SUMP 240 SUMP 250 SUMP 260 SUMP 270 SUMP 280 SUMP 290 SUMP 300 SUMP 310 SUMP 320 SUMP 330 SUMP 340 SUMP 350 SUMP 360 SUMP 370 SUMP 380 SUMP 390 SUMP 400 SUMP 410 SUMP 420 SUMP 430 SUMP 440 SUMP 450 SUMP 460 SUMP 470 SUMP 480 SUMP 490 SUMP 500 SUMP 510 SUMP 520 SUMP 530 SUMP 540 SUMP 550 SUMP 560
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# APPENDIX E — Continued

XN=(ALFS(I,J)-AMIN)/ASCAL2	SUMP 570
YN=(F0AT(I,J)-YMN)/YSCALE	SUMP 580
CALL SYMBOL(XN,YN,.14,ISI,0.,-1)	SUMP 590
IF(F0ATC(I,J).EQ.0.) GO TO 60	SUMP 600
HITE=F0ATC(I,J)/YSCALE	SUMP 610
YNH=YN+HITE	SUMP 620
XNP=XN+.03	SUMP 630
XNM=XN-.03	SUMP 640
CALL PLOT(XNM,YNH,3)	SUMP 650
CALL PLOT(XNP,YNH,2)	SUMP 660
CALL PLOT(XN,YNH,3)	SUMP 670
YNH=YN-HITE	SUMP 680
CALL PLOT(XN,YNH,2)	SUMP 690
CALL PLOT(XNM,YNH,3)	SUMP 700
CALL PLOT(XNP,YNH,2)	SUMP 710
60 CONTINUE	SUMP 720
C PLOT WIND TUNNEL DATA	SUMP 730
70 IF(.NOT.WTP) GO TO 90	SUMP 740
IF(NPARAM.GT.0 .AND. I.EQ.1) GO TO 80	SUMP 750
IF(NPARAM.GT.0 .OR. NCI.FQ.0) GO TO 90	SUMP 760
80 WTD(KWT+1,I)=YMN	SUMP 770
WTD(KWT+2,I)=YSCALE	SUMP 780
CALL LINES(ARPS,WTD(1,I),KWT,1,KWT1,ISI)	SUMP 790
90 CONTINUE	SUMP 800
YN=-YMN/YSCALE	SUMP 810
IF(YN.LE.0. .OR. YN.GT.YLEN2) GO TO 100	SUMP 820
CALL PLOT(ALEN,YN,3)	SUMP 830
CALL PLOT(0.,YN,2)	SUMP 840
100 CONTINUE	SUMP 850
RETURN	SUMP 860
END	SUMP 870

## APPENDIX E – Continued

### SUBROUTINE PSCALE

**Description:** Subroutine PSCALE selects flight data points to be plotted on the basis of the criteria specified in subroutine INSTR. It places flight data and predicted derivatives for a single derivative into arrays for plotting and determines ordinate scales if needed.

**Programing notes:** Flight data are moved from arrays FDATA and FDATAAC to arrays FDAT, FDATC, and ALFS. Array FDAT contains the derivative values, FDATC the confidence levels, and ALFS the angles of attack. Predicted derivatives are selected from array DATA and moved to array WTD.

Subroutine listing:

```

      SUBROUTINE PSCALE(NCMX,ND,ND2,FDATA,FDATAC,FOAT,FOATC,ALFS,DATA, PSCA  0
-      NBP,NMBP,NARP) PSCA 10
C   DETERMINES PLOT SCALES, SELECTS DATA TO BE PLOTTED PSCA 20
C   DATA TO BE PLOTTED IS SELECTED FROM ARRAYS FDATA AND FDATAAC PSCA 30
C   AND PLACED INTO THE SMALLER ARRAYS FOAT,FOATC, AND ALFS PSCA 40
      COMMON /CASES/ NCASE PSCA 50
      COMMON /PSCL/ CRFACT,IWT1,IWT2,YLEN2,II,NPARAM PSCA 60
      COMMON /SELECT/ PARAM,TOL,IDER,YMIN,YMAX,LATLON,DERIVS,LL,WTP PSCA 70
      COMMON /PDAT/ NOPLOT,YMN,YSCALE,NCAS,CRF,WTP,DERIV,WTC,KWT PSCA 80
      REAL FDATA(NCMX,ND,1),FDATAC(NCMX,ND,1),FOAT(ND2,1),FOATC(ND2,1), PSCA 90
-      ALFS(ND2,1),DATA(NBP,NMBP,1),YMIN(21),YMAX(21),ZSC(4), PSCA 100
-      DERIVS(21),WTD(18,16) PSCA 110
      INTEGER IDER(21),NCAS(16),NCASE(32) PSCA 120
      LOGICAL WTP,NOPLT PSCA 130
      WTP=WTP PSCA 140
      LONLAT=ND2*(2-LATLON) PSCA 150
      JDER=IDER(II) PSCA 160
      DERIV=DERIVS(II) PSCA 170
      ZSC(1)=0. PSCA 180
      ZSC(2)=0. PSCA 190
      CRF=CRFACT PSCA 200
      IF(JDER.GT.19) CRF=0. PSCA 210
      IF(JDER.EQ.21) WTP=.FALSE. PSCA 220
      NOPLT=.TRUE. PSCA 230
      DO 90 JJ=1,ND2 PSCA 240
      JJL=JJ+LONLAT PSCA 250
      NCJ=0 PSCA 260
      NCASEJ=NCASE(JJL) PSCA 270
      IF(NCASEJ.LE.0) GO TO 60 PSCA 280
      DO 50 I=1,NCASEJ PSCA 290
      IF( PARAM*FDATAC(22,JJL,I).NE.0. .AND. PSCA 300
-      ABS(PARAM-FDATAC(22,JJL,I)).GT.TOL) GO TO 50 PSCA 310
      IF(FDATAC(JDER,JJL,I).LE.0.) GO TO 50 PSCA 320
      NCJ=NCJ+1 PSCA 330
      FDAT(JJ,NCJ)=FDATA(JDER,JJL,I) PSCA 340
      FDATC(JJ,NCJ)=FDATAC(JDER,JJL,I)*CRF PSCA 350
      ALFS(JJ,NCJ)=FDATA(22,JJL,I) PSCA 360
      ZSC(1)=AMIN1(ZSC(1),FDAT(JJ,NCJ)-FDATC(JJ,NCJ)) PSCA 370
      ZSC(2)=AMAX1(ZSC(2),FDAT(JJ,NCJ)+FDATC(JJ,NCJ)) PSCA 380
50 CONTINUE PSCA 390
60 IF(.NOT. WTP) GO TO 85 PSCA 400
      IF(NPARAM.GT.0 .AND. JJ.EQ.1) GO TO 70 PSCA 410
      IF(NPARAM.GT.0 .OR. NCJ.EQ.0) GO TO 85 PSCA 420
70 K1=(JDER-1)*NABP+IWT1 PSCA 430
      KWT=IWT2-IWT1+1 PSCA 440
      K2=K1+IWT2-IWT1 PSCA 450
      J=0 PSCA 460
      DO 80 I=K1,K2 PSCA 470
      J=J+1 PSCA 480
      WTD(J,JJ)=DATA(LL,JJ,I) PSCA 490
      ZSC(1)=AMIN1(ZSC(1),DATA(LL,JJ,I)) PSCA 500
80 ZSC(2)=AMAX1(ZSC(2),DATA(LL,JJ,I)) PSCA 510
85 NCAS(JJ)=NCJ PSCA 520
90 NOPLT=NOPLT .AND. (NCJ.EQ.0) PSCA 530
      IF(NOPLT) GO TO 110 PSCA 540
      IF(YMAX(II).EQ.YMIN(II)) GO TO 100 PSCA 550
      YMN=YMIN(II) PSCA 560

```

## APPENDIX E — Concluded

YSCALE=(YMAX(II)-YMIN(II))/YLEN2	PSCA 570
GO TO 200	PSCA 580
100 CALL SCALES(ZSC,YLEN2,2,.,FALSE.)	PSCA 590
YMN=ZSC(3)	PSCA 600
YSCALE=ZSC(4)	PSCA 610
GO TO 200	PSCA 620
110 WRITE(3,2000)DERIV	PSCA 630
2000 FORMAT(30H000 FLIGHT DATA AVAILABLE FOR ,A4)	PSCA 640
200 RETURN	PSCA 650
END	PSCA 660

SUBROUTINES WINDIN, LOAD1, SCALES, LINES,  
PLTDAT, TIME, AND DATE

Subroutines WINDIN, LOAD1, SCALES, LINES, PLTDAT, TIME, and DATE are identical to those in the SETUP and MMLE program.



## APPENDIX F

### SAMPLE CASE FOR THE SUMARY PROGRAM

This appendix presents a sample case for the SUMARY program.

#### INPUT CARDS

```

SAMPLE CASE FOR SUMARY
$WIND NCLO=6, LONG(1)=T, NABP=4, BODY=T, AMAX=24., ASCALE=2., CRFACT=10., $END
CN      2
.4      .65      .9      1.
CNA     2      .07      .365      .06
CMA     2      -.005      -.008      -.012
CNDE    1
.02
CMDE    1
-.01
CMQ     2
-5.      -5.      -5.2      -6.
5.      10.      15.      20.
.5
1.
LONG    AIRCRAFT B    FLT 1 CASE 1      0.000  4.803  1.000  .260
A      3      4
-.069730  0.000000  0.000000  -.005420
-.005095 -5.276583  0.000000  0.000000
.003742  0.000000  0.000000  0.000000
B      3      6
-.008488  0.000000  0.000000  0.000000  -3.346488  .076020
-.010056  0.000000  0.000000  0.000000 -2.288757  0.000000
.003654  0.000000  0.000000  0.000000 -3.328265  0.000000
AC     3      3
.000720  0.000000  0.000000
.000077  .362775  0.000000
0.000000  0.000000  0.000000
BC     3      5
.000656  0.000000  0.000000  0.000000  .004551
.000213  0.000000  0.000000  0.000000  .000825
0.000000  0.000000  0.000000  0.000000  0.000000
LONG    AIRCRAFT B    FLT 1 CASE 4      0.000  10.031  1.000  .260
A      3      4
-.068788  0.000000  0.000000  -.016320
-.004044 -6.148364  0.000000  0.000000
.006651  0.000000  0.000000  0.000000
B      3      6
-.006378  0.000000  0.000000  0.000000  -6.53271  .115600
-.010248  0.000000  0.000000  0.000000 -5.328408  0.000000
.002856  0.000000  0.000000  0.000000 -3.011942  0.000000
AC     3      3
.001169  0.000000  0.000000
.000086  .433856  0.000000
0.000000  0.000000  0.000000
BC     3      5
.001016  0.000000  0.000000  0.000000  .313379
.000192  0.000000  0.000000  0.000000  .001911
0.000000  0.000000  0.000000  0.000000  0.000000
LONG    AIRCRAFT B    FLT 1 CASE 8      0.000  13.671  1.000  .260
A      3      4
-.051724  0.000000  0.000000  -.026070
-.005240 -2.218513  0.000000  0.000000
.005995  0.000000  0.000000  0.000000
B      3      6
-.019702  0.000000  0.000000  0.000000  -8.13778  .112380
-.009046  0.000000  0.000000  0.000000 -6.745284 -0.000000
.002492  0.000000  0.000000  0.000000 -3.002600  0.000000
AC     3      3
.001280  0.000000  0.000000
.000644  .296974  0.000000
0.000000  0.000000  0.000000
BC     3      5
.001391  0.000000  0.000000  0.000000  .020161
.000202  0.000000  0.000000  0.000000  .001633
0.000000  0.000000  0.000000  0.000000  0.000000

```

# APPENDIX F — Continued

LONG	AIRCRAFT B	FLT 1	CASE 11	0.000	16.399	1.000	.260
A	3	4					
	-.058530	0.000000	0.000000	-.012960			
	-.008326	-2.095303	0.000000	0.000000			
	.005033	0.000000	0.000000	0.000000			
B	3	6					
	-.013062	0.000000	0.000000	0.000000	-.935426	.120320	
	-.010224	0.000000	.000046	0.000000	-8.717713	-0.000000	
	.002516	0.000000	0.000000	0.000000	.002881	0.000000	
AC	3	3					
	.001301	0.000000	0.000000				
	.000051	.219645	0.000000				
	0.000000	0.000000	0.000000				
BC	3	5					
	.001209	0.000000	0.000000	0.000000	.023573		
	.000147	0.000000	0.000000	0.000000	.001681		
	0.000000	0.000000	0.000000	0.000000	0.000000		
LONG	AIRCRAFT B	FLT 1	CASE 12	0.000	17.993	1.000	.260
A	3	4					
	-.066610	0.000000	0.000000	-.015460			
	-.007499	-4.851715	0.000000	0.000000			
	.005784	0.000000	0.000000	0.000000			
B	3	6					
	.001381	0.000000	0.000000	0.000000	-1.008667	.171330	
	-.011126	0.000000	0.000000	0.000000	-9.911981	-0.000000	
	.002070	0.000000	0.000000	0.000000	.004800	0.000000	
AC	3	3					
	.001335	0.000000	0.000000				
	.000056	.222093	0.000000				
	0.000000	0.000000	0.000000				
BC	3	5					
	.001252	0.000000	0.000000	0.000000	.027691		
	.000157	0.000000	0.000000	0.000000	.002271		
	0.000000	0.000000	0.000000	0.000000	0.000000		
LONG	AIRCRAFT B	FLT 1	CASE 15	0.000	20.088	1.000	.260
A	3	4					
	-.061936	0.000000	0.000000	-.003870			
	-.010069	-3.778632	0.000000	0.000000			
	.006358	0.000000	0.000000	0.000000			
B	3	6					
	-.006655	0.000000	0.000000	0.000000	-1.085620	.148190	
	-.011583	0.000000	0.000000	0.000000	-11.977400	-0.000000	
	.001551	0.000000	0.000000	0.000000	.012342	0.000000	
AC	3	3					
	.001470	0.000000	0.000000				
	.000073	.254969	0.000000				
	0.000000	0.000000	0.000000				
BC	3	5					
	.001046	0.000000	0.000000	0.000000	.030336		
	.000171	0.000000	0.000000	0.000000	.002594		
	0.000000	0.000000	0.000000	0.000000	0.000000		
LONG	AIRCRAFT B	FLT 1	CASE 17	0.000	21.376	1.000	.260
A	3	4					
	-.055533	0.000000	0.000000	-.008290			
	-.011031	-.436157	0.000000	0.000000			
	.006307	0.000000	0.000000	0.000000			
B	3	6					
	-.015876	0.000000	0.000000	0.000000	-1.154961	.164710	
	-.008337	0.000000	0.000000	0.000000	-13.301825	-0.000000	
	.001350	0.000000	0.000000	0.000000	.011709	0.000000	
AC	3	3					
	.001023	0.000000	0.000000				
	.000039	.133743	0.000000				
	0.000000	0.000000	0.000000				
BC	3	5					
	.000712	0.000000	0.000000	0.000000	.021764		
	.000086	0.000000	0.000000	0.000000	.001495		
	0.000000	0.000000	0.000000	0.000000	0.000000		

# APPENDIX F — Continued

LONG	AIRCRAFT B	FLT 1	CASE 19	0.000	22.641	1.000	.260
A	3	4					
	-.057218	0.000000	0.000000	-.005510			
	-.011844	.165115	0.000000	0.000000			
	.006115	0.000000	0.000000	0.000000			
B	3	6					
	-.012764	0.000000	0.000000	0.000000	-1.187400	.185320	
	-.007307	0.000000	0.000000	0.000000	-15.322314	-0.000000	
	.001150	0.000000	0.000000	0.000000	.012945	0.000000	
AC	3	3					
	.001052	0.000000	0.000000				
	.000060	.161152	0.000000				
	0.000000	0.000000	0.000000				
9C	3	5					
	.000772	0.000000	0.000000	0.000000	.025420		
	.000118	0.000000	0.000000	0.000000	.002325		
	0.000000	0.000000	0.000000	0.000000	0.000000		
PLOT							
LATR							
CNB							
LONG							
CN		CNA		CMDE		CNDE	
CMA		CMQ		DE		CMDC	
END							

# APPENDIX F — Continued

## OUTPUT LISTING

MMLE SUMMARY PLOTTING PROGRAM \*\*\*\* 1 JULY 1974 \*\*\*\* VERSION 2

SAMPLE CASE FOR SUMARY

CONFIDENCE LEVELS WILL BE PLOTTED MULTIPLIED BY 10.0

LONG	AIRCRAFT B	FLT 1 CASE 1	0.0000	4.8630	1.0000	.2600
LONG	AIRCRAFT B	FLT 1 CASE 4	0.0000	10.6310	1.0000	.2600
LONG	AIRCRAFT B	FLT 1 CASE 8	0.0000	13.6710	1.0000	.2600
LONG	AIRCRAFT B	FLT 1 CASE 11	0.0000	16.3990	1.0000	.2600
LONG	AIRCRAFT B	FLT 1 CASE 12	0.0000	17.9930	1.0000	.2600
LONG	AIRCRAFT B	FLT 1 CASE 15	0.0000	20.8880	1.0000	.2600
LONG	AIRCRAFT B	FLT 1 CASE 17	0.0000	21.3760	1.0000	.2600
LONG	AIRCRAFT B	FLT 1 CASE 19	0.0000	22.6410	1.0000	.2600

LATR PLOTS PARAM= -0.0000 TOLERANCE= -0.0000  
 COEFFICIENTS TO BE PLOTTED  
 CNB

NO WIND TUNNEL DATA AVAILABLE

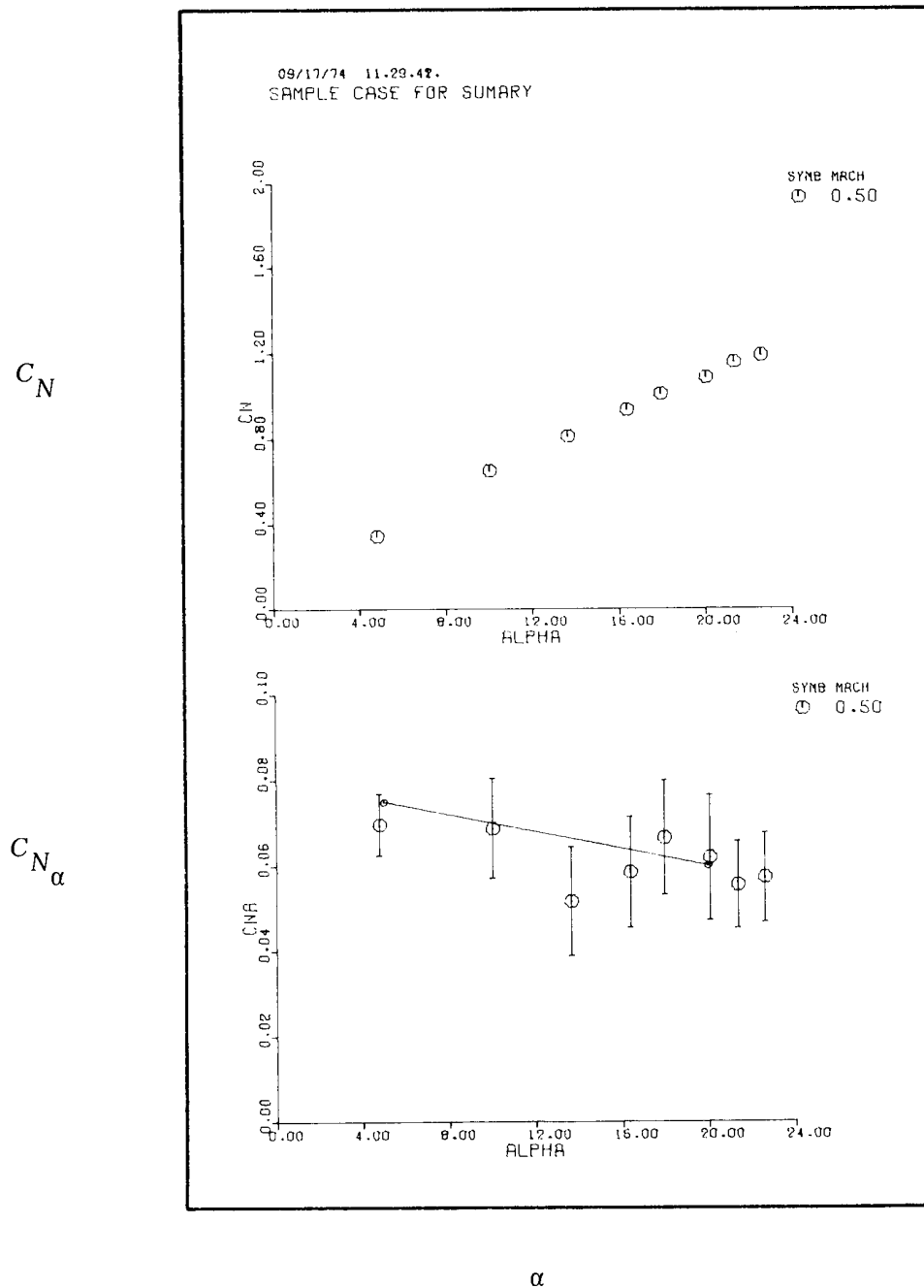
NO FLIGHT DATA AVAILABLE FOR CNB

LONG PLOTS PARAM= -0.0000 TOLERANCE= -0.0000  
 COEFFICIENTS TO BE PLOTTED  
 CN CNA CMDE CNDE CMA CMQ DE CMDC

NO FLIGHT DATA AVAILABLE FOR CMDC

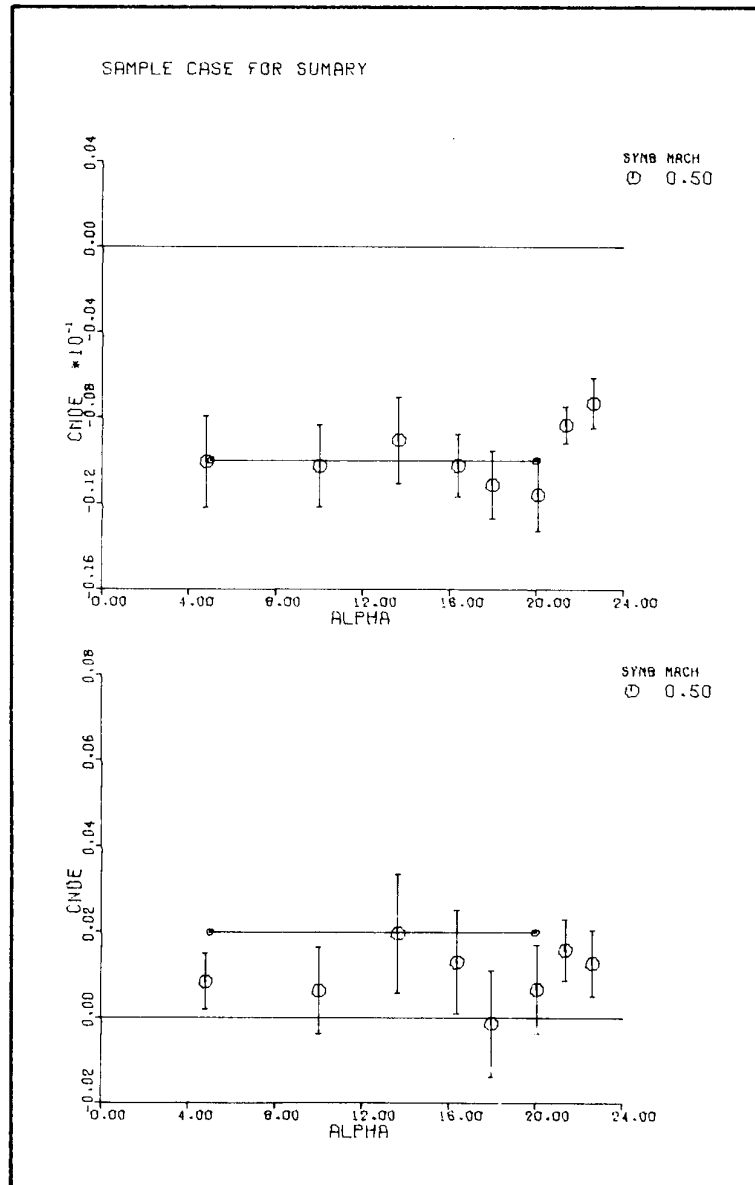
# APPENDIX F – Continued

A sample plot from the SUMARY program is shown. The plot is presented in four parts to avoid loss of detail from a large reduction. The plot as produced by the automatic plotter is shown within the heavy lines. Explanatory material is included to aid the user in implementing the program. Solid lines denote predicted derivatives. Vertical bars ( $\bar{I}$ ) indicate confidence levels.



# APPENDIX F — Continued

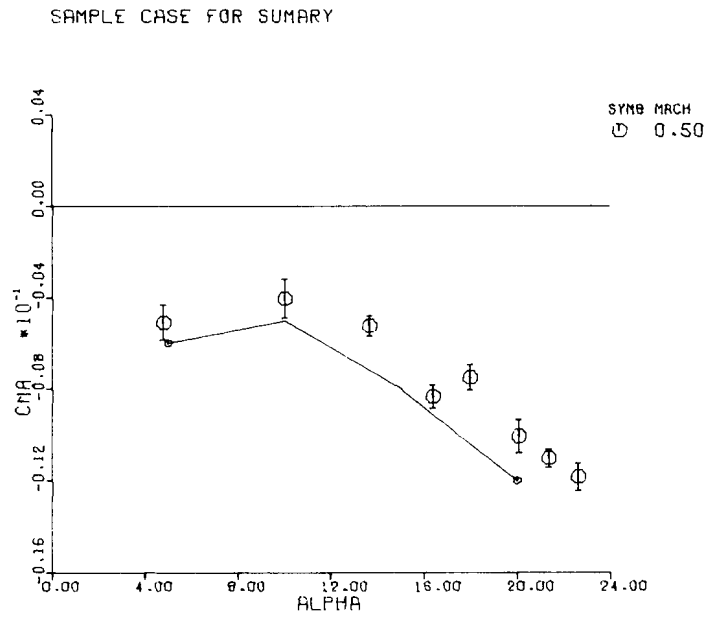
$C_{m\delta_e}$



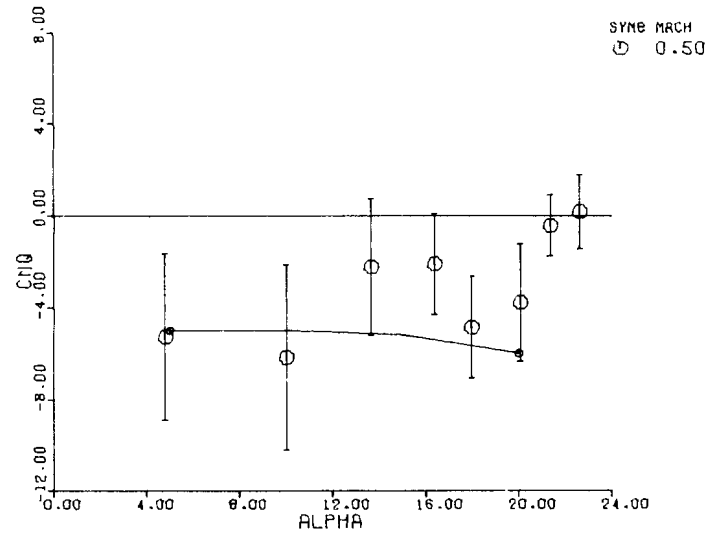
$\alpha$

# APPENDIX F — Continued

$C_{m_\alpha}$



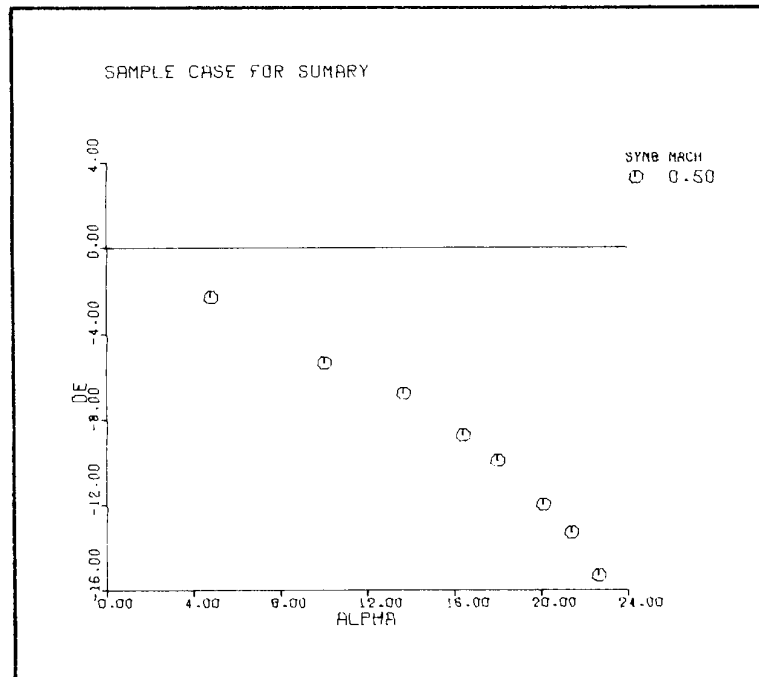
$C_{m_q}$



$\alpha$

# APPENDIX F — Concluded

$\delta_{e_{trim}}$



$\alpha$



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